

MULTILEVEL CONTROL OF LINEAR SYSTEMS

by

JACKY J. KRIEFF

Submitted in partial fulfillment of the requirements
for the Degree of Master of Science

School of Engineering
CASE WESTERN RESERVE UNIVERSITY

February 1968

CASE WESTERN RESERVE UNIVERSITY

GRADUATE STUDIES

We hereby approve the thesis of

Jacky Krieff

candidate for the M.S. Thesis

degree.

Signed:

R. Ritter
(Chairman)

Yasuhito Takahara
Donald Macko

Date

2/26/68

ABSTRACT

The "satisfaction approach" of Takahara [5] reduces the complexity of the computation of the control for a large scale system. Its aim is not to reach the optimum, but, given a reference control, to compute a new control such as to improve the performance. The fact that the optimum point is not reached is compensated by the fact that the computation is simplified. The numerical application of this technique is studied here (Chapter 2). This viewpoint of the problem leads (in Chapter 3) to an algorithm which improves the performance and deals with each subsystem separately. The iteration of this algorithm is shown to give the optimum, if some assumptions are satisfied.

Another approach for this kind of problem is the "decomposition technique": it reaches the optimal control of a large system by dealing with each subsystem separately and then coordinating the results. This technique was applied by S. Reich [3] in the case of linear systems with quadratic performances and is extended (Chapter 4) to the use of linear systems with disturbances. Moreover, with regard to the solution of the global system, the results do not show any reduction in the computing time of the optimal solution.

ACKNOWLEDGEMENTS

The author wishes to thank his thesis advisor Professor S. K. Mitter for his aid and encouragement during the course of this work. Appreciation is also extended to Professors M. D. Mesarovic and Y. Takahara for their helpful suggestions.

The author was supported in part by the National Science Foundation.

TABLE OF CONTENTS

List of Symbols.	vi
Chapter I-Introduction.	1
Chapter II-The Satisfaction Technique-Application To Linear Systems	3
2.1-Goals and Methods of the Satisfaction Approach.	3
2.2-Mathematical Formulation.	8
2.3-Theoretical Way of Applying the Satisfaction Technique.	14
2.4-A Heuristic for the Satisfaction Technique	18
2.5-Application of the Procedure to 2 Numerical Examples.	27
Chapter III-A Heuristic For a Satisfaction Approach With Separate Subsystems	35
3.1-The Method.	35
3.2-Application to Linear Quadratic Systems .	46
3.3-Application of the Heuristic to Slightly Non-Linear Systems.	49
3.4-Application of the Heuristic to a Linear System With 5 Variables. Computational Study of the Heuristic.	53
Chapter IV-Decomposition Technique Applied in Presence of Noise.	69
4.1-Case of Linear System with Quadratic Performances.	70
4.1.1-The Deterministic Problem	70
4.1.2-The Stochastic Problem.	76
4.2-A Case of Linear System With Non-Linear Coupling.	98
4.2.1-The Deterministic Problem	98
4.2.2-The Problem With Noises	99
4.3-Generalization.	112
Chapter V-Conclusions.	118

Appendix I-The Successive Sweep Method	120
Appendix II-The Decomposition Technique	123
Appendix III-Program 1	128
Program 2	134
Program 3	137
Program 4	142
Program 5	146
Appendix V-Program 6	151
Program 7	154
Program 8	157
Program 9	163
Program 10.	170
Program 11.	173
Bibliography	176

LIST OF SYMBOLS

- A Positive self adjoint linear operator from X into X .
- B Positive self adjoint linear operator from M into M .
- $C(T)$ Set of continuous real-valued functions defined on $[T]$.
- $D(T)$ Set of continuous real-valued functions defined on $[T]$.
- E Expectation operator.
- H Hamiltonian.
- H_m $\frac{\partial H}{\partial m}$.
- M Set of manipulated variables.
- M_i i^{th} projection of M .
- m Element of \underline{M} manipulated variable.
- m^r Reference control for the first level.
- m_j^r $P_j m^r$.
- n Number of the subsystems of the first level.
- N Vector Wiener Process: Noise in the system.
- N_i $P_i N$.
- P_i i^{th} projection operator.
- q Performance index on $M \times U$.
- q_j Performance index of the j^{th} subsystem on $M_j \times U_j$.
- r Desired value of a state variable.
- r_j j^{th} projection of r .

S_i	First kind of sensitivity functional for the i^{th} subsystem.
$S_m(t)$	Segment of $m(t)$.
s_j	Sensitivity (first kind) of the j^{th} subsystem - Uncertainty of the j^{th} subsystem.
T	Time index set : $[0, t_e]$.
t	Time index.
$t_{S(i)}$	Starting time of the i^{th} adaptation.
t_e	End time of control.
V	Uncertainty set - Posterior variance $\bar{V} = E [(x - \bar{x})(x - \bar{x})^T] = \text{matrix } (n, n)$
V_j	Set of v_j .
v_{ij}	Element of the matrix V .
v_j	Uncertainty for the j^{th} subsystem.
X	Set of state vector.
X_i	i^{th} projection of X .
x_i	Element of X_i .
x^r	State vector corresponding to m^r .
\bar{x}_i	$E(x_i)$.
\bar{x}	$E(x) = \text{posterior mean}$.
Y	Observation of the system.
Z	Vector Wiener Process: Noise in the measurements.
z_i	$P_i Z$.
ζ_j	Coordination variable for the j^{th} subsystem.
τ	Time index.
ϕ	Performance functional on $X \times M$.

- ϕ_i Performance functional of the i^{th} subsystem
on $X_i \times M_i$.
- $\leq(q)$ Ordering relation on M .
- $\leq(q_j)$ Ordering relation on M_j .

NOTATIONS

- $A^T =$ Transpose of A .
- $\dot{Y}(t) =$ Time derivative of $Y(t)$.
- $A, E, F, C:$ Time varying matrices defining the
successive sweep method.
- $h(t), w_1, w_2 :$ Time varying vectors defining the
successive sweep method.
- $g_1, g_2 :$ Real valued functions defined on T .
- $W :$ $\frac{1}{dt} [d N(t) \cdot d N^T(t)]$.
- $Q :$ $\frac{1}{dt} [d Z(t) \cdot d Z^T(t)]$.
- $v_{11}', v_{22}', \bar{x}_1', \bar{x}_2', v_{12}', v_{12}'' :$ Dummy variables.

CHAPTER I

INTRODUCTION

This thesis is concerned with the decomposition of the computation of optimal controls for large scale systems.

There are two parts:

The first part (Chapters 2 and 3) deals with a particular technique, the "satisfaction approach" studied by Takahara [5]. The satisfaction approach proceeds as follows: it allows performance improvement of a large system by dealing with separate subsystems, and the interconnections between the subsystems are viewed as internal disturbances. The second chapter is an application of the satisfaction approach to linear quadratic systems. The third chapter is another way of improving the performance by dealing with separate subsystems. With some assumptions this heuristic is shown to lead by iterations to the optimal control.

The second part (Chapter 4) deals with the use of the decomposition technique in large systems with disturbances. This decomposition technique is derived from a technique developed by Dantzig and Wolfe [1], and by Arrow [2]. The technique was studied and used by S. Reich [3] for deterministic linear systems, and deterministic linear systems with non-linear coupling. In this chapter, noises are introduced in an additive

way, both in the processes and the measurements. The noises are supposed to be Gaussian, uncorrelated, and their characteristics (mean and variance) are supposed to be known. The noises in the measurements introduce a new kind of interconnection between the subsystems so the decomposition technique cannot be applied directly. The Kalman technique [4] allows, however, in some specific cases the transformation of a stochastic problem into a deterministic one. Once the deterministic equations are found, the application of the decomposition technique presents no computational difficulty. However, it was not shown that this computation, based on a saddle-value argument should, in the general case, converge to the optimal point.

In all the numerical examples, the computation technique is the successive sweep method for the global method and the first level of the decomposition technique. The gradient method is used for the second level. The notations for the computation are those explained in Appendix 1.

CHAPTER II

THE SATISFACTION TECHNIQUE

APPLICATION TO LINEAR SYSTEMS

2.1 Goals and Methods of the Satisfaction Approach:

The decomposition technique is a way to break a large scale system into subsystems and then by a multi-level procedure find the overall optimum.

This is not the only way to approach the problem. The satisfaction approach, with the notion of "internal disturbances" leads to another multilevel procedure, dealing with separate subsystems. All the details on the method are taken from Takahara [5].

A multilevel system is a control system where a given controlled system is controlled by a group of goal seeking systems in a hierarchic arrangement.

By referring to Table 1 we find that: G_{11} , G_{12} , G_2 are goal seeking systems or controllers. G_{11} , G_{12} belong to the first level. G_2 belong to the second level.

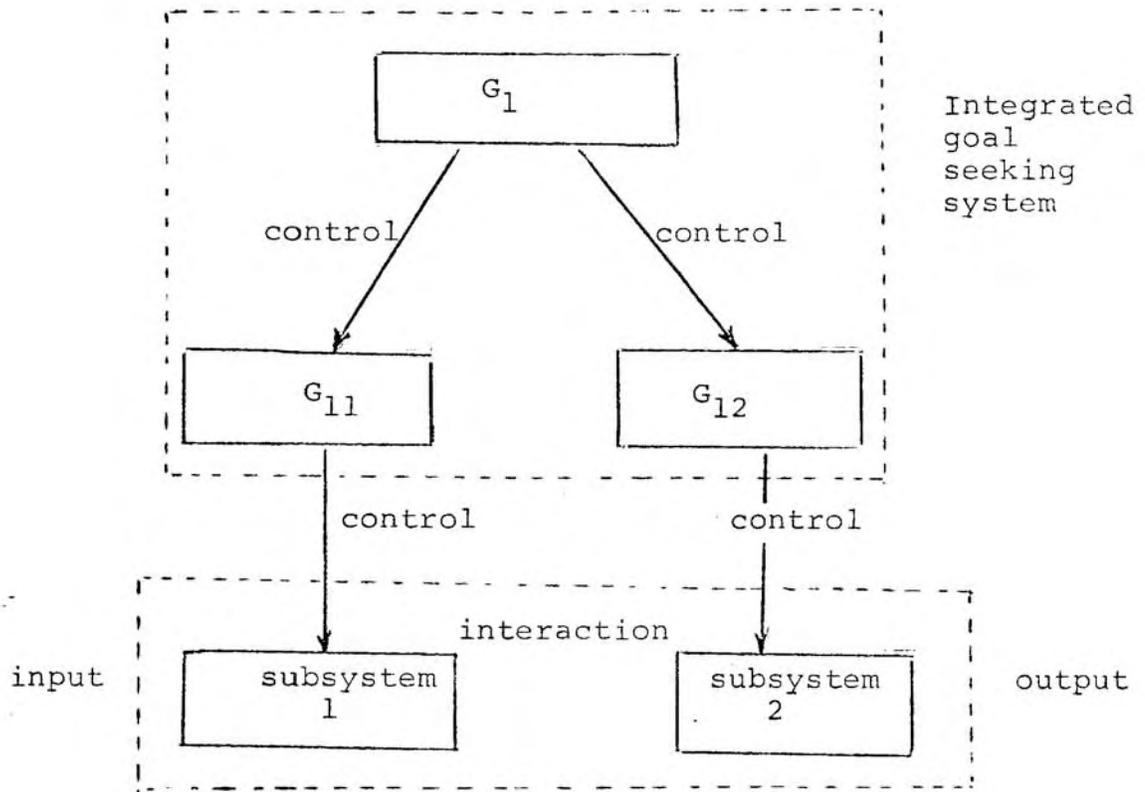


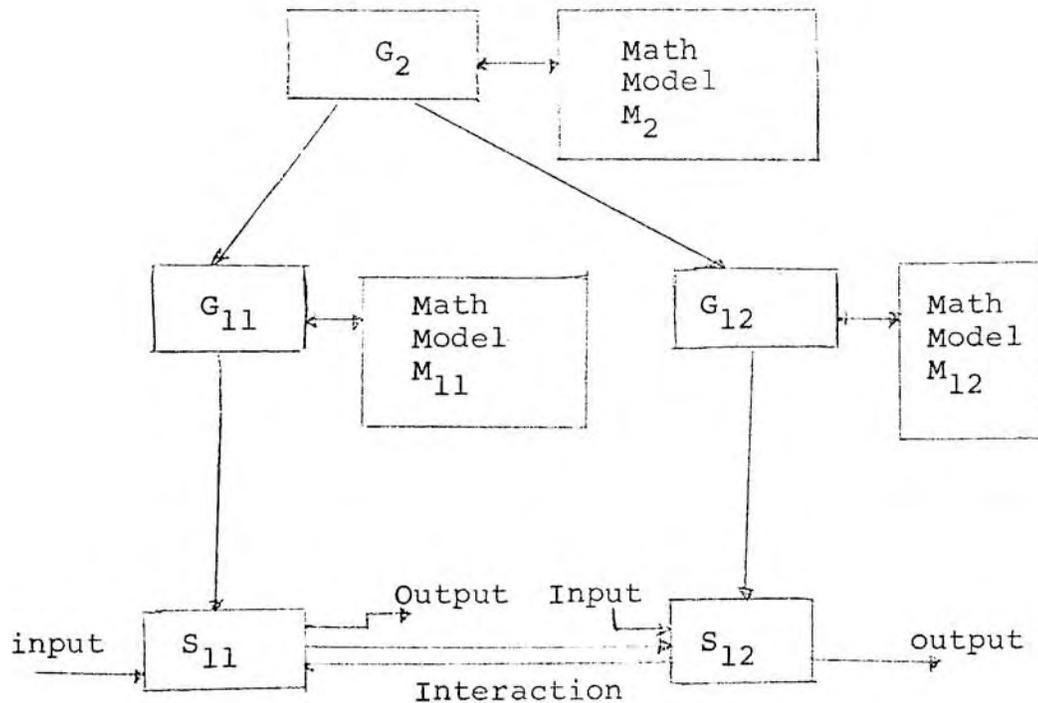
Table 1
Integrated Controlled System

G_{11} , G_{12} are assumed to control S_{11} and S_{12} separately. But in general S_{11} and S_{12} are interacting. So we must introduce a goal seeking G_2 in order to coordinate the G_{11} , G_{12} . G_2 improves the integrated performance by compensating the negligences of the interactions through the controllers G_{11} , G_{12} . Since these interactions are unknown for G_{11} and G_{12} , they are called internal disturbances (the term "external disturbances" being used for the noises).

The satisfaction approach uses a so-called on-line coordination, i.e., a coordination which does not use an iteration technique. The reason is that the use of an iteration technique, in a so-called off-line coordination technique supposes an harmoniously coordinable system, i.e., the system is such that there exists a best value for the coordination variable and this value can be reached by iteration technique.

Therefore, the goal of the satisfaction technique is not to get the optimum solution of the problem but to improve the overall performance, with respect to a reference control.

In a given control system, each controller has its own mathematical model for the control purpose.



The whole problem is to determine a mathematical model for each goal seeking system in relation to the integrated mathematical model.

We can repeat the problem of the satisfaction approach in the following way:

Let S be a real normed linear space on which an inner product is defined. The inner product is assumed to be continuous with respect to the topology derived from the norm. Let U , M and X be subsets of S . The relative topologies are defined on them. Let Ψ and ϕ be continuous mappings such that:

$$\Psi : M \times U \rightarrow X$$

$$\phi : X \times M \rightarrow R$$

$$\text{Let } q(m, u) = \phi (\Psi (m, u), m).$$

The satisfaction approach consists in finding:

1) If there exists $m^* \in M$ such that:

$$\forall u \in U \quad q(m^*, u) = V(u)$$

where $V(u)$ is the satisfaction threshold.

2) If m^* exists, then it is desired to find it explicitly.

2.2 Mathematical Formulation.

Hypothesis and Assumptions:

We consider a multilevel deterministic system in a real Banach space B . Let X and M be subsets of B ; we call them the state set and the manipulated variable set. The linear manifolds spanned by X and M will be written as \underline{X} and \underline{M} . Let the system have as its state equation

$$x = \Psi (m)$$

and performance functional:

$$q(m) = \phi (\Psi (m), m).$$

Assumptions:

1. Ψ and ϕ have Frechet derivatives.
2. M and X are convex sets in B and $X = \underline{X}$
 $\text{Int}(m) \neq \emptyset$. with respect to the relative topology.
3. $M = M_1 \oplus M_2 \oplus \dots \oplus M_n$

\oplus represents the direct sum operation.

$$M_i = P_i M$$

4. Let us call F_1 and F_2 the Frechet derivatives of ϕ with respect to x and m_1 . We assume that F_1 and F_2 have also continuous Frechet derivatives.

With these assumptions we can give some definitions very helpful for the classification of multilevel systems:

-The operator $K_i: M \rightarrow X$ such that

$$K_i: P_i \Psi(m) - \Psi(m) P_i$$

where P_i is the projection operator, is called the first kind of interaction operator.

If $K_i = 0$, we can write $x_i = \Psi(m_i) + x_0^i$ where x_0^i is a constant, i.e., the subsystems of the first level are isolated.

-The bounded linear functional $S_i : M \rightarrow R$ such that: $S_i = K_i^* F_1(x, m)$ where K_i^* is the adjoint of K_i and $F_1(x, m)$ is the Frechet derivative of ϕ with respect to x is called the first kind of sensitivity functional.

It can be shown that the variations of q with respect to the variations of m_i consist of two parts: one is the direct consequence of δm_i on x_i . The second, $\{-(S_i, \delta m_i)\}$ (inner product), is the consequence of the interactions among the subsystems.

Lastly we can deal with the interactions in the integrated performance functional with the help of the second kind of interaction operators, i.e.,

$$\begin{aligned} R_{i1} &: X \rightarrow \underline{X}' & R_{i2} &: X \rightarrow \underline{M}' \\ T_{i1} &: M \rightarrow \underline{X}' & T_{i2} &: M \rightarrow \underline{M}' \end{aligned}$$

with \underline{X}' , \underline{M}' conjugate spaces of the linear manifold spanned by X and M , and such that:

$$\begin{aligned} R_{ij} &= P_i^* D_x F_j(x, m) - D_x F_j(x, m) P_i \\ T_{ij} &= P_i^* D_m F_j(x, m) - D_m F_j(x, m) P_i \end{aligned}$$

where:

$$P_i^* \text{ is the adjoint of } P_i.$$

F_1 is the Frechet derivative of ϕ with respect to x .

F_2 is the Frechet derivative of ϕ with respect to m .

$D_x F_j$ is the Frechet derivative of F_j with respect to x .

We say that $\phi(x,m)$ is additive if $\phi(x,m)$ is represented

$$\text{as } \phi(x,m) = \sum_{i=1}^n \phi_i(x_i, m_i).$$

It was proved [5] that $\phi(x,m)$ is additive if and only if

$$R_{ij} (I - P_i) = 0 \text{ and } T_{ij} (I - P_i) = 0.$$

So, if the two kinds of interactions, K_i on one hand, R_{ij} and T_{ij} on the other hand, are equal to zero, then, the interactions are zero, the system can be reduced to n independent control subsystems. If any one of these is not zero, then we have interactions called internal disturbances.

In order to give a mathematical formulation of the subsystems we have to make some more assumptions on the system:

The integrated system is given as follows:

$$x = \Psi m + x^F \quad \text{state equation}$$

$$\phi(x,m) = [x - r, A(x - r)] + (m, B m) \quad \text{performance functional.}$$

Supplementary assumptions:

-M is compact.

$-q(m) = \phi(\Psi(m), m)$ is convex and it takes its unique unitical point in the interior of M .

$-\Psi$ is a linear operator such that: $\Psi : M \rightarrow X$.

$-A$ and B are linear, bounded, self adjoint positive operators.

$-r \in X$ is a constant.

$-\phi(x, m)$ is additive, i.e., ϕ can be rewritten in the following form:

$$\phi(x, m) = (x_1 - r_1, A_1(x_1 - r_1)) + \dots + (x_n - r_n, A_n(x_n - r_n)) + (m_1, B_1 m_1) + \dots + (m_n, B_n m_n)$$

With these assumptions, we can write the following formulation:

The j^{th} subsystem control problem of the first level is defined as follows:

$$x_j = \Psi_j m_j + v_j + x_j^F$$

$$\min_{m_j \in M_j} \phi_j(x_j, m_j, s_j) = (x_j - r_j, A_j(x_j - r_j)) + (m_j, B_j m_j) - (s_j, m_j)$$

$$q_j(m_j, v_j, s_j) = \phi_j(\Psi_j m_j + v_j + x_j^F, m_j, s_j)$$

where

$$x_j \in X_j, v_j \in V_j \subset X_j, m_j \in M_j, s_j \in S_j$$

and

$$\Psi_j = \Psi + P_j \Psi - \Psi P_j$$

$$x_j^F = P_j x^F$$

$$B_j = B_j + K_j^* A K_j$$

$$N_j = K_j \bar{m}_j$$

It was proved [5] that:

If

m'' & m' \in admissible set of controls

and

$$q_i(m''_i, v_i, s_i) \leq q_i(m'_i, v_i, s_i) \quad \forall_i \quad \forall v_i \in V_i, \quad \forall s_i \in S_i$$

then

$$q(m'') \leq q(m').$$

But the following theorem is also true and the demonstration is exactly the same:

Theorem: For m'' and m' \in admissible set of controls, such that:

$$q_i(m''_i, v''_i, s''_i) \leq q_i(m'_i, v''_i, s''_i) \quad \forall_i$$

we have:

$$q(m'') \leq q(m').$$

with

$$v''_i = K_i \bar{m}''_i$$

$$s''_i = 2(K_i^* A(x'' - r) + K_i^* A K_i m'')$$

This formulation of the problem, i.e., the mathematical models of the subsystems, is a second order approximation of the integrated system. Since the integrated system we shall deal with is assumed to be linear-quadratic a second order approximation can represent the global property precisely and if a general system

can be approximated by a linear quadratic system, then this formulation will be applicable.

2.3 Theoretical Way of Applying the Satisfaction Technique

We shall study a linear example:

$$\frac{dx}{dt} = C x + m.$$

or

$$\begin{cases} \frac{dx_1}{dt} = c_{11} x_1 + c_{12} x_2 + m_1 \\ \frac{dx_2}{dt} = c_{21} x_1 + c_{22} x_2 + m_2 \end{cases}$$

with the performance:

$$\phi = \int_0^t e^{-\lambda t} \{ (x - r)^T A (x - r) + m^T B m \} dt$$

with

$$A = \begin{bmatrix} A_1 & 0 \\ 0 & A_2 \end{bmatrix} \quad B = \begin{bmatrix} B_1 & 0 \\ 0 & B_2 \end{bmatrix}$$

Notations:

For a linear example like the one we are studying we can write:

$$x_1(t) = x_1^f + (\Psi_1 m_1)(t) + (K_1 m_2)(t).$$

with

x_1^f = free movement of the subsystem 1.

$\Psi_1 m_1$ = control action within subsystem 1.

$K_1 m_2$ = interaction between the two subsystems.

This can be shown in the following way: $x(t)$, solution of a linear differential equation can be written:

$$x(t) = \varphi(t) x(0) + \int_0^t \varphi(t - \tau) m(\tau) d\tau$$

with $\varphi(t)$ = transition matrix.

If we call

$$\varphi = \begin{bmatrix} \varphi_{11} & \varphi_{12} \\ \varphi_{21} & \varphi_{22} \end{bmatrix}$$

we get

$$\begin{cases} x_1^f(t) = \varphi_{11}(t) x_1(0) + \varphi_{12}(t) x_2(t) \\ \psi_1 m_1(t) = \int_0^t \varphi_{11}(t - \tau) m_1(\tau) d\tau \\ K_1 m_2(t) = \int_0^t \varphi_{12}(t - \tau) m_2(\tau) d\tau \end{cases}$$

Fundamental theorem:

Given a reference control $[m_1^r, m_2^r]$, the internal disturbances $v_1^r = K_1 m_2^r$

$$v_2^r = K_2 m_1^r$$

$$s_1^r = 2[K_1^* A (x^r - r) + K_1^* A K_1 m^r]$$

$$s_2^r = 2[K_2^* A (x^r - r) + K_2^* A K_2 m^r]$$

and the following systems, equations and performances:

-sub system 1:

$$\begin{cases} x_1 = \psi_1 m_1 + x_1^f + v_1^r \\ \phi_1(x_1, m_1) = \int_0^t e^{\{A_1(x_1 - r_1)^2 + B_1^1 m_1^2 - s_1^r m_1\}} dt \\ = q(m_1, v_1^r, s_1^r) \end{cases}$$

-sub system 2:

$$x_2 = \Psi_2 m_2 + x_2^f + v_2^r$$

$$\begin{aligned} \phi(x_2, m_2) &= \int_0^t e^{(A_2(x_2-r_2)^2 + B_2^1 m_2^2 - s_2^r m_2)} dt \\ &= q_2(m_2, v_2^r, s_2^r). \end{aligned}$$

If we can find controls $m_1'(t)$ and $m_2'(t)$ such that

$$\text{and } \begin{cases} q_1(m_1', v_1^r, s_1^r) \leq q_1(m_1^r, v_1^r, s_1^r) \\ q_2(m_2', v_2^r, s_2^r) \leq q_2(m_2^r, v_2^r, s_2^r) \end{cases}$$

Then we have, for the overall problem:

$$q(m') \leq q(m).$$

Proof: This is exactly the fundamental theorem we stated in the preceding paragraph.

The heuristic is now obvious:

1st level - 1st subsystem - ith stage:

$$\text{equation } x_1 = \Psi_1 m_1 - x_1^f + v_1^r$$

performance:

$$\phi(i, x_1, m_1) = q_1(i, m_1, v_1^r, s_1^r) = \int_{t_S(i)}^t e^{\{A_1(x_1-r_1)^2 + B_1^1 m_1^2 - s_1^r m_1\}} dt$$

Given m_1^r, v_1^r, s_1^r by the second level, find:

$m_1'(t)$ such that:

$$q_1(i, m_1', v_1^r, s_1^r) \leq q_1(i, m_1^r, v_1^r, s_1^r).$$

2nd level - ith stage:

Let us call $m(i, t)$ the ith adaptation stage control of the first level, $q(i, m)$ the first level performance

index for the i^{th} adaptation stage, $t_s(i)$ the starting time of the i^{th} adaptation stage and

$Sm^r(i-1, t)$ the restriction of $m^r(i-1, t)$ to $[t_s(i), t_e]$

Let us call $Sm'(i-1, t)$ the restriction of $m'(i-1, t)$ to $[t_s(i), t_e]$

Given the control in the following way:

$$m^r(i, t) = \lambda S m^r(i-1, t) + (1 - \lambda) S m'(i-1, t)$$

and the system:

$$\dot{x}^r(i, t) = \Psi(i)m^r(i, t) + x^f(i, t)$$

the performance:

$$\phi = \int_{t_s(i)}^{t_e} \{ (x^r - r)^T A (x^r - r) + m^{rT} B m^r \} dt$$

Find:

$-\lambda_0$ such that: λ_0 minimizes ϕ

-Compute: $v_1^r = K_1 m_2^r$ $v_2^r = K_2 m_1^r$

$$s_1^r = 2[K_1^* A (x^r - r) + K_1^* A K_1 m^r]$$

$$s_2^r = 2[K_2^* A (x^r - r) + K_2^* A K_2 m^r]$$

With this scheme we have:

$$\begin{aligned} q[i, S m^r(i-1)] & \geq q[i, m^r(i)] \geq q[i, m'(i)] \\ q[i, S m'(i-1)] & \end{aligned}$$

This scheme is perfect from a theoretical point of view, but not easy to implement with a computer.

2.4 A Heuristic for the Satisfaction Technique

In this paragraph, no new concept is introduced. The preceding theoretical scheme is adapted in order to be computable.

This computation scheme is an adaptation of the scheme outlined in [5].

The system we study is always the same, i.e., a linear quadratic system. But the trick is to exchange the roles of x and m , i.e.,

$$\begin{cases} m_1(t) = \frac{dx_1}{dt} - c_{11} x_1 - c_{12} x_2 \\ m_2(t) = \frac{dx_2}{dt} - c_{22} x_2 - c_{21} x_1 \end{cases}$$

with the performance:

$$\phi = \int_0^t e^{\dots} \{ (x - r)^T A (x - r) + m^T B m \} dt$$

Fundamental theorem:

Given a reference control (m_1^r, m_2^r) that is to say a reference trajectory (x_1^r, x_2^r) and given the sets of disturbances V_1, V_2, S_1, S_2 which contain respectively $v_1^r, v_2^r, s_1^r, s_2^r$ and the following systems, equations and performances:

*subsystem 1:

$$m_1(t) = \frac{dx_1}{dt} - c_{11} x_1 - v_1$$

$$q_1(i, x_1, v_1, s_1) = \phi_1(i, x_1, m_1) = \int_{t_S(i)}^t e^{-(t-\tau)} [A_1 + c_{21}^2 B_2] (x_1 - r_1)^2 + B_1 m_1^2 - 2x_1 s_1] d\tau$$

*subsystem 2:

$$m_2(t) = \frac{dx_2}{dt} - c_{22} x_2 - v_2$$

$$q_2(i, x_2, v_2, s_2) = \phi_2(i, x_2, m_2) = \int_{t_S(i)}^t e^{-(t-\tau)} [A_2 + c_{12}^2 B_1] (x_2 - r_2)^2 + B_2 m_2^2 - 2x_2 s_2] d\tau$$

If we can find controls $m_1'(t)$ and $m_2'(t)$ such that:

$$q_1(i, x_1', v_1, s_1) \leq q_1(i, x_1^r, v_1, s_1) \quad \forall v_1 \in V_1, \quad \forall s_1 \in S_1$$

and $q_2(i, x_2', v_2, s_2) \leq q_2(i, x_2^r, v_2, s_2) \quad \forall v_2 \in V_2, \quad \forall s_2 \in S_2$

Then we have, for the overall problem:

$$q(i, m') \leq q(i, m^r)$$

Proof:

$$q_1(i, x_1', v_1^r, s_1^r) = \int_{t_S(i)}^t e^{-(t-\tau)} [A_1 + B_2 c_{21}^2] (x_1' - r_1)^2 + B_1 m_1'^2 - 2s_1^r x_1'] d\tau$$

But

$$v_1^r = c_{12} x_2^r$$

$$s_1^r = B_2 c_{21} m_2^r + c_{21}^2 B_2 (x_1^r - r_1)$$

Then replacing v_1^r , s_1^r , m_1' by their value, we get:

$$q_1(i, x_1^r, v_1^r, s_1^r) = \int_{t_S(i)}^t e^{\{ (A_1 + B_2 c_{21}^2) (x_1^r - r_1) + B_1 \left[\frac{dx_1^r}{dt} - c_{11} x_1^r - c_{12} x_2^r \right] - 2[B_2 c_{21}^2 m_2^r + c_{21}^2 (x_1^r - r_1)] x_1^r \} dt}$$

Now we write:

$$q_1(i, x_1^r, v_1^r, s_1^r) = \int_{t_S(i)}^t e^{\{ [A_1 + B_2 c_{21}^2] [x_1^r - r_1]^2 + B_1 \left[\frac{dx_1^r}{dt} - c_{11} x_1^r - c_{12} x_2^r \right] - 2[B_2 c_{21}^2 m_2^r + c_{21}^2 (x_1^r - r_1)] x_1^r \} dt}$$

We call

$$\delta = \begin{pmatrix} \delta_1 \\ \delta_2 \end{pmatrix} = \begin{pmatrix} x_1^r - x_1^r \\ x_2^r - x_2^r \end{pmatrix} = x^r - x^r.$$

By hypothesis we have:

$$q_1(i, x_1^r, v_1^r, s_1^r) - q(i, x_1^r, v_1^r, s_1^r) \leq 0$$

Replacing

$$x_1^r \text{ by } (x_1^r - \delta_1)$$

and

$$q_1(i, x_1^r, v_1^r, s_1^r), q_1(i, x_1^r, v_1^r, s_1^r)$$

by their values, we get the following inequality = (2) :

$$\int_{t_S}^t e^{(i)} \left\{ (A_1 + B_2 c_{21}^2) (x_1^r - \delta_1 - r_1)^2 + B_1 \left[\frac{dx_1^r}{dt} - c_{11} x_1^r - c_{12} x_2^r - \frac{d\delta_1}{dt} + c_{11} \delta_1 \right]^2 \right.$$

$$- 2[B_2 c_{21} \left[\frac{dx_2^r}{dt} - c_{22} x_2^r - c_{21} x_1^r \right] + c_{21}^2 (x_1^r - r_1) (x_1^r - \delta_1)]$$

$$- [A_1 + B_2 c_{21}^2] (x_1^r - r_1)^2 - B_1 \left[\frac{dx_1^r}{dt} - c_{11} x_1^r - c_{12} x_2^r \right]^2$$

$$+ 2[B_2 c_{21} \left\{ \frac{dx_2^r}{dt} - c_{22} x_2^r - c_{21} x_1^r \right\} + c_{21}^2 (x_1^r - r_1)] x_1^r \} dt \leq 0$$

Now we compute:

$$q(x^r - \delta_1) - q(x^r) =$$

$$\int_{t_S}^t e^{(i)} \left\{ A_1 (x_1^r - \delta_1 - r_1)^2 + B_1 \left[\frac{dx_1^r}{dt} - c_{11} x_1^r - c_{12} x_2^r - \frac{d\delta_1}{dt} + c_{11} \delta_1 \right]^2 \right.$$

$$+ B_2 c_{21}^2 [x_1^r - r_1 - \delta_1]^2 - 2(x_1^r - r_1)(x_1^r - \delta_1) - 2B_2 c_{21} \left(\frac{dx_1^r}{dt} - c_{22} x_2^r - c_{21} x_1^r \right) (x_1^r - \delta_1)$$

$$- A_1 (x_1^r - r_1)^2 - B_2 c_{21}^2 (x_1^r - r_1)^2 - B_1 \left[\frac{dx_1^r}{dt} - c_{11} x_1^r - c_{12} x_2^r \right]^2$$

$$+ 2x_1^r [B_2 c_{21} \left(\frac{dx_2^r}{dt} - c_{22} x_2^r - c_{21} x_1^r \right) + c_{21}^2 B_2 (x_1^r - r_1)] dt$$

Developing this expression algebraically we can find that $q(x^r - \delta_1) - q(x^r)$ is equal to the left hand side

of the inequality (2) .

So

$$q(x^r - \delta_1) - q(x^r) \leq 0.$$

In the same way we could have shown that:

$$q(x^r - \delta_1 - \delta_2) \leq q(x^r - \delta_1)$$

so

$$q(x') \leq q(x^r)$$

End of the proof.

Corollary:

Given a reference control (m_1^r, m_2^r) , i.e., a reference trajectory (x_1^r, x_2^r) and given

$$v_1^r = c_{12} x_2^r \quad s_1^r = B_2 c_{21} m_2^r + c_{21}^2 B_2 (x_1^r - r_1)$$

$$v_2^r = c_{21} x_1^r \quad s_2^r = B_1 c_{12} m_1^r + c_{21}^2 B_1 (x_2^r - r_2).$$

and the following systems, equations and performances:

-subsystem 1:

$$m_1(t) = \frac{dx_1}{dt} - c_{11} x_1 - v_1^r$$

$$q_1(i, x_1, v_1^r, s_1^r) = \phi_1(i, x_1, m_1) = \int_{t_S(i)}^t e^{-(A_1 + c_{21}^2 B_2)(x_1 - r_1)^2} + B_1 m_1^2 - 2x_1 s_1^r] dt$$

-subsystem 2:

$$m_2(t) = \frac{dx_2}{dt} - c_{22} x_2 - v_2^r$$

$$q_2(i, x_2, v_2^r, s_2^r) = \phi_2(i, x_2, m_2) = \int_{t_s(i)}^t e^{-(A_2 + c_{12}^2 B_1)(x_2 - r_2)^2 + B_2 m_2^2 - 2x_2 s_2^r} dt$$

If we can find controls $m_1'(t)$ and $m_2'(t)$ such that:

$$q_1(i, x_1^r, v_1^r, s_1^r) \leq q_1(i, x_1^r, v_1^r, s_1^r)$$

and $q_2(i, x_2^r, v_2^r, s_2^r) \leq q_2(i, x_2^r, v_2^r, s_2^r)$.

Then we have for the overall problem:

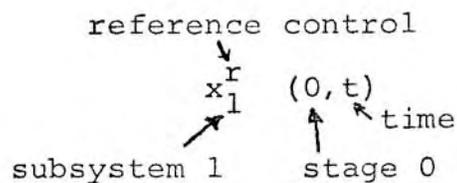
$$q(i, m') \leq q(i, m^r).$$

The proof of the corollary is straightforward.

A procedure was derived by Takahara [5] based on the preceding theories.

Procedure (1st stage only):

1. Given the system without any correlation, (we make $c_{12} = c_{21} = 0$), we compute the optimal solution, which we call: $x_1^r(0, t)$, $x_2^r(0, t)$, $m_1^r(0, t)$, $m_2^r(0, t)$ with



In this part 1, the problem is divided in two independent sub problems.

2. We compute

$$v_1^r(0, t) = c_{12} x_2^r(0, t)$$

$$s_1^r(0, t) = B_2 c_{21} m_2^r(0, t) + c_{21}^2 B_2 [x_1^r(0, t) - r_1].$$

3. subsystem 1:

$$\left\{ \begin{aligned} m_1(t) &= \frac{dx_1}{dt} - c_{11} x_1 - v_1^r \\ q_1(0, x_1, v_1^r, s_1^r) &= \phi_1(0, x_1, m_1) = \int_{t_S(0)}^t e^{-(t-\tau)} [(A_1 + c_{21}^2 B_2) (x_1 - r_1)^2 \\ &\quad + B_1 m_1^2 - 2x_1 s_1^r] d\tau \end{aligned} \right.$$

$$\min_{m_1} \phi_1(0, x_1, m_1) = \phi_1(0, x_1^0, m_1^0)$$

4. Compute:

$$v_2^r(0, t) = c_{21} x_1'$$

$$s_2^r(0, t) = B_1 c_{12} \left[\frac{dx_1'}{dt} - c_{11} x_1' - c_{12} x_2^r \right] + c_{12}^2 B_1 (x_2^r - r_2).$$

5. subsystem 2:

$$m_2(t) = \frac{dx_2}{dt} - c_{22} x_2 - v_2^r$$

$$q_2(0, x_2, v_2^r, s_2^r) = \phi_2(0, x_2, m_2) = \int_{t_S(0)}^t e^{-(t-\tau)} [(A_2 + c_{12}^2 B_1) (x_2 - r_2)^2 + B_2 m_2^2 - 2x_2 s_2^r] d\tau$$

$$\min_{m_2} \phi_2(0, x_2, m_2) = \phi_2(0, x_2^0, m_2^0)$$

6. Computation of $m_1'(0, t)$, $m_2'(0, t)$.

$$m_1'(0, t) = \frac{dx_1'}{dt} - c_{11} x_1' - c_{12} x_2'$$

$$m_2'(0, t) = \frac{dx_2'}{dt} - c_{21} x_1' - c_{22} x_2'$$

7. Computation of the new performance:

$$q[m'_1(0,t), m'_2(0,t)] = A_1(x'_1 - r_1)^2 + A_2(x'_2 - r_2)^2 + B_1 m'^2_1 + B_2 m'^2_2$$

And at this stage we have:

$$q[m'_1(0,t), m'_2(0,t)] \leq q[m^r_1(0,t), m^r_2(0,t)]$$

And the procedure can be applied again with a new reference control; in a new stage:

8. Computation of $m^r_1(1,t), m^r_2(1,t)$:

Given the feedback information

$$Sm_1(i-1,t)$$

$$Sm_2(i-1,t)$$

consider the control:

$$m^r(1,t) = \lambda Sm^r(0,t) + (1-\lambda) Sm(0,t)$$

the system

$$\frac{dx^r}{dt}(1,t) = c x^r(1,t) + m^r(1,t)$$

the performance

$$\phi = \int_{t_s(1)}^t e^{-\lambda t} \{ [x^r(1,t) - r]^T A [x^r(1,t) - r] + m^{rT}(1,t) B m^r(1,t) \} dt$$

Find λ such that $\min_{\lambda} \phi$

which gives the new reference control for the next stage:

$$m^r(1, t) = \begin{pmatrix} m_1^r(1, t) \\ m_2^r(1, t) \end{pmatrix}$$

Now the cycle is complete: we can start the computation again.

Survey of the procedure:

The procedure is a two level, multistage, updating procedure:

1st level:

steps 1, 3, 5: computation of a better control for the subsystems.

2nd level:

steps 2, 4: computation of $v_1^r, v_2^r, s_1^r, s_2^r$.

steps 6, 7: computation of the new control, and the new performance.

step 8: updating.

2.5 Application of the Procedure to 2 Numerical Examples

Example 1

Let us consider the following integrated system and performance functional:

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 2 & 2 \\ 2 & 3 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} m_1 \\ m_2 \end{bmatrix}$$

$$\phi(x, m) = \int_0^1 \{10(x_1^2 + x_2^2) + m_1^2 + m_2^2\} dt$$

$$x_1(0) = 5 \quad \text{and} \quad x_2(0) = 2.$$

Then

$$c = \begin{bmatrix} 2 & 2 \\ 2 & 3 \end{bmatrix} \quad A = \begin{bmatrix} 10 & 0 \\ 0 & 10 \end{bmatrix} \quad B = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$$

The procedure is the following:

Step 1

part a	{	system	$\dot{x}_1 = 2x_1 + m_1$
		performance	$\phi_1(x_1, m_1) = 10x_1^2 + m_1^2$
		Min m ₁	$\phi_1(x_1, m_1) = \phi_1[x_{1F}(0, t), m_1^r(0, t)]$
part b	{	system	$\dot{x}_2 = 3x_2 + m_2$
		performance	$\phi_2(x_2, m_2) = 10x_2^2 + m_2^2$
		min m ₂	$\phi_2(x_2, m_2) = \phi_2[x_{2F}(0, t), m_2^r(0, t)]$

part c $\frac{dx_1^r}{dt} = 2 x_1^r + 2 x_2^r + m_1^r (0, t)$

$$\frac{dx_2^r}{dt} = 2 x_1^r + 3 x_2^r + m_2^r (0, t)$$

Step 2

$$v_1^r (0, t) = 2 x_2^r (0, t)$$

$$s_1^r (0, t) = 2 m_2^r (0, t) + 4 [x_1^r (0, t) - r_1]$$

Step 3

$$\left\{ \begin{array}{l} \text{system} \quad \frac{dx_1}{dt} = 2 x_1 + m_1 + v_1^r (0, t) \\ \text{performance} \quad \phi_1[0, x_1, m_1] = \int_0^t e^{t-\tau} [14(x_1 - r_1)^2 + m_1^2 - 2 x_1 s_1^r] dt \end{array} \right.$$

$$\min_{m_1} \quad \phi_1[0, x_1, m_1] = \phi_1[0, x_1^0, m_1^0]$$

Step 4

$$v_2^r [0, t] = 2 x_1^r$$

$$s_2^r (0, t) = 2 \left[\frac{dx_1^r}{dt} - 2 x_1^r - 2 x_2^r \right] + 4 (x_2^r - r_2)$$

Step 5

$$\left\{ \begin{array}{l} \text{system} \quad \frac{dx_2}{dt} = 3 x_2 + m_2 + v_2^r (0, t) \\ \text{performance} \quad \phi_2(0, x_2, m_2) = \int_0^t e^{t-\tau} \{ 14(x_2 - r_2)^2 + m_2^2 - 2 x_2 s_2^r \} dt \end{array} \right.$$

$$\min_{m_2} \quad \phi_2(0, x_2, m_2) = \phi_2(0, x_2^0, m_2^0).$$

Step 6

$$\frac{dx'_1}{dt} = 2 x'_1 + 2 x'_2 + m'_1 (0, t)$$

$$\frac{dx'_2}{dt} = 2 x'_1 + 3 x'_2 + m'_2 (0, t)$$

Step 7

$$q[m'_1(0, t), m'_2(0, t)] = \int_0^t S \{ 10(x'_1 - r_1)^2 + 10(x'_2 - r_2)^2 + m'^2_1 + m'^2_2 \} dt$$

Step 8

Given the feedback information

$$Sm_1 (i-1, t)$$

$$Sm_2 (i-1, t)$$

$$\left\{ \begin{array}{l} \text{system} \quad \frac{dx^r}{dt} (1, t) = C x^r (1, t) + m^r (1, t) \\ \text{control} \quad m^r (1, t) = \lambda Sm^r (0, t) + (1-\lambda) Sm(0, t) \\ \text{performance} \quad \phi = \int_{t_S(1)}^t e^{-\lambda t} \{ A_1(x^r_1(1, t) - r_1)^2 + A_2(x^r_2(1, t) - r_2)^2 + B_1 m^r_1(1, t) + B_2 m^r_2(1, t) \} dt \end{array} \right.$$

Find λ_0 such that

$$\min_{\lambda} \phi (\lambda) = \phi [\lambda_0]$$

Computation:

Step 1:

-part a:

$$H = 10 x^2_{1F} + (m^r_1)^2 + p_1 (2 x_{1F} + m^r_1)$$

$$\mathcal{L} = 2 \quad \mathcal{E} = -0.5 \quad w_1 = \frac{1}{2} \quad \delta H m_1 \quad \mathcal{L} = -20 \quad w_2 = 0$$

-part b:

$$H = 10 x_{2F}^2 + (m_2^r)^2 + p_2 (3 x_{2F} + m_2^r)$$

$$\mathcal{L} = 3 \quad \mathcal{E} = -0.5 \quad w_1 = 0.5 \quad \delta H m_{2r} \quad \mathcal{L} = -20 \quad w_2 = 0$$

Step 3:

$$H = 14(x_1' - r_1)^2 + (m_1^0)^2 - 2 x_1' s_1^r + q_1 (2x_1' + m_1^0 + v_1^r)$$

$$\mathcal{L} = 2 \quad \mathcal{E} = -0.5 \quad w_1 = 0.5 \quad \delta H m_{11} \quad \mathcal{L} = -28 \quad w_2 = 0$$

Step 5:

$$H = 14(x_2' - r_2)^2 + (m_2^0)^2 - 2 x_2' s_2^r + q_2 (3x_2' + m_2^0 + v_2^r)$$

$$\mathcal{L} = 3 \quad \mathcal{E} = -0.5 \quad w_1 = 0.5 \quad \delta H m_{22} \quad \mathcal{L} = -28 \quad w_2 = 0$$

Example 2: A linear system with 5 variables:

The most general system is:

$$\frac{dx_i}{dt} = \sum_{j=1}^5 c_{ij} x_j + m_i \quad i = 1, 2, 3, 4, 5.$$

$$\phi = \int_0^t e^{-\sum_{j=1}^5 [A_j (x_j - r_j)^2 + B_j m_j^2]} dt.$$

We break the system in two parts:

$$\mathcal{L}_1 = \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} \quad \mathcal{L}_2 = \begin{bmatrix} x_3 \\ x_4 \\ x_5 \end{bmatrix}$$

$$M_1 = \begin{bmatrix} m_1 \\ m_2 \end{bmatrix}$$

$$M_2 = \begin{bmatrix} m_1 \\ m_2 \\ m_3 \end{bmatrix}$$

$$C_{11} = \begin{bmatrix} c_{11} & c_{12} \\ c_{21} & c_{22} \end{bmatrix}$$

$$C_{12} = \begin{bmatrix} c_{12} & c_{14} & c_{15} \\ c_{23} & c_{24} & c_{25} \end{bmatrix}$$

$$C_{21} = \begin{bmatrix} c_{31} & c_{32} \\ c_{41} & c_{42} \\ c_{51} & c_{52} \end{bmatrix}$$

$$C_{22} = \begin{bmatrix} c_{33} & c_{34} & c_{35} \\ c_{43} & c_{44} & c_{45} \\ c_{53} & c_{54} & c_{55} \end{bmatrix}$$

$$A_1 = \begin{bmatrix} A_1 & 0 \\ 0 & A_2 \end{bmatrix}$$

$$A_2 = \begin{bmatrix} A_3 & 0 & 0 \\ 0 & A_4 & 0 \\ 0 & 0 & A_5 \end{bmatrix}$$

$$B_1 = \begin{bmatrix} B_1 & 0 \\ 0 & B_2 \end{bmatrix}$$

$$B_2 = \begin{bmatrix} B_3 & 0 & 0 \\ 0 & B_4 & 0 \\ 0 & 0 & B_5 \end{bmatrix}$$

The system can now be written:

$$\frac{dX_1}{dt} = C_{11} X_1 + C_{12} X_2 + M_1$$

$$\frac{dX_2}{dt} = C_{21} X_1 + C_{22} X_2 + M_2$$

We can compute now:

$$\begin{aligned} v_1^r &= C_{12} x_2^r & v_2^r &= C_{21} x_1^r \\ s_1^r &= C_{21}^T b_2 m_2^r + C_{21}^T b_2 C_{21} (x_1^r - k_1) \\ s_2^r &= C_{12}^T b_1 m_1^r + C_{12}^T b_1 C_{12} (x_2^r - k_2) \end{aligned}$$

Now we consider the two subsystems:

1st subsystem:

$$\begin{aligned} \frac{dx_1}{dt} &= C_{11} x_1 + v_1^r \\ \min_{x_1} \phi_1 &= \int_0^t e^{\dots} \{ (x_1 - k_1)^T [a_1 + C_{21}^T b_2 C_{21}] [x_1 - k_1] \\ &\quad + m_1^T b_1 m_1 - 2 s_1^{rT} x_1 \} dt \end{aligned}$$

2nd subsystem:

$$\begin{aligned} \frac{dx_2}{dt} &= C_{22} x_2 + v_2^r \\ \min_{x_2} \phi_2 &= \int_0^t e^{\dots} \{ (x_2 - k_2)^T [a_2 + C_{12}^T b_1 C_{12}] [x_2 - k_2] \\ &\quad + m_2^T b_2 m_2 - 2 s_2^{rT} x_2 \} dt \end{aligned}$$

For the computation, with the successive sweep method, we get:

1st subproblem:

$$A = \begin{bmatrix} C_{11} & C_{12} \\ C_{21} & C_{22} \end{bmatrix} \quad \mathcal{E} = \begin{bmatrix} -\frac{1}{2B_1} & 0 \\ 0 & -\frac{1}{2B_2} \end{bmatrix} \quad w_1 = \begin{bmatrix} \frac{1}{2B_1} & \delta H m_1 \\ \frac{1}{2B_2} & \delta H m_2 \end{bmatrix}$$

$$\mathcal{L} = \begin{bmatrix} -2[A_1 + B_3 c_{31}^2 + B_4 c_{41}^2 + B_5 c_{51}^2] & -2[B_3 c_{31} c_{32} + B_4 c_{41} c_{42}] \\ & +B_5 c_{51} c_{52} \\ -2[B_3 c_{31} c_{32} + B_4 c_{41} c_{42} + B_5 c_{51} c_{52}] & -2[A_2 + B_3 c_{32}^2 + B_4 c_{42}^2] \\ & +B_5 c_{52}^2 \end{bmatrix}$$

$$w_2 = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

2nd subproblem:

$$A = \begin{bmatrix} c_{33} & c_{34} & c_{35} \\ c_{43} & c_{44} & c_{45} \\ c_{53} & c_{54} & c_{55} \end{bmatrix} \quad \mathcal{E} = \begin{bmatrix} -\frac{1}{2}B_3 & 0 & 0 \\ 0 & -\frac{1}{2}B_4 & 0 \\ 0 & 0 & -\frac{1}{2}B_5 \end{bmatrix}$$

$$\mathcal{L} = \begin{bmatrix} -2[A_3 + B_1 c_{13}^2 + B_2 c_{23}^2] & -2[B_1 c_{13} c_{14} + B_2 c_{23} c_{24}] \\ & -2[B_1 c_{13} c_{15} + B_2 c_{23} c_{25}] \\ -2[B_1 c_{13} c_{14} + B_2 c_{23} c_{24}] & -2[A_4 + B_1 c_{14}^2 + B_2 c_{24}^2] \\ & -2[B_1 c_{14} c_{15} + B_2 c_{24} c_{25}] \\ -2[B_1 c_{13} c_{15} + B_2 c_{23} c_{25}] & -2[B_1 c_{14} c_{15} + B_2 c_{24} c_{25}] \\ & -2[A_5 + B_1 c_{15}^2 + B_2 c_{25}^2] \end{bmatrix}$$

$$w_1 = \begin{bmatrix} \frac{1}{2B_3} & \delta Hm_3 \\ \frac{1}{2B_4} & \delta Hm_4 \\ \frac{1}{2B_5} & \delta Hm_5 \end{bmatrix} \quad w_2 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

The program of the computation is shown in Appendix 3, Program 1.

The results of this satisfaction approach are shown and compared to a new heuristic in the following chapter.

CHAPTER III

A HEURISTIC FOR A SATISFACTION APPROACH WITH SEPARATE SUBSYSTEMS

3.1 The Method:

Goal of the method:

In the last chapter we saw that the general technique of the satisfaction approach is rather complex when applied to linear systems. It is possible, at least when dealing with difference equations, to find a Heuristic much simpler and with the same advantages as the satisfaction approach.

What are the advantages of the application of the satisfaction approach with deterministic systems? Given a reference control, the technique allows us to find a control which improves the performance of the overall system, and this only by dealing with separate subsystems and considering the interconnections as uncertainties. The reduction of dimensionality and the fact that the computation is done in one iteration are the basic interests of this method. The latter is the one which makes the satisfaction approach different from the decomposition technique. The decomposition technique gets the overall optimum but this needs a second iterative level.

A single Heuristic can be implemented which has these advantages:

Consider the following discrete linear system:

$$x(t_{i+1}) = x(t_i) + h[A x(t_i) + Bm(t_i)]$$

with the t_i such that

$$t_0 = 0 < t_1 < t_2 < \dots < t_i < t_{i+1} < \dots < t_m = t_e$$

and

$$t_{i+1} - t_i = h$$

with h greater than 0

and the performance functional:

$$\phi = \phi [x(t_0), \dots, x(t_m), m(t_0) \dots m(t_m)].$$

We call $x(t_0)$ the vector $(x_1(t_0) \dots x_n(t_0))$

x_j the array $(x_j(t_0), x_j(t_1) \dots x_j(t_m))$

$m(t_0)$ the vector $(m_1(t_0) \dots m_n(t_0))$

m_j the array $(m_j(t_0), m_j(t_1) \dots m_j(t_m))$

We make the following assumptions:

-Assumption 1:

B is non singular.

So we can express $m(t_i)$ as a function of $x(t_i)$ and $x(t_{i+1})$

$$m(t_i) = B^{-1} \left[\frac{x(t_{i+1}) - x(t_i)}{h} - A x(t_i) \right]$$

If we replace $m(t_i)$ by its value in function of $x(t_i)$ and $x(t_{i+1})$ in the functional performance, we will get a functional:

$$\begin{aligned} \phi [x(t_0), \dots, x(t_m), m(t_0), \dots, m(t_m)] \\ = \phi' [x(t_0), \dots, x(t_m)] \\ = \phi'' [x_1, \dots, x_n]. \end{aligned}$$

-Assumption 2:

ϕ'' is a continuous, non negative function with respect to the x_j , and it has Frechet derivatives.

-Assumption 3:

$\phi'' [x_1, \dots, x_n]$ is convex and it takes its unique critical point in the interior of M.

-Assumption 4:

$$X \text{ is convex and } X = X_1 \oplus X_2 \oplus \dots \oplus X_n$$

with X = set of the arrays of vectors $(x(t_0), \dots, x(t_m))$

$$X_1 = \text{set of the arrays: } (x_1(t_0), \dots, x_1(t_m))$$

$$X_2 = \text{set of the arrays: } (x_2(t_0), \dots, x_2(t_m))$$

⋮

$$X_n = \text{set of the arrays: } (x_n(t_0), \dots, x_n(t_m)).$$

-Assumption 5:

$$\forall j, \forall x_1^0, \dots, x_{j-1}^0, x_{j+1}^0, \dots, x_n^0,$$

if

$$\min_{x_j \in X_j} \phi [x_1^0, \dots, x_{j-1}^0, x_j, x_{j+1}^0, \dots, x_n^0] =$$

$$\phi [x_1^0, \dots, x_{j-1}^0, x_j^0, x_{j+1}^0, \dots, x_n^0],$$

then

$$x_j^0 \in \text{Int}(x_j).$$

With these assumptions, the procedure is the following:

Given a reference control m_1^r, \dots, m_n^r and the corresponding trajectories x_1^r, \dots, x_n^r and performance $\phi''(x_1^r, \dots, x_n^r)$

Step 1:

We consider the function

$$f_1(x_1) = \phi''(x_1, x_2^r, \dots, x_n^r)$$

By assumption 2, $f_1(x_1)$ is a continuous function of x_1 .

By assumption 4, if

$$x_1 \in X_1, (x_1, x_2^r, \dots, x_n^r) \in X.$$

So we can compute x_1^i such that:

$$\min_{x_1 \in X_1} f_1(x_1) = f_1(x_1^i)$$

By assumption 4, we know that $(x_1^i, x_2^r, \dots, x_n^r) \in X$.

Further, by assumption 5, we can say that $(x_1^i, x_2^r, \dots, x_n^r)$ is not a boundary point of X . So we can say:

$$\phi''(x_1^i, x_2^r, \dots, x_n^r) < \phi''(x_1^r, x_2^r, \dots, x_n^r) \quad \text{if } x_1^i \neq x_1^r$$

or

$$\frac{\partial \phi''(x_1^i, \dots, x_n^r)}{\partial x_1} = 0 \quad \text{if } x_1^i = x_1^r$$

We are using too assumption 2 (ϕ'' has derivatives).

Step 2:

We consider now the function:

$$f_2(x_2) = \phi''(x_1^i, x_2, x_3^r, \dots, x_n^r)$$

In the same way $f_2(x_2)$ is a continuous function of x_2 and

$$x_2 \in X_2 \rightarrow (x_1^i, x_2, x_3^r, \dots, x_n^r) \in X.$$

We compute x_2^i such that:

$$\min_{x_2 \in X_2} f_2(x_2) = f_2(x_2^i)$$

We can say again that: $(x_1^i, x_2^i, x_3^r, \dots, x_n^r) \in X$

and that: $(x_1^i, x_2^i, x_3^r, \dots, x_n^r) \in \text{Int } X$

$$\begin{aligned} \phi''(x_1^i, x_2^i, x_3^r, \dots, x_n^r) &< \phi''(x_1^i, x_2^r, x_3^r, \dots, x_n^r) \\ &\text{if } x_2^i \neq x_2^r. \end{aligned}$$

or

$$\frac{\partial \phi''}{\partial x_2}(x_1^i, x_2^i, x_3^r, \dots, x_n^r) = 0 \quad \text{if } x_2^i = x_2^r.$$

We compute n steps in the same way. We have n problems of optimal control, each of which is only one dimensional.

At the n^{th} step we have:

either

$$\left\{ \phi'' [x_1^i, \dots, x_n^i] < \phi'' [x_1^r, \dots, x_n^r] \right.$$

with $(x_1', \dots, x_n') \in X$ and $(x_1', \dots, x_n') \in \text{Int } X$.

or

$$\left\{ \begin{aligned} \frac{\partial \phi''(x_1' \dots x_n')}{\partial x_1} &= \frac{\partial \phi''(x_1' \dots x_n')}{\partial x_2} = \\ &\dots = \frac{\partial \phi''(x_1' \dots x_n')}{\partial x_n} = 0 \end{aligned} \right.$$

if $x_1' = x_1^r$ & $x_2' = x_2^r$ & \dots & $x_n' = x_n^r$

In the first case we improve the performance.

In the second, we got the same point but we know that the reference control is a local minimum, and hence, by assumption 3, the optimal control.

Iteration of the technique:

At the end of the procedure we improve the performance or we are at the optimum. If we are not at the optimum and if we iterate the procedure we will get

$$0 \leq \dots < \phi''(x_1^k, x_2^k, \dots, x_n^k) < \phi''(x_1^{k-1}, x_2^{k-1}, \dots, x_n^{k-1}) < \dots < \phi''(x_1^r, \dots, x_n^r).$$

So the iteration will give a sequence of performance functionals. This sequence is monotone decreasing, and has a lower bound (assumption 4). So this sequence is convergent. To compute the limit $\phi(x_1, \dots, x_n)$ we have to write:

$$\phi''(x_1^k, \dots, x_n^k) = \phi''(x_1^{k-1}, \dots, x_n^{k-1}) = \phi''(x_1^\ell, \dots, x_n^\ell).$$

But by assumption 5, this equality means that:

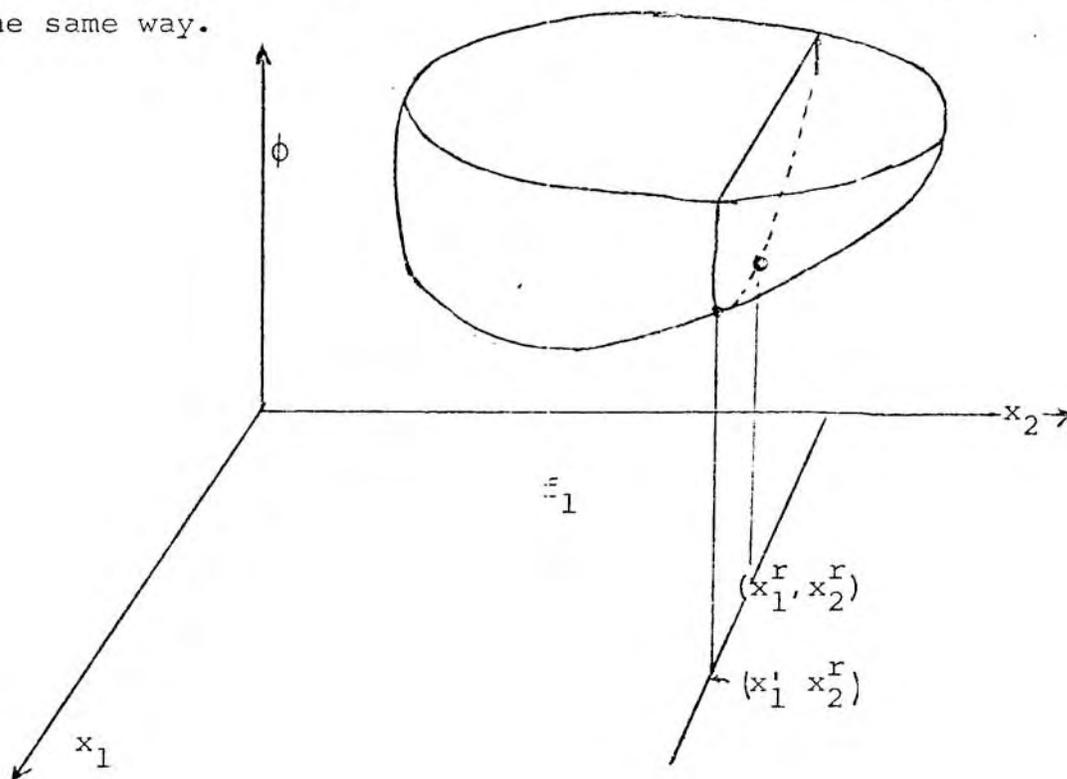
$$\rightarrow (x_1^k, \dots, x_n^k) = (x_1^{k-1}, \dots, x_n^{k-1}) = (x_1^\ell, \dots, x_n^\ell)$$

which means, by the preceding demonstration that:

$$(x_1^\ell, \dots, x_n^\ell)$$

is the global minimum of the performance functional.

The geometrical interpretation of this iterative heuristic is very simple. Consider the curve $f_1(x_1)$ section of the surface $z = \phi''(x_1, \dots, x_n)$ by the curves $x_2 = x_2^r, \dots, x_n = x_n^r$. Then consider on this curve the minimum of ϕ'' call it x_1' , and proceed again with x_2 in the same way.



The decomposition technique will proceed as follows:

$$x_1 = s_1, \dots, x_n = s_n$$

1st level:

$$\left. \begin{array}{l} \text{1^{st} \\ \text{sub} \\ \text{system} \end{array} \right\} \begin{cases} \frac{x_1(t_{i+1}) - x_1(t_i)}{h} = c_{11} x_1(t_i) + c_{12} s_2(t_i) + \\ \dots + c_{1n} s_n(t_i) + B_{11} m_1(t_i) \\ \\ \min_{m_1, s_2, \dots, s_n} \phi_1''[x_1, s_2, \dots, s_n, K_1, \dots, K_n] = \phi_1''^0 \end{cases}}$$

⋮

$$\left. \begin{array}{l} \text{n^{th} \\ \text{sub} \\ \text{system} \end{array} \right\} \begin{cases} \frac{x_n(t_{i+1}) - x_n(t_i)}{h} = c_{n1} s_n(t_i) + \dots + c_{nn} x_n(t_i) \\ \\ \dots + B_{nn} m_n(t_i) \\ \\ \min_{m_n, s_1, \dots, s_{n-1}} \phi_n''[s_1, \dots, s_{n-1}, x_n, K_1, \dots, K_n] = \phi_n''^0 \end{cases}}$$

2nd level:

$$\text{maximize}_{K_1, \dots, K_n} \varphi = \phi_1''^0 + \phi_2''^0 + \dots + \phi_n''^0 = \varphi^0$$

Once the min-max problem is solved (by a multilevel iteration procedure) we get:

$$\varphi^0 = \phi''^0 \text{ and } x_1 = s_1, x_2 = s_2, \dots, x_n = s_n.$$

- 1) For each subsystem the minimization of the performance is to be computed with respect to one variable, instead of $(n+1)$ in the decomposition technique.
- 2) We do not have a 2nd level but an iteration technique, which means an easier programming.
- 3) On the whole, the effectiveness of this heuristic is dependent upon the form of the performance. This heuristic can give the optimal point in one iteration, while with some other surfaces the convergence might be very slow.

$$L = \begin{bmatrix} -2A_1 & 0 \\ 0 & -2A_2 \end{bmatrix} \quad w_2 = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

The program of the computation is shown in Appendix 4, Program 2.

Use of the Heuristic:

We start with a reference control m_1^r, m_2^r . We compute the corresponding trajectory x_1^r, x_2^r by:

$$\frac{x_1^r(t_{i+1}) - x_1^r(t_i)}{h} = c_{11} x_1^r(t_i) + c_{12} x_2^r(t_i) + m_1^r(t_i)$$

$$\frac{x_2^r(t_{i+1}) - x_2^r(t_i)}{h} = c_{21} x_1^r(t_i) + c_{22} x_2^r(t_i) + m_2^r(t_i)$$

Then we have:

1st subsystem:

$$\left\{ \begin{array}{l} \min_{x_1=x_1^r} \phi(x_1, x_2^r) = \sum_{i=0}^m \{A_1 [x_1(t_i) - r_1]^2 + A_2 [x_2^r(t_i) - r_2]^2 \\ \quad + B_1 m_1^2(t_i) + B_2 m_2^2(t_i)\}. \\ \\ \text{with} \\ \left\{ \begin{array}{l} m_1(t_i) = \frac{x_1(t_{i+1}) - x_1(t_i)}{h} - c_{11} x_1(t_i) - \\ \quad c_{12} x_2^r(t_i) \\ \\ m_2(t_i) = \frac{x_2^r(t_{i+1}) - x_2^r(t_i)}{h} - c_{21} x_1(t_i) - \\ \quad c_{22} x_2^r(t_i) \end{array} \right. \end{array} \right.$$

3.3 Application of the Heuristic to Slightly Non-Linear

Systems:

By slightly non linear system, we mean the following system:

$$\left\{ \begin{array}{l} \frac{x_1(t_{i+1}) - x_1(t_i)}{h} = c_{11} x_1(t_i) + c_{12} x_2(t_i) \\ \quad + D_{11} x_1^2(t_i) + D_{12} x_2^2(t_i) + m_1(t_i) \\ \\ \frac{x_2(t_{i+1}) - x_2(t_i)}{h} = c_{21} x_1(t_i) + c_{22} x_2(t_i) \\ \quad + D_{21} x_1^2(t_i) + D_{22} x_2^2(t_i) + m_2(t_i) \end{array} \right.$$

performance:

$$\phi = \sum_{i=0}^m \{A_1 [x_1(t_i) - r_1]^2 + A_2 [x_2(t_i) - r_2]^2 + B_1 m_1^2(t_i) + B_2 m_2^2(t_i)\} \cdot h$$

The advantage of the heuristic is obvious from the following example. The computation of the coefficients in a successive sweep method for the overall problem is very complex, while, it is simple to do, with this heuristic:

subsystem 1:

$$\min_{x_1=x_1^r} \phi(x_1, x_2^r) = \sum_{i=0}^m \{A_1 [x_1(t_i) - r_1]^2 + A_2 [x_2^r(t_i) - r_2]^2 + B_1 m_1^2(t_i) + B_2 m_2^2(t_i)\} \cdot h$$

with

$$\left\{ \begin{aligned} \frac{x_1(t_{i+1}) - x_1(t_i)}{h} &= c_{11} x_1(t_i) + c_{12} x_2^r(t_i) \\ &+ D_{11} x_1^2(t_i) + D_{12} (x_2^r(t_i))^2 \\ &+ m_1(t_i) \\ \frac{x_2^r(t_{i+1}) - x_2^r(t_i)}{h} &= c_{21} x_1(t_i) + c_{22} x_2^r(t_i) \\ &+ D_{21} x_1^2(t_i) + D_{22} (x_2^r(t_i))^2 \\ &+ m_2(t_i) \end{aligned} \right.$$

subsystem 2:

Given x_1^i from the subsystem 1:

$$\min_{x_2 = x_2^i} \phi(x_1^i, x_2) = \sum_{i=0}^m \{A_1 [x_1^i(t_i) - r_1]^2 + A_2 [x_2(t_i) - r_2]^2 + B_1 m_1^2(t_i) + B_2 m_2^2(t_i)\} \cdot h$$

with

$$\left\{ \begin{aligned} \frac{x_1^i(t_{i+1}) - x_1^i(t_i)}{h} &= c_{11} x_1^i(t_i) + c_{12} x_2(t_i) \\ &+ D_{11} (x_1^i(t_i))^2 + D_{12} x_2^2(t_i) \\ &+ m_1(t_i) \\ \frac{x_2(t_{i+1}) - x_2(t_i)}{h} &= c_{21} x_1^i(t_i) + c_{22} x_2(t_i) \\ &+ D_{21} (x_1^i(t_i))^2 + D_{22} x_2^2(t_i) \\ &+ m_2(t_i) \end{aligned} \right.$$

We then have $\phi (x'_1, x'_2) < \phi (x_1^r, x_2^r)$

or $\left. \begin{array}{l} x'_1 = x_1^r \\ x'_2 = x_2^r \end{array} \right\}$ and the reference control
is a local minimum.

Application: Appendix 4, Program 4.

USE OF THE THEORY OF CHAPTER III
WITHOUT ITERATION

LINEAR SYSTEM

Initial Performance	Performance after Iteration
41.667	→ 59.566
71.172	→ 39.865
22.10	→ 22.56
Optimal Performance	39.566

NON LINEAR SYSTEM

Initial Performance	Performance after Iteration
115.56	→ 112.62
115.36	→ 112.54
122.61	→ 115.36
179.14	→ 141.26
2165.5	→ 134.60
45.34	→ 155.22
Optimal Performance	112.52

system

$$\begin{cases} 2x_1 + 3x_2 + x_3 = 200 \\ x_1 + x_2 + 2x_3 = 100 \\ x_1, x_2, x_3 \geq 0 \end{cases}$$

Performance

$$Z = 100x_1 + 150x_2 + 200x_3$$

$Z = 0.11$

system

$$\begin{cases} 2x_1 + 3x_2 + x_3 = 200 \\ x_1 + x_2 + 2x_3 = 100 \\ x_1, x_2, x_3 \geq 0 \end{cases}$$

Performance

$$Z = 100x_1 + 150x_2 + 200x_3$$

3.4 Application of the Heuristic to a Linear System

with 5 Variables. Computational Study of the Heuristic:

The system is the most general one:

$$\frac{x_i(t_{k+1}) - x_i(t_k)}{h} = \sum_{j=1}^5 c_{ij} x_j(t_k) + m_i(t_k)$$

$$i = 1, 2, 3, 4, 5.$$

$$\phi = \sum_{k=0}^m \sum_{j=1}^5 [A_j (x_j(t_k) - r_j)^2 + B_j m_j^2(t_k)] \cdot h$$

The computation at the N^{th} stage, j^{th} step is the following one:

$$\frac{x_j^{(N)}(t_{k+1}) - x_j^{(N)}(t_k)}{h} = \sum_{1 \leq i \leq j} c_{ji} x_i^{(N)}(t_k)$$

$$+ \sum_{j < k \leq 5} c_{jk} x_k^{(N-1)}(t_k)$$

$$+ m_j^{(N)}(t_k)$$

$$\min_{x_j^{(N)}} \phi_j^{(N)} = \sum_{i=0}^m \{ \sum_{1 \leq i \leq j} [A_i (x_i^{(N)}(t_k) - r_i)^2$$

$$+ B_i m_i^{(N)2}(t_k)]$$

$$+ \sum_{j < \ell \leq 5} [A_\ell (x_\ell^{(N-1)}(t_k) - r_\ell)^2$$

$$+ B_\ell m_\ell^{(N-1)2}(t_k)] \}. h$$

Program of computation: See Appendix 4, Program 5.

Performance with the reference control	Performance after application of the satisfaction approach	Application of the heuristic and iteration					
		Number of iterations	step 1	step 2	step 3	step 4	step 5
31.891	31.879	1	31.891	31.888	31.887	31.887	31.887
		2	31.879	31.879	31.875	31.875	31.875
38.791	32.791	1	36.792	34.815	33.879	32.796	31.894
		2	31.896	31.881	31.880	31.879	31.879
		3	31.879	31.879	31.879	---	---
731.29	33.67	1	531.36	351.79	255.68	164.42	32.865
		2	32674	32.356	32.285	31.885	31.881
		3	31.879	31.879	31.879	31.879	31.879

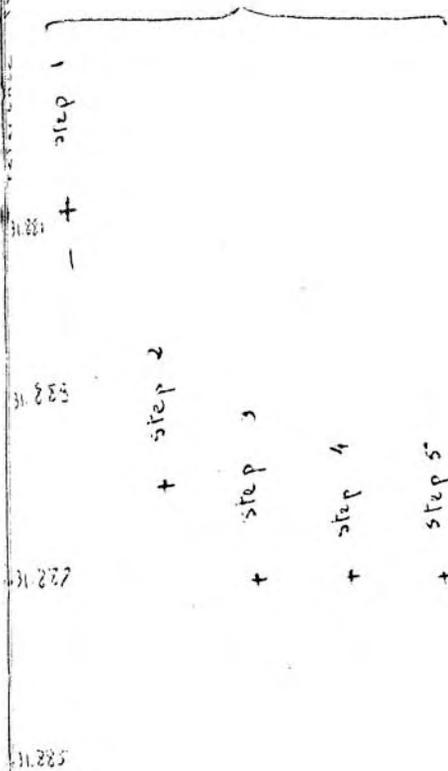
Maximum value of $|H_m|$ or $|L_m|$ when the heuristic is applied and iterated.

Iteration No	step No	$ H_{m1} $	$ H_{m2} $	$ H_{m3} $	$ H_{m4} $	$ H_{m5} $
1	1	8.175	4.00	199.5	199.4	211.35
	2	5.80	17.3	199.65	199.9	225.0
	3	5.80	12.8	5.00	192.7	229.7
	4	14.58	17.66	4.77	12.93	232.60
	5	14.955	17.60	5.19	11.05	0.004
2	1	$7.06 \cdot 10^{-3}$	11.24	3.64	12.91	0.127
	2	0.166	$6.2 \cdot 10^{-2}$	5.18	12.94	0.570
	3	0.166	0.119	0.00422	12.92	0.660
	4	1.168	1.35	0.0337	0.120	1.463
	5	1.026	1.35	0.0322	0.120	0.00020
3	1	0.00042	1.35	0.0322	0.120	0.0173
	2	0.0057	0.00209	0.0328	0.120	0.0375
	3	0.0057	0.00231	0.00145	0.120	0.0262
	4	0.00652	0.0217	0.00191	0.00164	0.0283
	5	0.00551	0.0217	0.00191	0.00164	0.000012
4	1	0.000386	0.0217	0.00191	0.00164	0.000120
	2	0.000593	0.0015	0.00191	0.00170	0.000525
	3	0.00060	0.00159	0.000244	0.00171	0.000637
	4	0.000663	0.00161	0.000244	0.00235	0.000673
	5	0.000662	0.00161	0.000243	0.00237	0.000030
5	1	0.000321	0.00161	0.000244	0.00237	0.00061
	2	0.000471	0.00155	0.000244	0.00237	0.000061
	3	0.000662	0.00161	0.000262	0.00237	0.000061
	4	0.000635	0.00161	0.000263	0.00240	0.000057
	5	0.000665	0.00161	0.000263	0.00241	0.000030

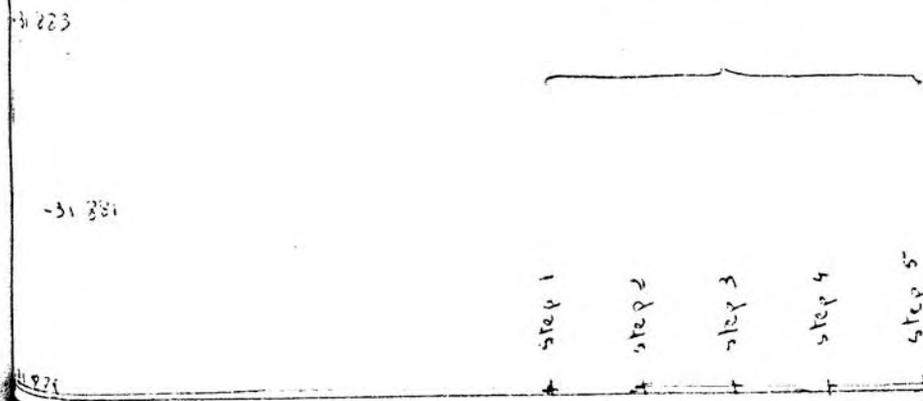
Evolution of the Performance Versus
the number of iterations

Performance

1st ~~and unique~~ iteration



2nd iteration



optimal performance

Evolution of the Performance Versus
the number of iterations

performance →

reference performance

1st iteration

2nd iteration

+ step 1

+ step 2

+ step 3

+ step 4

+ step 5

+ step 1

+ step 2

+ step 3

+ step 4

+ step 5

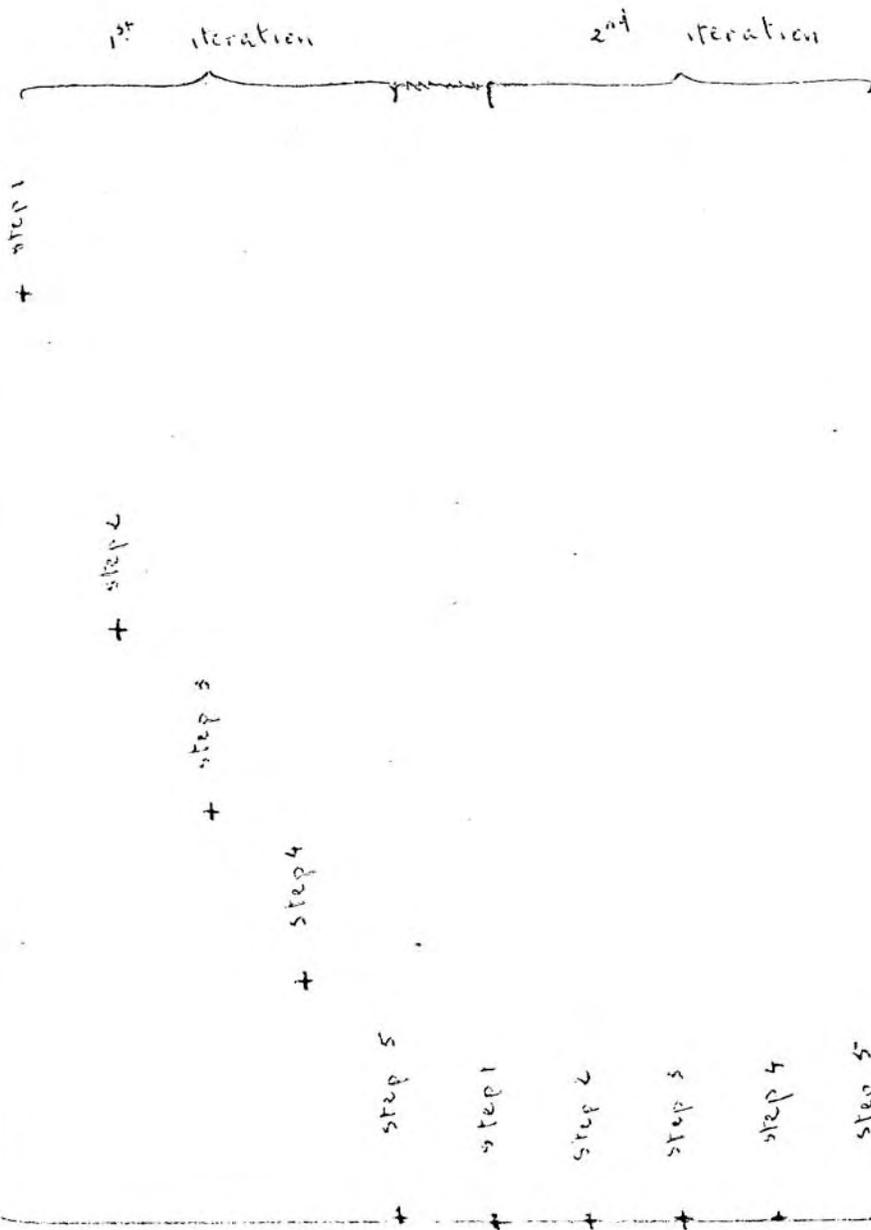
optimal performance

no. of iterat

performances

Evolution of the performance versus
the number of iterations

reference performance



optimal performance

number of iterations

If, for the same system, we vary h/t_e from 0.1 to 0.01, we can see that:

-The computing time is proportional to the number of intervals in which $[t_0, t_e]$ is divided, or proportional to $1/(h/t_e)$.

-After 5 iterations, we get almost the same performance.

-When h decreases, we get a smoother curve of the control.

-The difference of the trajectories computed with different h/t_e can be neglected. The difference in the controls are more important; but this puts in evidence two facts: For this system, a small variation in the controls will not affect too much the trajectories, and the cost of the control is very little compared to the cost of the deviation from the desired trajectory.

Computing Time

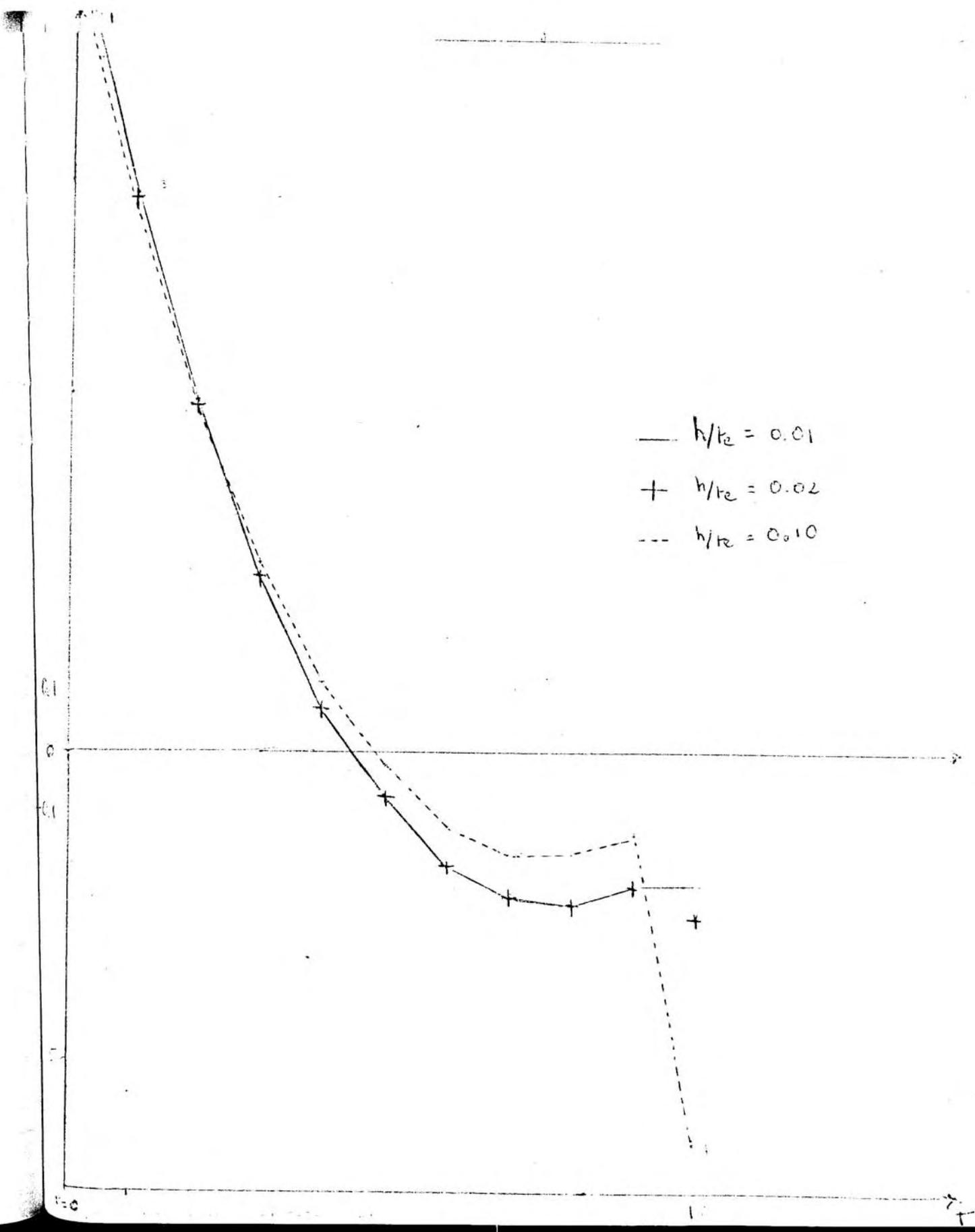
Variation of the computing time
with respect to the steps of integration.



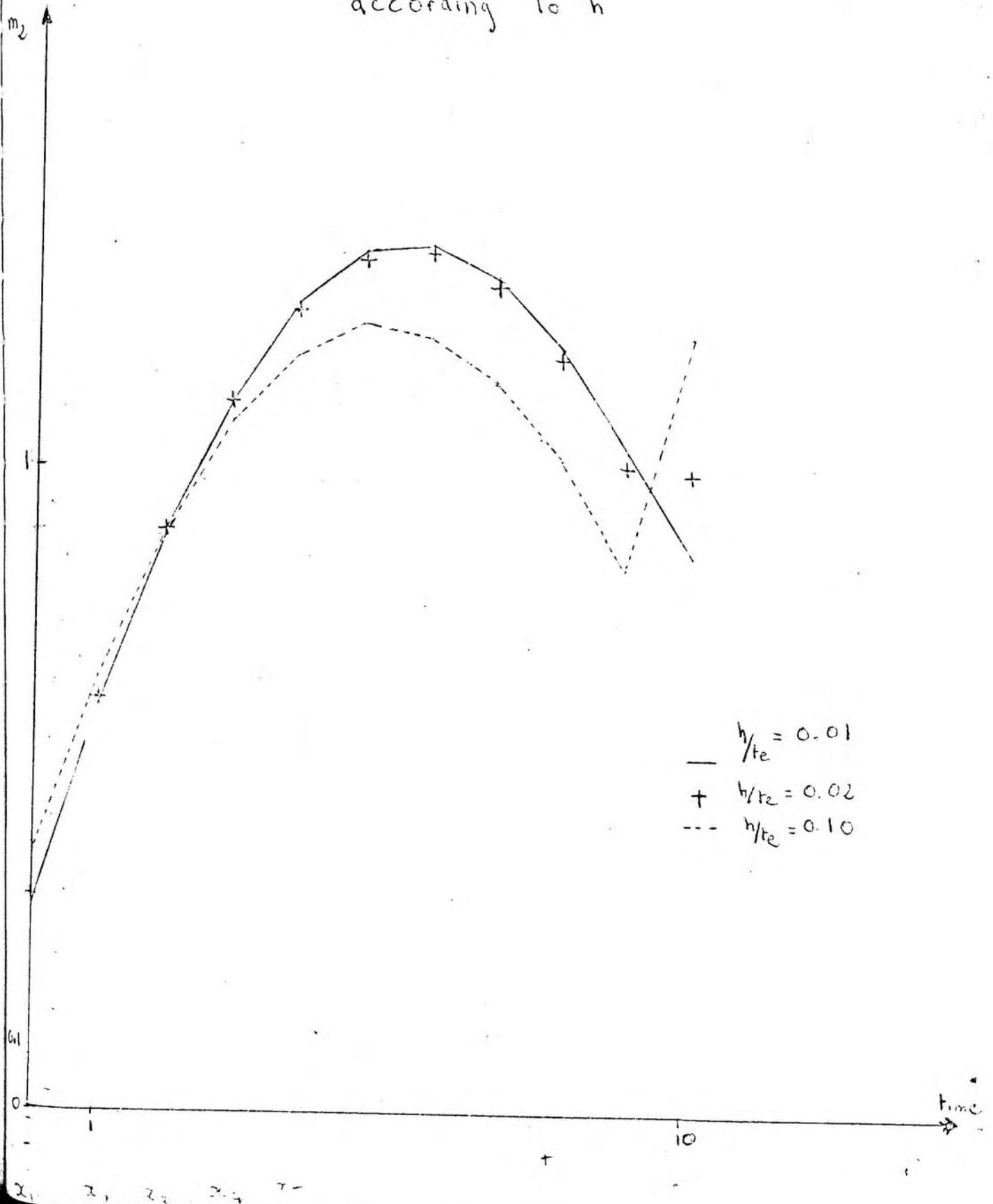
Number of
intervals on
 $\frac{b-a}{n}$

Variation of the evolution of the Performance index
with respect to the step of integration, h

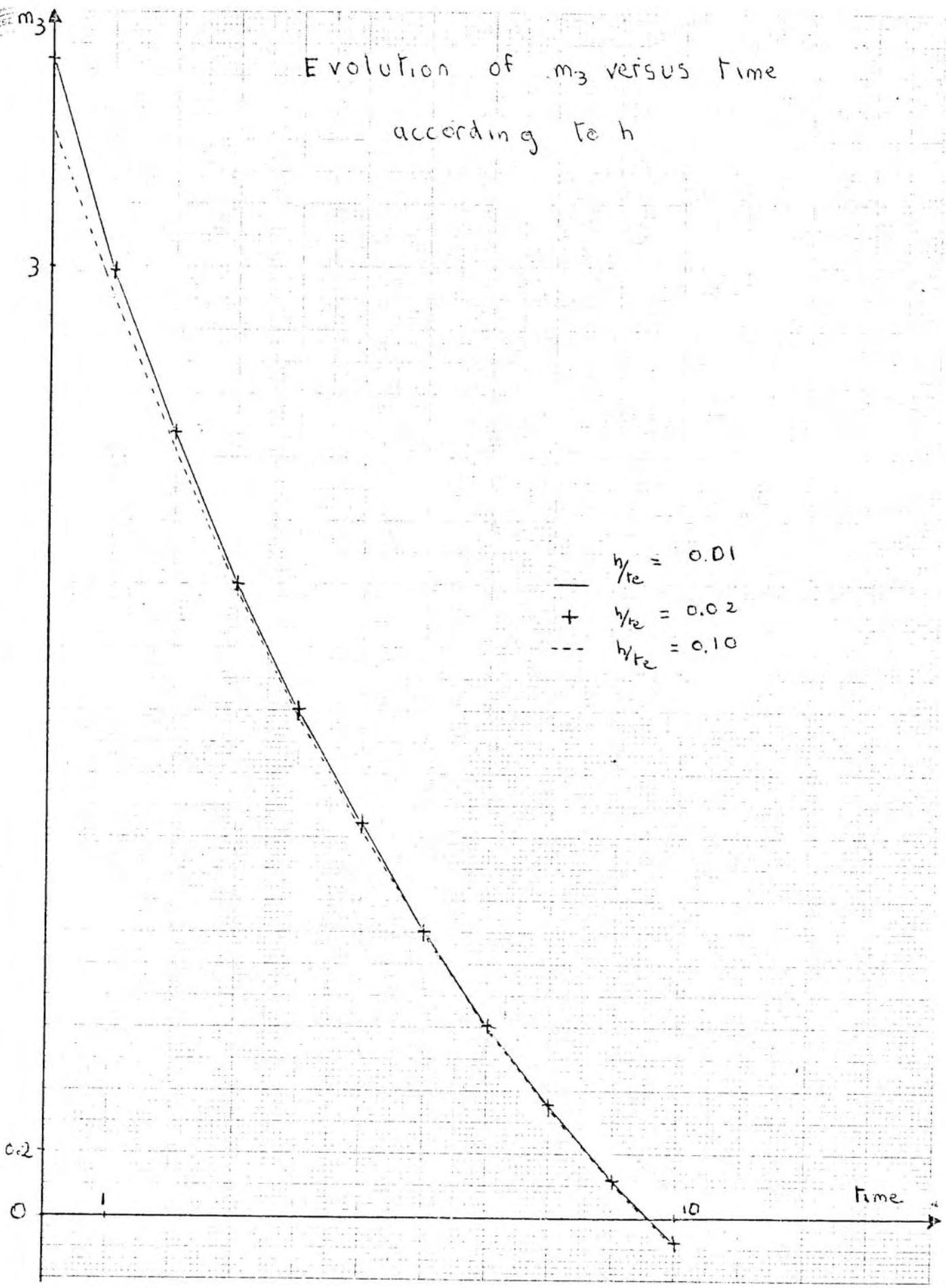
h _{te}	0.1	0.05	0.033	0.02	0.016	0.012	0.01
aver of [D,T]	10	20	30	50	60	80	100
Step No.							
1	7373.1	12087	17263	27886	33241	43986	54753
2	6225.4	8409.2	12677	19367	23541	30709	37889
3	5939.1	9266.6	12778	19908	23490	30663	37856
4	5614.7	8998.2	12660	19830	23420	30613	37867
5	744.63	664.66	641.16	623.28	618.93	613.55	610.35
1	434.88	444.91	438.06	408.35	407.26	405.90	405.09
2	380.89	361.25	355.42	351.02	349.96	348.66	347.88
3	371.82	355.38	350.52	346.80	345.91	344.82	344.18
4	342.38	337.69	337.14	336.79	336.77	336.76	336.74
5	338.90	337.20	336.92	336.77	336.74	336.71	336.70
1	326.39	325.76	325.92	325.75	325.76	325.98	325.79
2	324.94	324.90	325.00	325.11	325.14	325.18	325.20
3	324.78	324.88	325.00	325.11	325.13	325.17	325.20
4	322.85	321.96	322.12	321.93	322.	321.93	321.94
5	321.55	321.63	321.68	321.71	321.72	321.73	321.74
1	320.33	320.26	320.26	320.27	320.27	320.27	320.28
2	318.84	318.93	318.97	319.01	319.02	319.03	319.04
3	318.77	318.89	318.94	318.98	318.99	319.00	319.01
4	318.00	317.96	318.03	318.02	318.02	317.95	318.02
5	317.86	317.79	317.77	317.75	317.74	317.73	317.73
1	317.73	317.62	317.58	317.55	317.55	317.54	317.53
2	317.16	317.04	317.00	316.97	316.96	316.95	316.95
3	317.15	317.02	316.98	316.95	316.94	316.93	316.92
4	316.97	316.80	316.77	316.73	316.72	316.70	316.70
5	316.96	316.75	316.68	316.63	316.61	316.59	316.58

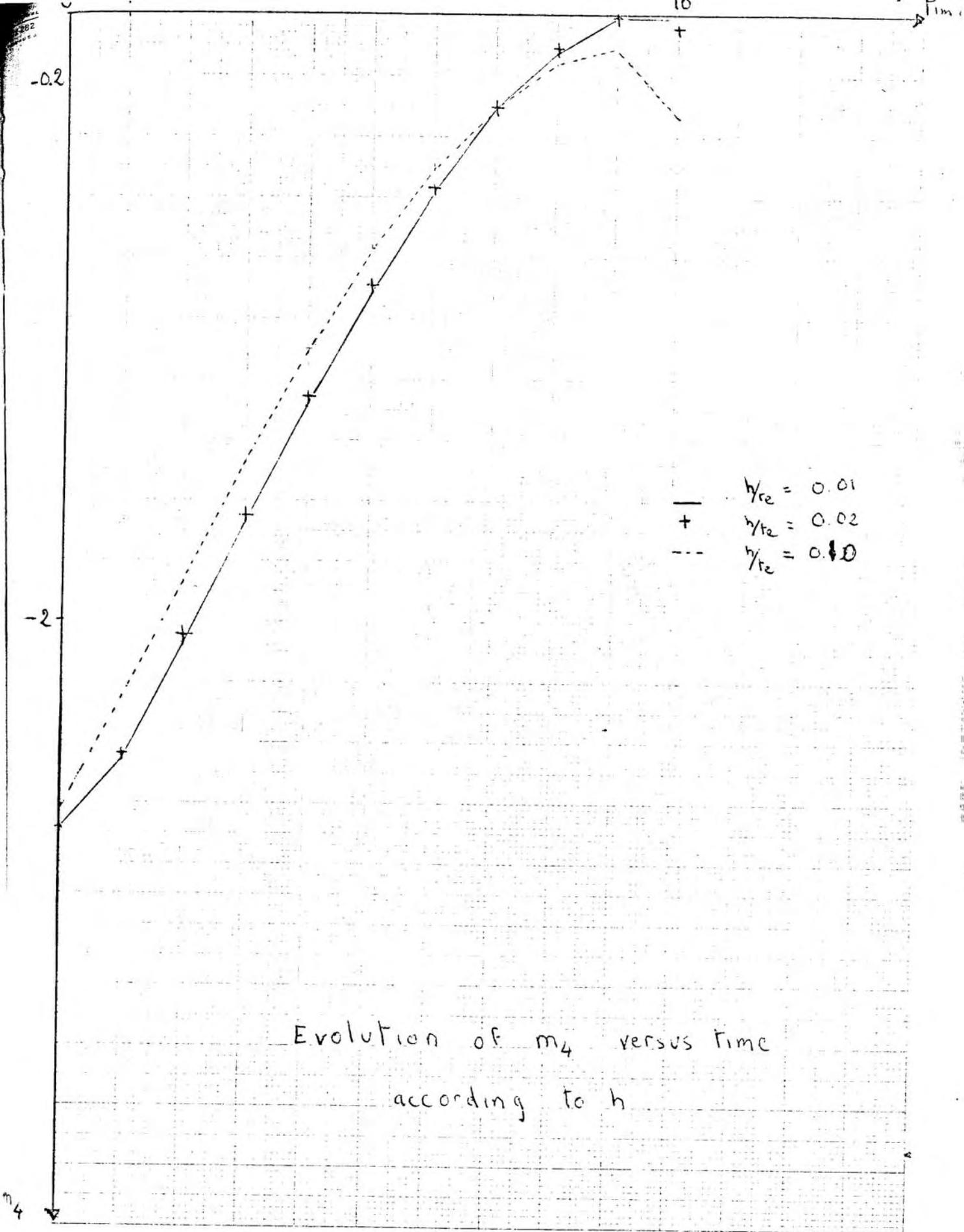


Evolution of m_2 versus time
according to h

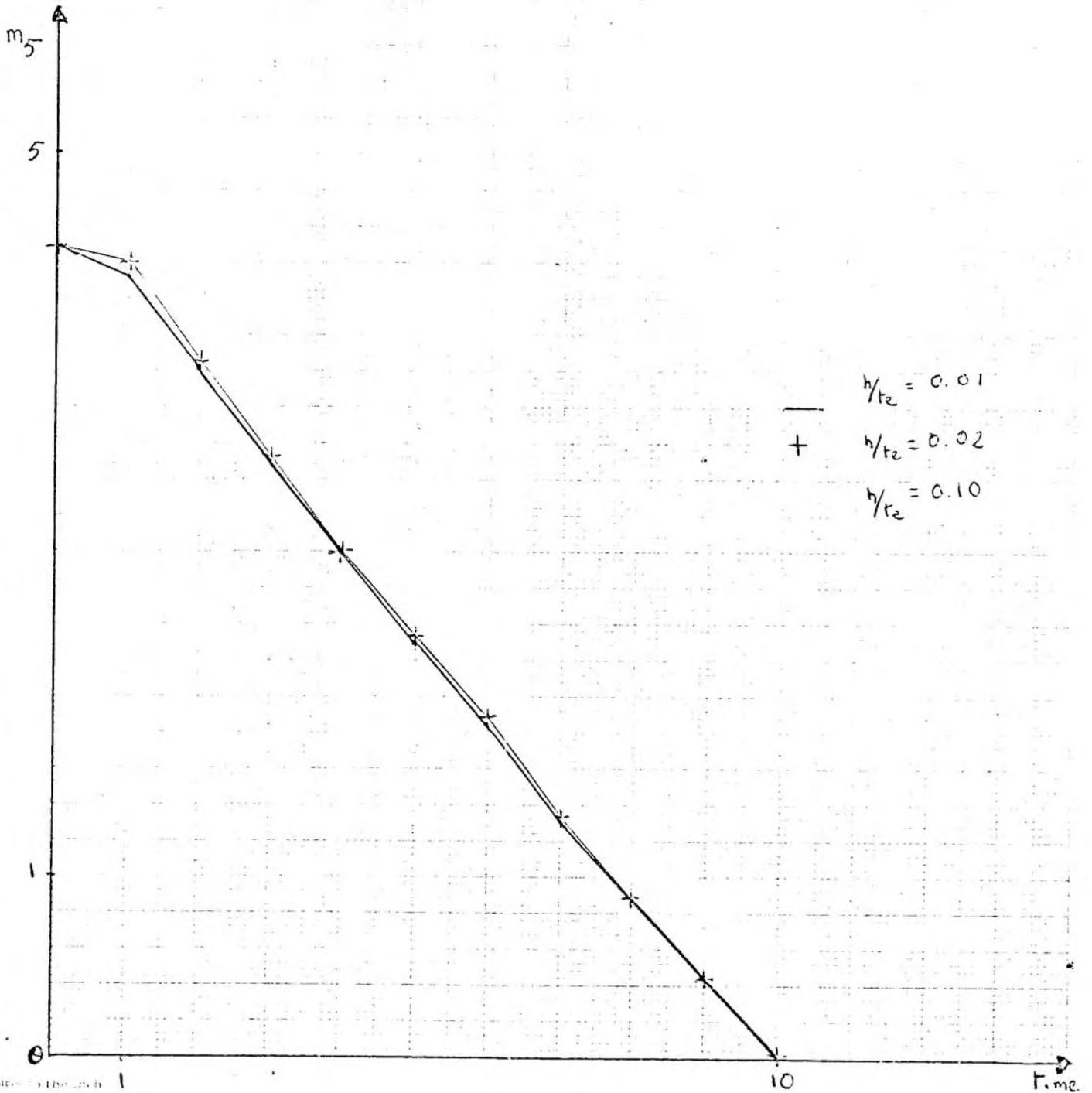


Evolution of m_3 versus time
according to h





Evolution of m_5 versus time
according to h



Difference in % of the solutions with various h compared to the solution with $h=0.01$

F_0

h/te	m_1	m_2	m_3	m_4	m_5	x_1	x_2	x_3	x_4	x_5
0.1	4	27	3.2	6.7	1.2	0	0	0	0	0
0.05	2.3	15	1.5	2.5	0.5	0	0	0	0	0
0.033	1.5	9.6	0.5	1.4	0.3	0	0	0	0	0
0.02	0.7	4.3	0.4	0.6	0.1	0	0	0	0	0
0.016	0.46	3	0.3	0.4	0.08	0	0	0	0	0
0.012	0.23	1.2	0.1	0.14	0.02	0	0	0	0	0

} h

F_5

h/te	m_1	m_2	m_3	m_4	m_5	x_1	x_2	x_3	x_4	x_5
0.1	65	8.2	1.7	15	1.1	0.08	0.06	0.45	2.8	0.8
0.05	15	2.5	0.8	7.5	0.47	0.05	0	0.21	1.6	0.35
0.033	6	1.2	0.5	4.9	0.3	0.03	0	0.12	0.7	0.2
0.02	1.7	0.45	0.2	2.2	0.13	0.01	0	0.04	0.3	0.08
0.016	1	0.3	0.16	1.5	0.086	0.008	0	0.03	0.2	0.05
0.012	0.25	0.07	0.06	0.6	0.04	0	0	0.01	0.08	0

F_{10}

h/te	m_1	m_2	m_3	m_4	m_5	x_1	x_2	x_3	x_4	x_5
0.1	200	51	0.1	1530	0	0.3	0	0.5	3.2	0.2
0.05	98	21	0.4	550	0	0.1	0	0.2	1.25	0
0.033	55	13	0.3	310	0	0	0	0.1	0.675	0
0.02	26	6	0.1	118	0	0	0	0	0.25	0
0.016	17	4	0.1	77	0	0	0	0	0	0
0.012	6	1.5	0.03	28	0	0	0	0	0	0

CHAPTER IV
DECOMPOSITION TECHNIQUE APPLIED
IN PRESENCE OF NOISE

The decomposition technique cannot be applied directly to a system with disturbances, for the noises in the measurements introduce a new kind of correlation between the subsystems. If we consider one subsystem and the measurements related only to this subsystem we are neglecting in this subsystem the information brought by the data of the other subsystems. Hence, the computed control would not be the optimal control computed with all the data given by the measurements.

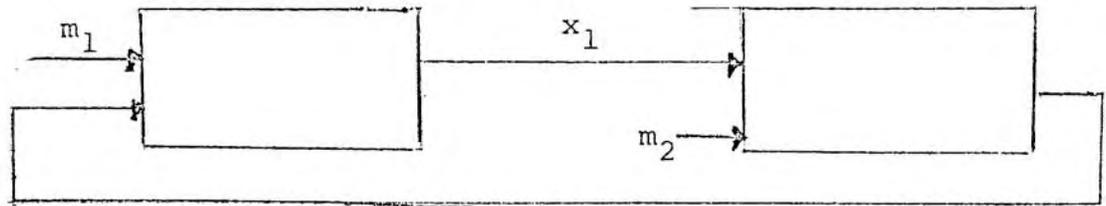
Nevertheless, in terms of the means and the variances of the state variables, it is possible to use this technique once deterministic equations of the global system are found. We then consider these equations as defining a new system, the state variables of which are the means and the variances of the previous state variables. The examples will show how this can be implemented.

4.1 Case of Linear System with Quadratic Performances

4.1.1 The Deterministic Problem

Part 1 The global method:

The system is the following one:



$$\begin{bmatrix} dx_1 \\ dx_2 \end{bmatrix} = \begin{bmatrix} c_{11} & c_{12} \\ c_{21} & c_{22} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} dt + \begin{bmatrix} l_1 & 0 \\ 0 & l_2 \end{bmatrix} \begin{bmatrix} m_1 \\ m_2 \end{bmatrix} dt$$

or

$$dx = (C + C') x dt + L m dt.$$

$$\text{with } C = \begin{bmatrix} c_{11} & 0 \\ 0 & c_{22} \end{bmatrix} \quad C' = \begin{bmatrix} 0 & c_{12} \\ c_{21} & 0 \end{bmatrix} \quad L = \begin{bmatrix} l_1 & 0 \\ 0 & l_2 \end{bmatrix}$$

The performance criterion is:

$$\begin{aligned} \phi[x, m] = \int_0^t e^{\{ (r-x)(r-x)^T + m m^T \}} dt &= \int_0^t e^{\{ (r_1 - x_1)^2 \\ &+ (r_2 - x_2)^2 + m_1^2 + m_2^2 \}} dt \end{aligned}$$

This problem corresponds to something real:

$\int_0^t e^{-\lambda t} (m_1^2 + m_2^2) dt$ corresponds to the cost of the control

action. $r_1(t), r_2(t)$ corresponds to the desired trajectories of $x_1(t), x_2(t)$. $\int_0^t e^{-\lambda t} \{(r_1-x_1)^2 + (r_2-x_2)^2\} dt$

is the cost of deviation from the desired output.

This problem is a classical problem of control which can be solved by well known techniques:

$$H = (r_1-x_1)^2 + (r_2-x_2)^2 + m_1^2 + m_2^2 + p_1[c_{11} x_1 + c_{12} x_2 + l_1 m_1] + p_2[c_{21} x_1 + c_{22} x_2 + l_2 m_2]$$

We have to solve the following T. P. B. V. P.:

$$\left\{ \begin{array}{l} \frac{dx_1}{dt} = c_{11} x_1 + c_{12} x_2 + l_1 m_1 \quad x_1(0) = x_{10} \\ \frac{dx_2}{dt} = c_{21} x_1 + c_{22} x_2 + l_2 m_2 \quad x_2(0) = x_{20} \\ \frac{dp_1}{dt} = -H_{x_1} \quad p_1(t_e) = 0 \\ \frac{dp_2}{dt} = -H_{x_2} \quad p_2(t_e) = 0 \\ H_{m_1} = 0 \quad H_{m_2} = 0 \end{array} \right.$$

-Computation of a numerical example:

-Data:

$$c_{11}(t) = c_{22}(t) = c_{21}(t) = l_1(t) = l_2(t) = 1$$

$$r_1(t) = t \quad r_2(t) = 2t \quad t_e = 0.05.$$

-Computation:

$$\mathcal{D} = \mathcal{D}' = \begin{bmatrix} 1 & 1 \\ 1 & 1 \end{bmatrix} \quad \mathcal{E} = \begin{bmatrix} -\frac{1}{2} & 0 \\ 0 & -\frac{1}{2} \end{bmatrix} \quad w_1 = \begin{bmatrix} \frac{1}{2} & \delta H m_1 \\ \frac{1}{2} & \delta H m_2 \end{bmatrix}$$

$$\mathcal{L} = \begin{bmatrix} -2 & 0 \\ 0 & -2 \end{bmatrix} \quad w_2 = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

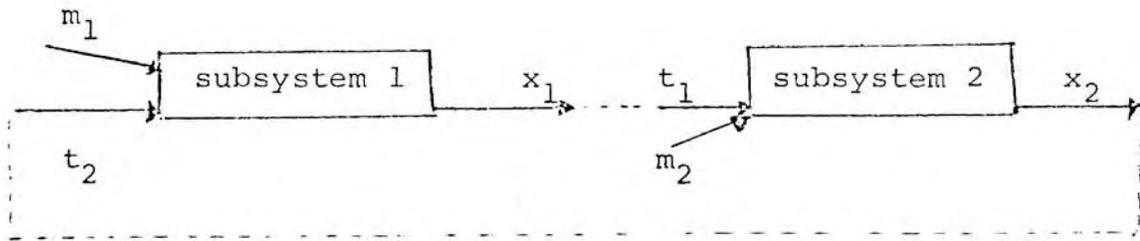
-Results: see Appendix 5, Program 6.

Part 2 The decomposition technique:

The system is decomposed in two subsystems (Appendix 2 and the thesis of S. Reich [3]). For this, the chosen system must have the two following fundamental properties:

- a) It can be split into two subsystems such that the output of one system can be viewed as an input to the other subsystem.
- b) The performance is additively separable.

In this case we have the following scheme:



We have:

subsystem 1:

$$\frac{dx_1}{dt} = c_{11} x_1 + c_{12} t_2 + \ell_1 m_1$$

subsystem 2:

$$\frac{dx_2}{dt} = c_{21} t_1 + c_{22} x_2 + \ell_2 m_2.$$

with the supplementary constraints: $x_2 = t_2$

$$x_1 = t_1$$

The Lagrangian for the whole system can be written as:

$$\begin{aligned} J = & (r_1 - x_1)^2 + (r_2 - x_2)^2 + m_1^2 + m_2^2 + p_1 [c_{11} x_1 + c_{12} t_2 \\ & + \ell_1 m_1 - \dot{x}_1] + p_2 [c_{21} t_1 + c_{22} x_2 + \ell_2 m_2 - \dot{x}_2] \\ & + k_1 (x_1 - t_1) + k_2 (x_2 - t_2). \end{aligned}$$

This Lagrangian can be split, due to the fact that the performance is additively separable. This leads to

the decomposition technique. It was shown [3] that the decomposition technique and the global method give the same results. The advantage of the decomposition technique is to break the problem in several subproblems easier to handle by the computer. In this case we have:

First Level

Given k_1, k_2 for the 2nd level we have the two

T. P. B. V. P.:

-subproblem 1:

$$J = (r_1 - x_1)^2 + m_1^2 + p_1 [c_{11} x_1 + c_{12} t_2 + l_1 m_1 - \dot{x}_1] + k_1 x_1 - k_2 t_2.$$

$$\left\{ \begin{array}{l} \frac{dx_1}{dt} = c_{11} x_1 + l_1 m_1 + c_{12} t_2 \quad x_1(0) = x_{10} \\ \frac{dp_1}{dt} = -Hx_1 = - \{ 2 (x_1 - r_1) + p_1 c_{11} + k_1 \} \quad p_1(t_e) = 0 \\ 2m_1 + p_1 l_1 = 0 \\ p_1 c_{12} - k_2 = 0 \end{array} \right.$$

-subproblem 2:

$$J = (r_2 - x_2)^2 + m_2^2 + p_2 [c_{21} t_1 + c_{22} x_2 + l_2 m_2 - \dot{x}_2] - k_1 t_1 + k_2 x_2.$$

$$\left\{ \begin{array}{l} \frac{dx_2}{dt} = c_{21} t_1 + c_{22} x_2 + l_2 m_2 \quad x_2(0) = x_{20} \\ \frac{dp_2}{dt} = -Hx_2 = -\{2(x_2 - r_2) + p_2 c_{22} + k_2\} p_2(t_e) = 0 \\ 2m_2 + p_2 l_2 = 0 \\ p_2 c_{21} - k_1 = 0 \end{array} \right.$$

Second Level or Coordination Level

The 2nd level coordinates the two subproblems by varying k_1 and k_2 .

$$[k_1]_{n+1} = [k_1]_n - \varepsilon (x_1 - t_1)$$

$$[k_2]_{n+1} = [k_2]_n - \varepsilon (x_2 - t_2)$$

The multilevel procedure consists in solving the first level and making one coordination step at the 2nd level. The procedure repeats until $|x_1 - t_1|$ and $|x_2 - t_2|$ are within a tolerance limit.

Computation of a numerical example:

-Data:

$$c_{11}(t) = c_{21}(t) = c_{22}(t) = l_1(t) = l_2(t) = 1$$

$$r_1(t) = t \quad r_2(t) = 2t \quad t_e = 0.05.$$

-Computation:

subsystem 1:

$$\mathcal{D} = \mathcal{D}' = 1 \quad \mathcal{E} = -\frac{3}{2} \quad w_1 = \frac{1}{2} \delta H m_1 + \delta H t_2$$

$$\mathcal{L} = -1 \quad w_2 = 0$$

subsystem 2:

$$\mathcal{D} = \mathcal{D}' = 1 \quad \mathcal{E} = -\frac{3}{2} \quad w_1 = \frac{1}{2} \delta H m_2 + \delta H t_1$$

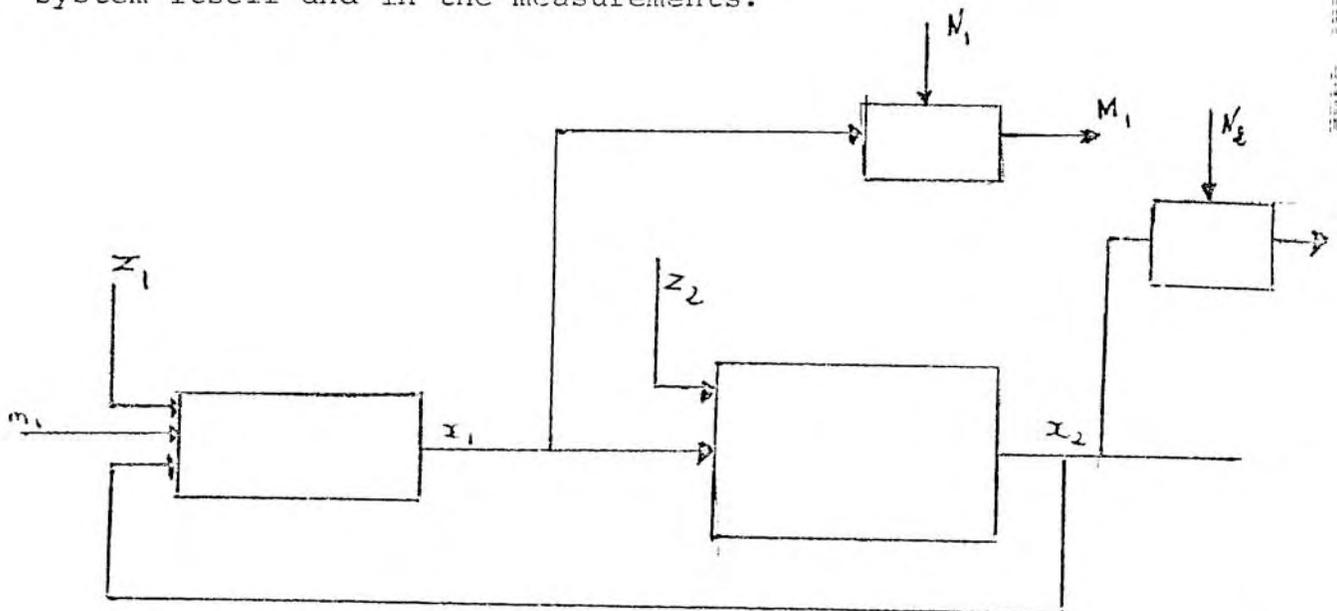
$$\mathcal{L} = -1 \quad w_2 = 0$$

-Results: see Appendix 5, Program 7.

4.1.2 The Stochastic Problem

A Formulation of the Problem:

We take the same system but with noises in the system itself and in the measurements.



The control actions are m_1 and m_2 .

-The system is:

$$\begin{bmatrix} dx_1 \\ dx_2 \end{bmatrix} = \begin{bmatrix} c_{11} & c_{12} \\ c_{21} & c_{22} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} dt + \begin{bmatrix} l_1 & 0 \\ 0 & l_2 \end{bmatrix} \begin{bmatrix} m_1 \\ m_2 \end{bmatrix} dt + \begin{bmatrix} dz_1 \\ dz_2 \end{bmatrix}$$

or

$$dx = (C + C') x dt + L m dt + dz.$$

The measurements are:

$$\begin{bmatrix} dM_1 \\ dM_2 \end{bmatrix} = \begin{bmatrix} g_1 & 0 \\ 0 & g_2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} dt + \begin{bmatrix} dN_1 \\ dN_2 \end{bmatrix}$$

or

$$dM = G x dt + dN$$

-Assumptions on the noises:

dN and dz are uncorrelated vector Wiener processes, such that:

For any $t \in T$ and any $s \neq t$:

$$E[dN(t)] = E[dz(t)] = 0 \quad E[dN(t) \cdot dz^T(t)] = 0$$

$$E[dN(t) \cdot dN^T(s)] = E[dN(t) \cdot dz^T(s)] = E[dz(t) \cdot dz^T(s)] = 0$$

$$E[dN(t) \cdot dN^T(t)] = W dt$$

$$E[dz(t) \cdot dz^T(t)] = Q dt$$

with

$$W = \begin{bmatrix} w_1 & 0 \\ 0 & w_2 \end{bmatrix} \quad Q = \begin{bmatrix} q_1 & 0 \\ 0 & q_2 \end{bmatrix}$$

-Notations:

$$\bar{x} = E(x) = \begin{bmatrix} \bar{x}_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} E(x_1) \\ E(x_2) \end{bmatrix}$$

$$V = E \{ (x - \bar{x}) \cdot (x - \bar{x})^T \} = \begin{bmatrix} v_{11} & v_{12} \\ v_{21} & v_{22} \end{bmatrix}$$

-Performance criterion:

We use the same performance criterion as in the deterministic case but with an expectation:

$$\begin{aligned} \phi &= E \left\{ \int_0^t e^{-\rho t} [(r_1 - x_1)^2 + (r_2 - x_2)^2 + m_1^2 + m_2^2] dt \right. \\ &= \int_0^t e^{-\rho t} \{ (m_1^2 + (r_1 - \bar{x}_1)^2 + v_{11}) + (m_2^2 + (r_2 - \bar{x}_2)^2 + v_{22}) \} dt \end{aligned}$$

B Solution of the global problem:

To solve the global problem we need to know an expression of \bar{x}_1 , v_1 , \bar{x}_2 , v_2 which are in the formulation of the performance criterion. To compute these values

we shall use the method of Kalman [4]. This method will be explained in detail in this section. In the following demonstrations only the main steps of the calculation will be written.

We will solve the problem first with the vectorial notation, which will give \bar{x} and V . Taking the elements of \bar{x} and V we will get $\bar{x}_1, v_1, \bar{x}_2, v_2$.

Prior mean and variance of : \bar{x} and V .

Posterior mean and variance of : $\underline{\bar{x}}$ and \underline{V} .

We approximate the continuous-time model by a finite time difference model:

$$\delta x = x(t + \delta t) - x(t) = (C + C') x \delta t + L m \delta t + \delta Z. \quad (1)$$

$$\delta M = M(t + \delta t) - M(t) = G x \delta t + \delta N. \quad (2)$$

Now we proceed in two stages: the first stage is the determination of the conditional probability density of δx just after an observation δM during the time δt , in terms of the conditional probability density of δx just before the observation δM . These conditional probabilities are known respectively as posterior and prior. In the second stage the effect of the dynamics of the process are taken in account and determine the transformation between the prior conditional probability density at time $t + \delta t$ and the posterior conditional probability density of x at time t .

It is assumed, and it can be shown inductively

that the conditional probability densities of $x(t)$ are gaussian.

Stage 1: The effect of the observation:

Bayes rule gives:

$$f(x, t+\delta t / t+\delta t) = \frac{f[x, t+\delta t ; \delta M / t]}{f(\delta M/t)}$$

$$f(x, t+\delta t / t+\delta t) = \frac{f(\delta M, t+\delta t / x, t+\delta t ; t)}{f(\delta M/t)} \cdot f(x, t+\delta t/t).$$

↑
↑
↑

posterior
"likelihood"
prior

probability

probability

density

density

which gives:

$$\exp\left[-\frac{1}{2} (x-\bar{x})^T V^{-1} (x-\bar{x})\right] = k' \exp\left[-\frac{1}{2} (\delta M - G x \delta t) (W \delta t)^{-1}\right]$$

$$(\delta M - G x \delta t) \times \exp\left[-\frac{1}{2} (x-\bar{x})^T \underline{V}^{-1} (x-\bar{x})\right] \tag{4}$$

Where all the terms are evaluated at $t+\delta t$. By equating coefficients of x in (4), we get:

$$\left. \begin{aligned} (5) \quad V &= [\underline{V}^{-1} + G^T W^{-1} G \delta t]^{-1} \\ (6) \quad \bar{x} &= V \underline{V}^{-1} \bar{x} + V G^T W^{-1} \delta M \end{aligned} \right\} \begin{array}{l} \text{where all the terms are} \\ \text{evaluated at } t+\delta t. \end{array}$$

Expanding (5) in a matrix Taylor's series, we get:

$$\left. \begin{aligned} (7) \quad \left\{ \begin{array}{l} V = \underline{V} - \underline{V} G^T W^{-1} G \underline{V} \delta t + O(\delta t). \\ (6) \quad \bar{x} = V \underline{V}^{-1} \bar{x} + V G^T W^{-1} \delta M \end{array} \right. \end{aligned}$$

Taking the conditional moments of (1), we get:

$$(8) \quad \bar{x}(t+\delta t) = [I + (C + C') \delta t] \bar{x}(t) + L m \delta t$$

$$(9) \quad \underline{v}(t+\delta t) = [I + (C + C') \delta t] v(t) [I + (C + C') \delta t]^T + Q \delta t.$$

Substituting (9) in (7), we get:

$$v(t+\delta t) = v(t) + \delta t \{ (C + C') v + v (C + C')^T + Q - v G^T W^{-1} G v \} + o(\delta t).$$

which gives:

$$(10) \quad \frac{dv}{dt} = (C + C') v + v (C + C')^T + Q - v G^T W^{-1} G v$$

Similarly eliminating $\bar{x}(t+\delta t)$ $\underline{v}(t+\delta t)$ from (6), we get:

$$(11) \quad \frac{d\bar{x}}{dt} = (C + C') \bar{x} + L m - v G^T W^{-1} G \bar{x} + v G^T W^{-1} \frac{dM}{dt}$$

Taking the components of (10) and (11) we get the solution of the problem or more precisely its statement:

-system:

$$\frac{dv_{11}}{dt} = 2 c_{11} v_{11} + 2 c_{12} v_{12} + q_1 - \frac{v_{11}^2 g_1^2}{w_1} - \frac{v_{12}^2 g_2^2}{w_2}$$

$$\frac{dv_{22}}{dt} = 2 c_{22} v_{22} + 2 c_{21} v_{12} + q_2 - \frac{v_{12}^2 g_1^2}{w_1} - \frac{v_{22}^2 g_2^2}{w_2}$$

$$\frac{dv_{21}}{dt} = (c_{11} + c_{22}) v_{12} + c_{12} v_{22} + c_{21} v_{11} - \frac{v_{11} v_{12} g_1^2}{w_1} - \frac{v_{22} v_{12} g_2^2}{w_2}$$

$$\frac{d\bar{x}_1}{dt} = c_{11} \bar{x}_1 + c_{12} \bar{x}_2 + l_1 m_1 - \frac{v_{11} g_1^2 \bar{x}_1}{w_1} - \frac{v_{12} g_2^2 \bar{x}_2}{w_2} + \frac{v_{11} g_1}{w_1} \frac{dM_1}{dt} + \frac{v_{12} g_2}{w_2} \frac{dM_2}{dt}$$

$$\frac{d\bar{x}_2}{dt} = c_{22} \bar{x}_2 + c_{21} \bar{x}_1 + l_2 m_2 - \frac{v_{12} g_1^2 \bar{x}_1}{w_1} - \frac{v_{22} g_2^2 \bar{x}_2}{w_2} + \frac{v_{12} g_1}{w_1} \frac{dM_1}{dt} + \frac{v_{22} g_2}{w_2} \frac{dM_2}{dt}$$

-Performance criterion:

$$\phi = \int_0^t e^{\rho t} \{ m_1^2 + m_2^2 + (r_1 - \bar{x}_1)^2 + (r_2 - \bar{x}_2)^2 + v_{11} + v_{22} \} dt$$

The endpoint conditions are:

$$\left\{ \begin{array}{l} \bar{x}_1(0) = x_{10} \\ \bar{y}_1(0) = y_{10} \\ v_{11}(0) = 0 \\ v_{22}(0) = 0 \\ v_{12}(0) = 0 \\ v_{21}(0) = 0 \end{array} \right.$$

The problem is now formulated in terms of a deterministic problem. It can be solved easily.

[Note: p. 83 missing from original. Could just be mis-numbering. RC]

Computation of a numerical example:

-Data:

$$c_{11}(t) = c_{12}(t) = c_{22}(t) = 0 \quad c_{21}(t) = 1 \quad l_1(t) = 1 \quad l_2(t) = 0$$

$$t_e = 0.05 \quad r_1(t) = t \quad r_2(t) = 2t \quad \frac{dM_1}{dt} = t + 0.01 \text{ Sint}$$

$$\frac{dM_2}{dt} = 2t + 0.01 \text{ Sint} \quad w_1 = w_2 = 0.2 \quad q_1 = q_2 = 0.3.$$

-Computation:

$$\begin{aligned}
 & \begin{bmatrix} 2(1-5v_{11}) & 0 & 2(1-5v_{12}) & 0 & 0 \\ 0 & 2(1-5v_{22}) & 2(1-5v_{12}) & 0 & 0 \\ 1-5v_{12} & 1-5v_{12} & 2(5v_{11}-5v_{22}) & 0 & 0 \\ -5\bar{x}_1+5 & 0 & -5\bar{x}_2+5 & 1-5v_{11} & 1-5v_{12} \\ (t+0.01sint) & (t+0.01sint) & (2t+0.01sint) & 1-5v_{11} & 1-5v_{22} \\ 0 & -5\bar{x}_2+5 & -5\bar{x}_1+5 & 1-5v_{12} & 1-5v_{22} \\ & (2t+0.01sint) & (t+0.01sint) & & \end{bmatrix} \\
 & = \\
 & \begin{bmatrix} 2(1-5v_{11}) & 0 & 2(1-5v_{12}) & 0 & 0 \\ 0 & 2(1-5v_{22}) & 2(1-5v_{12}) & 0 & 0 \\ 1-5v_{12} & 1-5v_{12} & 2(5v_{11}-5v_{22}) & 0 & 0 \\ -5\bar{x}_1+5 & 0 & -5\bar{x}_2+5 & 1-5v_{11} & 1-5v_{12} \\ (t+0.01sint) & (t+0.01sint) & (2t+0.01sint) & 1-5v_{11} & 1-5v_{22} \\ 0 & -5\bar{x}_2+5 & -5\bar{x}_1+5 & 1-5v_{12} & 1-5v_{22} \\ & (2t+0.01sint) & (t+0.01sint) & & \end{bmatrix}
 \end{aligned}$$

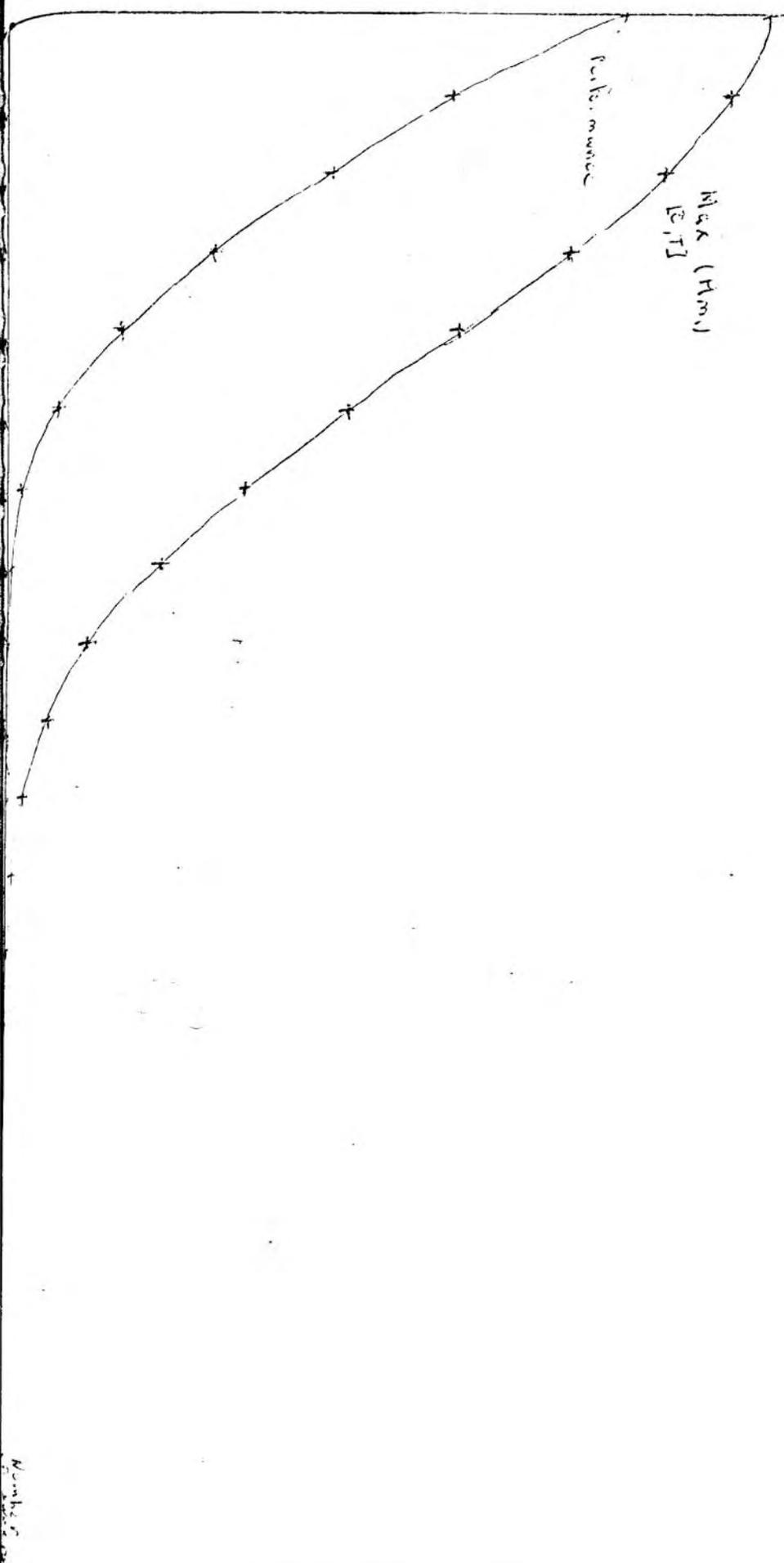
2

$$\mathcal{E} = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & -\frac{1}{2} & 0 \\ 0 & 0 & 0 & 0 & -\frac{1}{2} \end{bmatrix} \quad w_1 = \begin{bmatrix} 0 \\ 0 \\ 0 \\ \frac{\delta H x_1}{2} \\ \frac{\delta H x_2}{2} \end{bmatrix}$$

$$\mathcal{L} = \begin{bmatrix} 10p_1 & 0 & 5p_3 & 5p_4 & 0 \\ 0 & 10p_2 & 5p_3 & 0 & 5p_5 \\ 5p_3 & 5p_3 & 10(p_1+p_2) & 5p_5 & 5p_4 \\ 5p_4 & 0 & 5p_5 & -2 & 0 \\ 0 & 5p_5 & 5p_4 & 0 & -2 \end{bmatrix} \quad w_2 = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

-Results: see Appendix 5, Program 8.

Evolution of the criterion of Performance (curve G) and of the derivative of the norm (curve H) with respect to the control (curve E) versus the number of sweeps in the successive sweep method applied to the system with disturbances (integrated problem).



C Application of the decomposition technique:

If we consider the equations derived in the preceding paragraph we can draw some conclusions:

-A linear system with noises will give a linear system.

-The noise increases the difficulty of the problem: if the former state vector was n -dimensional, the new one will be $[n + \frac{n^2+n}{2}]$ -dimensional [n for the means, $\frac{n^2+n}{2}$ for the variances].

-The deterministic formulation of the stochastic problem shows that the two subproblems are not separated now: in particular when we compute x_1 we have to know the measurements of x_2 and vice-versa. So if we want to use all the data given by the measurements we have to deal with the whole system and transform it in a deterministic problem as we did in the preceding paragraph and then apply the decomposition technique.

For that we introduce dummy variables:

$$\begin{cases} v'_{11} = v_{11} \\ v'_{22} = v_{22} \\ \bar{x}'_1 = \bar{x}_1 \\ \bar{x}'_2 = x_2 \end{cases}$$

$$\begin{cases} v'_{12} = v_{12} \\ v''_{12} = v_{12} \end{cases}$$

Now we can state the problem:

$$\phi = \int_0^t e^{\left\{ \frac{1}{2} [r_1 - \bar{x}_1]^2 + m_1^2 + v_{11} + \frac{1}{2} [r_2 - \bar{x}_2]^2 \right\}} dt +$$

$$\int_0^t e^{\left\{ \frac{1}{2} [r_2 - \bar{x}_2]^2 + m_2^2 + v_{22} + \frac{1}{2} [r_2 - \bar{x}_1]^2 \right\}} dt.$$

With the following constraints:

Lagrange multiplier

$$\left\{ \begin{aligned} \frac{dv_{11}}{dt} &= 2 c_{11} v_{11} + 2 c_{12} v_{12} + q_1 \\ &\quad - \frac{v_{11}^2 g_1^2}{w_1} - \frac{v_{12}^2 g_2^2}{w_2} && p_1 \\ \frac{dv'_{12}}{dt} &= (c_{11} + c_{22}) v'_{12} + c_{12} v'_{22} + c_{21} v_{11} \\ &\quad - \frac{v_{11} v'_{12} g_1^2}{w_1} - \frac{v'_{22} v'_{12} g_2^2}{w_2} && p_2 \\ \frac{d\bar{x}_1}{dt} &= c_{11} \bar{x}_1 + c_{12} \bar{x}_2 + l_1 m_1 - \frac{v_{11} g_1^2 \bar{x}_1}{w_1} \\ &\quad - \frac{v'_{12} g_2^2 \bar{x}_2}{w_2} + \frac{v_{11} g_1}{w_1} \frac{dM_1}{dt} + \frac{v'_{12} g_2}{w_2} \frac{dM_2}{dt} && p_3 \end{aligned} \right.$$

$$\left\{ \begin{aligned} \frac{dv_{22}}{dt} &= 2 c_{22} v_{22} + 2 c_{21} v''_{12} + q_2 - \frac{v''_{12} g_1^2}{w_1} \\ &\quad - \frac{v_{22}^2 g_2^2}{w_2} \quad q_1 \\ \frac{dv''_{12}}{dt} &= (c_{11} + c_{22}) v''_{12} + c_{12} v_{22} + c_{21} v'_{11} \\ &\quad - \frac{v'_{11} v''_{12} g_1^2}{w_1} - \frac{v_{22} v''_{12} g_2^2}{w_2} \quad q_2 \\ \frac{d\bar{x}_2}{dt} &= c_{22} \bar{x}_2 + c_{21} \bar{x}'_1 + l_2 m_2 - \frac{v''_{12} g_1^2 \bar{x}'_1}{w_1} \\ &\quad - \frac{v_{22} g_2^2 \bar{x}_2}{w_2} + \frac{v''_{12} g_1}{w_1} \frac{dM_1}{dt} + \frac{v_{22} g_2}{w_2} \frac{dM_2}{dt} \quad q_3 \\ \bar{x}_1 - \bar{x}'_1 &= 0 \quad R_1 \\ \bar{v}_{11}^2 - \bar{v}'_{11}{}^2 &= 0 \quad R_2 \\ \bar{x}_2 - \bar{x}'_2 &= 0 \quad K_1 \\ v_{22}^2 - v'_{22}{}^2 &= 0 \quad K_2 \end{aligned} \right.$$

Now we can apply the decomposition technique:

Level 1:

subproblem 1:

Given R_1, R_2, K_1, K_2 by the 2nd level, we have:

-Control variables : m_1, \bar{x}'_2, v'_{22} .

-State variables : \bar{x}_1, v_1, v'_{12} .

-Hamiltonian:

$$\begin{aligned}
 H = & \frac{1}{2} [r_1 - \bar{x}_1]^2 + m_1^2 + \frac{1}{2} [r_2 - \bar{x}'_2]^2 + R_1 \bar{x}_1 + R_2 v_{11} \\
 & - K_1 \bar{x}'_2 - K_2 v'_{22} + p_1 [2 c_{11} v_{11} + 2 c_{12} v'_{12} + q_1 \\
 & - \frac{v_{11}^2 g_1^2}{w_1} - \frac{v'_{12}{}^2 g_2^2}{w_2}] + p_2 [(c_{11} + c_{22}) v'_{12} + c_{12} v'_{22} \\
 & + c_{21} v_{11} - \frac{v_{11} v'_{12} g_1^2}{w_1} - \frac{v'_{22} v'_{12} g_2^2}{w_2} + p_3 [c_{11} \bar{x}_1 \\
 & + c_{12} \bar{x}'_2 + l_1 m_1 - \frac{v_{11} g_1^2 \bar{x}_1}{w_1} - \frac{v'_{12} g_2^2 \bar{x}'_2}{w_2} \\
 & + \frac{v_{11} g_1}{w_1} - \frac{dM_1}{dt} + \frac{v'_{12} g_2}{w_2} \frac{dM_2}{dt}] .
 \end{aligned}$$

subproblem 2:

Given R_1, R_2, K_1, K_2 by the 2nd level, we have:

-Control variables : $m_2, \bar{x}'_1, \bar{v}'_{11}$.

-State variables : $\bar{x}_2, v_{22}, v''_{12}$.

-Hamiltonian:

$$\begin{aligned}
 H = & \frac{1}{2} [r_2 - \bar{x}_2]^2 + m_2^2 + v_{22} + \frac{1}{2} [r_1 - \bar{x}'_1]^2 - R_1 \bar{x}'_1 \\
 & - R_2 v'_{11} + K_1 \bar{x}_{22} + K_2 v_{22} + q_1 [2 c_{22} v_{22} \\
 & + 2 c_{21} v''_{12} + q_2 - \frac{v''_{12}{}^2 g_1^2}{w_1} - \frac{v_{22}^2 g_2^2}{w_2}]
 \end{aligned}$$

$$\begin{aligned}
 & + q_2 [(c_{11} + c_{22}) v_{12}'' + c_{12} v_{22} + c_{21} v_{11}' \\
 & - \frac{v_{11}' v_{12}'' g_1^2}{w_1} - \frac{v_{22} v_{12}'' g_2^2}{w_2}] + q_3 [c_{22} \bar{x}_2 + c_{21} \bar{x}_1' \\
 & + l_2 m_2 - \frac{v_{12}'' g_1^2 \bar{x}_1'}{w_1} - \frac{v_{22} g_2^2 \bar{x}_2}{w_2} + \frac{v_{12}'' g_1}{w_1} \frac{dM_1}{dt} \\
 & + \frac{v_{22} g_2}{w_2} \frac{dM_2}{dt}]
 \end{aligned}$$

Level 2 or coordination level:

We vary K_1, K_2, R_1, R_2 according to:

$$[K_1]_{n+1} = [K_1]_n + \epsilon * [\bar{x}_2 - \bar{x}_2']$$

$$[K_2]_{n+1} = [K_2]_n + \epsilon * [v_{22}^2 - v_{22}'^2]$$

$$[R_1]_{n+1} = [R_1]_n + \epsilon * [\bar{x}_1 - \bar{x}_1']$$

$$[R_2]_{n+1} = [R_2]_n + \epsilon * [v_{11}^2 - v_{11}'^2]$$

Computation of a numerical example:

-Data:

$$c_{11}(t) = c_{12}(t) = c_{22}(t) = 0 \quad c_{21}(t) = 1 \quad l_1(t) = 1 \quad l_2(t) = 0$$

$$t_e = 0.05 \quad r_1(t) = t \quad r_2(t) = 2t \quad \frac{dM_1}{dt} = t + 0.01 \sin t$$

$$\frac{dM_2}{dt} = 2t + 0.01 \sin t \quad w_1 = w_2 = 0.2 \quad q_1 = q_2 = 0.3$$

-Computation:

subsystem 1:

$$D = \begin{bmatrix} -2 \frac{v_{11}}{w_1} & -2 \frac{v'_{12}}{w_2} & 0 \\ 1 - \frac{v'_{12}}{w_1} & -\frac{v_{11}}{w_1} - \frac{v'_{22}}{w_2} - \frac{v'_{12} p_2}{2K_2 w_2^2} & 0 \\ -\frac{\bar{x}_1}{w_1} + \frac{1}{w_1} \frac{dM_1}{dt} & -\frac{x'_2}{w_2} + \frac{1}{w_2} \frac{dM_2}{dt} - \frac{2p_3 v'_{12}}{w_2^2} & -\frac{v_1}{w_1} \end{bmatrix}$$

$$E = \begin{bmatrix} 0 & 0 & 0 \\ 0 & -\frac{v'_{12}{}^2}{2K_2 w_2^2} & 0 \\ 0 & 0 & -\frac{2v'_{12}{}^2}{w_2^2} - 1 \end{bmatrix} \quad w_1 = \begin{bmatrix} 0 \\ -\frac{v'_{12}}{2K_2 w_2} \delta H v'_{22} \\ \delta H m_1 - \frac{2v_{12}}{w_2} \delta H \bar{x}'_2 \end{bmatrix}$$

$$L = \begin{bmatrix} \frac{2p_1}{w_1} - 2K_1 & \frac{p_2}{w_1} & \frac{p_3}{w_1} \\ \frac{p_2}{w_1} & \frac{2p_1 + \frac{p_2^2}{2K_2 w_2^2} + \frac{2p_3}{w_2}}{w_2} & 0 \\ \frac{p_3}{w_1} & 0 & -0.5 \end{bmatrix} \quad w_2 = \begin{bmatrix} 0 \\ \frac{p_2}{2K_2 w_2} + \frac{2p_3}{w_2} \delta H \bar{x}'_2 \\ 0 \end{bmatrix}$$

subsystem 2:

$$D = \begin{bmatrix} -2 \frac{v_{22}}{w_2} & 2(1 - \frac{v''_{12}}{w_1}) & 0 \\ -\frac{v''_{12}}{w_2} & -\frac{v'_{11}}{w_1} - \frac{v_{22}}{w_2} - \frac{q_2}{2K_1 w_1} (1 - \frac{v''_{12}}{w_1}) & 0 \\ -\frac{\bar{x}_2}{w_2} + \frac{1}{w_2} \frac{dM_2}{dt} & -\frac{\bar{x}_1}{w_1} + \frac{1}{w_1} \frac{dM_1}{dt} + (1 - \frac{v''_{12}}{w_1}) \frac{2q_3}{w_1} & -\frac{v_2}{w_2} \end{bmatrix}$$

$$Q = \begin{bmatrix} 0 & 0 & 0 \\ 0 & \frac{1}{2K_1} (1 - \frac{v''_{12}}{w_1})^2 & 0 \\ 0 & 0 & -2(1 - \frac{v''_{12}}{w_1})^2 \end{bmatrix} \quad w_1 = \begin{bmatrix} 0 \\ -\frac{1}{2K_1} (1 - \frac{v''_{12}}{w_1}) \delta H v'_{11} \\ 2(1 - \frac{v''_{12}}{w_1}) \delta H \bar{x}'_1 \end{bmatrix}$$

-Results: see Appendix 5, Program 9.

time

total computing time

Computation time (total # per iteration) for a system with disturbances, when the decomposition technique is used.

computing time per each iteration (# of)

200



Number of computing iterations

SOM 1

Evaluation of the effectiveness of the
decomposition technique program:

$$SOM 1 = \int_0^T \{ (\bar{x}_1 - \bar{x}'_1)^2 + (x_2 - x'_2)^2 + (V_1 - V'_1)^2 + (V_2 - V'_2)^2 \} dt.$$

Number of
coordination iterations

We can make the following observations:

- The decomposition technique for deterministic systems is based on a saddle value point argumentation. Since we are dealing with another kind of problem, i.e., a stochastic problem, it should be shown that the optimum point is a saddle value point. This argument is still true since we transformed the stochastic problem into a more complex but deterministic linear quadratic problem.
- The advantages of the decomposition technique are the same as in the deterministic case.
- To find the equations of the subsystems we had first to compute the equations of the global system. The set of equations of the two subsystems is equivalent to the set of equations of the global system. So the solutions will be the same. In particular, the information about the measurements of the global system are included in the equations of each subsystem.

4.2 A Case of Linear System With Non-Linear Coupling

In this section we deal with a numerical example of linear system with non-linear coupling. It is the case of slightly non-linear systems, the non-linearity of which can be expanded in a Taylor's series for which all the terms $\{ x^n / n \geq 3 \}$ are neglected.

4.2.1 The Deterministic Problem

Part 1: global method:

-system:

$$\begin{aligned}\dot{x}_1 &= m \\ \dot{x}_2 &= x_1 + 0.1 x_1^2\end{aligned}$$

-Control variable : m.

-State variables : $x_1 + x_2$.

-performance:

$$\phi = \int_0^t e^{-\frac{1}{2} [x_1^2 + x_2^2 + m^2]} dt$$

-Computation:

$$\mathcal{D} = \begin{bmatrix} 0 & 0 \\ 1+0.2x_1 & 0 \end{bmatrix} \quad \mathcal{E} = \begin{bmatrix} -1 & 0 \\ 0 & 0 \end{bmatrix} \quad w_1 = \begin{bmatrix} \delta Hm \\ 0 \end{bmatrix}$$

$$\mathcal{L} = \begin{bmatrix} -(1+0.2p_2) & 0 \\ 0 & -1 \end{bmatrix} \quad w_2 = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

-Results: see Appendix 5, Program 10.

Part 2: decomposition technique:

Level 1:

subsystem 1:

$$\dot{x}_1 = m H = \frac{1}{2} m^2 + \frac{1}{2} x_1^2 + K x_1 (1+0.1 x_1) + p_1 m$$

subsystem 2:

$$\dot{x}_2 = t_1 \quad H = \frac{1}{2} x_2^2 - K t_1^2 + p_2 t_1$$

Level 2:

$$[K]_{n+1} = [K]_n + \epsilon * [x_1 + 0.1 x_1^2 - t_1]$$

Computation:

subsystem 1:

$$\mathcal{D} = 0 \quad \mathcal{E} = -1 \quad w_1 = \delta H m \quad \mathcal{L} = -(1 \pm 0.2 K) \quad w_2 = 0$$

subsystem 2:

$$\mathcal{D} = 0 \quad \mathcal{E} = -\frac{2 t_1^2}{p_2 - K} \quad w_1 = \frac{t_1 \delta H t_1}{p_2 - K} \quad \mathcal{L} = -1 \quad w_2 = 0$$

-Results: see Appendix 5, Program 11.

4.2.2 The Problem With Noises

A Statement of the problem:

System:

$$\left\{ \begin{array}{l} dx_1 = x_1 dt + dz_1 \end{array} \right.$$

$$\{ dx_2 = (x_1 + 0.1 x_1^2) dt + dz_2$$

Measurements:

$$\begin{cases} dM_1 = x_1 dt + dN_1 \\ dM_2 = x_2 dt + dN_2 \end{cases}$$

dz, dz_2, dN_1, dN_2 are uncorrelated noises with gaussian probability such that: $\forall t, \forall s \neq t$, we have

$$E[dz_1(t)] = E[dz_2(t)] = E[dN_1(t)] = E[dN_2(t)] = 0$$

$$E[dz_1(t)^2] = q_1 dt \qquad E[dN_1^2(t)] = w_1 dt$$

$$E[dz_2(t)^2] = q_2 dt \qquad E[dN_2^2(t)] = w_2 dt$$

We are assuming too that the variables x_1, x_2 have a two dimensional normal distribution, which, in fact, is not true, because of the non-linear term. But we shall consider that the coefficients of this term is small enough and does not greatly affect the distribution of x , the density function of which is given by:

$$F(x_1, x_2) = \frac{1}{2\pi} \frac{1}{\sqrt{v_{11} v_{22} - v_{12}^2}} \text{Exp} \left\{ \frac{-1}{2 \left(1 - \frac{v_{12}^2}{v_{11} v_{22}}\right)} \left[\frac{(x_1 - \bar{x}_1)^2}{v_{11}} - \frac{2(x_1 - \bar{x}_1)(x_2 - \bar{x}_2) v_{12}}{v_{11} v_{22}} + \frac{(x_2 - \bar{x}_2)^2}{v_{22}} \right] \right\}.$$

which means:

$$E[(x_1 - \bar{x}_1)^2 (x_2 - \bar{x}_2)] = E\{ [x_2 - \bar{x}_2]^2 [x_1 - \bar{x}_1] \}$$

$$= E\{ [x_1 - \bar{x}_1]^{2K+1} \} = E\{ [x_2 - \bar{x}_2]^{2K+1} \} = 0$$

$$E\{ (x_1 - \bar{x}_1)^2 (x_2 - \bar{x}_2)^2 \} = \frac{v_{11} v_{22} (v_{11} v_{22} + 2 v_{12}^2)}{2(v_{11} v_{22} - v_{12}^2)}$$

B The global method.

The method is the same as in the linear case. We have the following steps:

$$\bar{x}_1(t+\delta t) = \bar{x}_1(t) + m_1(t) \delta t$$

$$\bar{x}_2(t+\delta t) = \bar{x}_2(t) + \delta t[\bar{x}_1(t) + 0.1 v_1(t) + 0.1 x_1(t)^2]$$

$$v_1(t+\delta t) = v_1(t) + q_1 \delta t$$

$$v_2(t+\delta t) = v_2(t) + \delta t [2.4 v_{12}(t) + q_2]$$

$$v_{12}(t+\delta t) = v_{12}(t) + v_1(t) (1 + 0.2 \bar{x}_1(t))$$

The assumption of a normal distribution gives:

$$\left(v_{11} = \frac{v_{11}}{w_1} - \frac{v_{11}^2}{w_1} \delta t - \frac{v_{12}^2}{w_2} \delta t \right)$$

with all
the
variables
evaluated
at
 $t+\delta t$.

$$\left. \begin{aligned} v_{12} &= \frac{v_{12}}{w_1} - \frac{v_{11} v_{12}}{w_1} \delta t - \frac{v_{22} v_{12}}{w_2} \delta t \\ v_{22} &= \frac{v_{22}}{w_1} - \frac{v_{12}^2}{w_1} \delta t - \frac{v_{22}}{w_2} \delta t \\ \bar{x}_1 &= \bar{x}_1 = \frac{\bar{x}_1 v_{11}}{w_1} \delta t - \frac{\bar{x}_2 v_{12}}{w_2} \delta t + \frac{v_{11}}{w_1} \delta M_1 \\ &\quad + \frac{v_{12}}{w_2} \delta M_2 \\ \bar{x}_2 &= \bar{x}_2 - \frac{\bar{x}_1 v_{12}}{w_1} \delta t - \frac{\bar{x}_2 v_{22}}{w_2} \delta t + \frac{v_{12}}{w_1} \delta M_1 \\ &\quad + \frac{v_{22}}{w_2} \delta M_2 \end{aligned} \right\}$$

Finally the equations of the system are:

$$\left\{ \begin{aligned} \frac{dv_{11}}{dt} &= q_1 - \frac{v_{11}^2}{w_1} - \frac{v_{12}^2}{w_2} \\ \frac{dv_{12}}{dt} &= v_{11} (1 + 0.2 \bar{x}_1) - \frac{v_{11} v_{12}}{w_1} - \frac{v_{22} v_{12}}{w_2} \\ \frac{dv_{22}}{dt} &= 2.4 v_{12} + q_2 - \frac{v_{12}^2}{w_1} - \frac{v_{22}^2}{w_2} \\ \frac{d\bar{x}_1}{dt} &= m_1 - \frac{\bar{x}_1 v_{11}}{w_1} - \frac{\bar{x}_2 v_{12}}{w_2} + \frac{v_{11}}{w_1} \frac{dM_1}{dt} + \frac{v_{12}}{w_2} \frac{dM_2}{dt} \end{aligned} \right.$$

$$\left(\frac{d\bar{x}_2}{dt} = \bar{x}_1 + 0.1 v_{11} + 0.1 \bar{x}_1^2 - \frac{\bar{x}_1 v_{12}}{w_1} - \frac{\bar{x}_2 v_{22}}{w_2} \right. \\ \left. + \frac{v_{12}}{w_1} \frac{dM_1}{dt} + \frac{v_{22}}{w_2} \frac{dM_2}{dt} \right)$$

Criterion of performance:

$$\phi = \int_0^t e^{-\frac{1}{2} t} [\bar{x}_1^2 + \bar{x}_2^2 + v_{11} + v_{22} + m_1^2] dt$$

Computation of the solution

$$\mathcal{D} = \begin{bmatrix}
 -\frac{2 v_{11}}{w_1} & -\frac{2 v_{12}}{w_2} & 0 & 0 \\
 1 + 0.2 \bar{x}_1 - \frac{v_{12}}{w_1} & -\frac{v_{11}}{w_1} - \frac{v_{22}}{w_2} & 0.2 v_{11} & 0 \\
 0 & 2.4 - \frac{2 v_{12}}{w_1} & 0 & -\frac{2 v_{22}}{w_2} \\
 -\frac{\bar{x}_1}{w_1} + \frac{1}{w_1} \frac{dM_1}{dt} & -\frac{\bar{x}_2}{w_2} + \frac{1}{w_2} \frac{dM_2}{dt} & -\frac{v_{11}}{w_1} & -\frac{v_{12}}{w_2} \\
 0.1 & -\frac{\bar{x}_1}{w_1} + \frac{1}{w_1} \frac{dM_1}{dt} & 1 + 0.2 \bar{x}_1 - \frac{v_{12}}{w_1} & -\frac{v_{22}}{w_2}
 \end{bmatrix}$$

Computation of the solution (con't)

$$\mathcal{E} = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & 0 & 0 \end{bmatrix} \quad w_1 = \begin{bmatrix} 0 \\ 0 \\ 0 \\ \delta Hm_1 \\ 0 \end{bmatrix}$$

$$\mathcal{L} = \begin{bmatrix} \frac{2p_1}{w_1} & \frac{p_2}{w_1} & 0 & \frac{p_4}{w_1} - 0.2 p_2 & 0 \\ \frac{p_2}{w_1} & \frac{2p_1}{w_2} + \frac{2p_3}{w_1} & \frac{p_2}{w_2} & \frac{p_5}{w_1} & \frac{p_4}{w_2} \\ 0 & \frac{p_2}{w_2} & \frac{2p_3}{w_2} & 0 & \frac{p_5}{w_2} \\ 0 & \frac{p_4}{w_2} & \frac{p_5}{w_2} & 0 & -1 \end{bmatrix}$$

$$w_2 = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

C The decomposition technique:

As before we take the dummy variables:

$$\begin{cases} \bar{x}'_1 = \bar{x}_1 \\ \bar{x}'_2 = \bar{x}_2 \\ v'_{11} = v_{11} \\ v'_{22} = v_{22} \\ v'_{12} = v''_{12} = v_{12} \end{cases}$$

we get:

Level 1:

*subsystem 1:

-Control variables : m_1, v'_{22}, \bar{x}'_2 .

-performance:

$$\int_0^t e^{\left\{ \frac{1}{2} \left[\frac{1}{2} \bar{x}_1^2 + \frac{1}{2} \bar{x}_2^2 + v_{11} + m_1^2 \right] + R_1 \bar{x}_1 + R_2 v_{11}^2 - K_1 \bar{x}'_2 - K_2 v_{22}'^2 \right\}} dt$$

-constraints:

Lagrange
multipliers

$$\begin{cases} \frac{dv_{11}}{dt} = -\frac{v_{11}^2}{w_1} - \frac{v_{12}'^2}{w_2} & p_1 \\ \frac{dv_{12}'}{dt} = v_{11} (1 + 0.2 \bar{x}_1) - \frac{v_{11} v_{12}'}{w_1} - \frac{v_{22}' v_{12}'}{w_2} & p_2 \end{cases}$$

$$\left\{ \begin{aligned} \frac{d\bar{x}_1}{dt} &= m_1 - \frac{\bar{x}_1 v_{11}}{w_1} - \frac{\bar{x}_2' v_{12}'}{w_2} + \frac{v_{11}}{w_1} \frac{dM_1}{dt} \\ &+ \frac{v_{12}'}{w_2} \frac{dM_2}{dt} \end{aligned} \right. \quad p_3$$

*subsystem 2:

-Control variables : v_{11}', \bar{x}_1'

-performance:

$$\int_0^t e^{-\rho t} \left\{ \frac{1}{2} \left[\frac{1}{2} \bar{x}_1'^2 + \frac{1}{2} \bar{x}_2^2 + v_{22} \right] + K_1 \bar{x}_2 + K_2 v_{22}^2 - R_1 \bar{x}_1' \right. \\ \left. - R_2 v_{11}'^2 \right\}$$

-constraints:

Lagrange
multipliers

$$\left\{ \begin{aligned} \frac{dv_{22}}{dt} &= 2.4 v_{12}'' + q_2 - \frac{v_{12}''^2}{w_1} - \frac{v_{22}^2}{w_2} & q_1 \\ \frac{dv_{12}''}{dt} &= v_{11}' (1 + 0.2 \bar{x}_1') - \frac{v_{11}' v_{12}''}{w_1} \\ &- \frac{v_{22} v_{12}''}{w_2} & q_2 \\ \frac{d\bar{x}_2}{dt} &= \bar{x}_1' + 0.1 v_{11}' + 0.1 \bar{x}_1'^2 - \frac{\bar{x}_1' v_{12}''}{w_1} \\ &- \frac{\bar{x}_2 v_{22}}{w_2} + \frac{v_{12}''}{w_1} \frac{dM_1}{dt} + \frac{v_{22}}{w_2} \frac{dM_2}{dt} & q_3 \end{aligned} \right.$$

Level 2 or coordination level:

We vary R_1 , R_2 , K_1 , K_2 according to:

$$[R_1]_{n+1} = [R_1]_n + \epsilon * [\bar{x}_1 - \bar{x}'_1]$$

$$[R_2]_{n+1} = [R_2]_n + \epsilon * [v_{11}^2 - v'_{11}{}^2]$$

$$[K_1]_{n+1} = [K_1]_n + \epsilon * [\bar{x}_2 - \bar{x}'_2]$$

$$[K_2]_{n+1} = [K_2]_n + \epsilon * [v_{22}^2 - v'_{22}{}^2]$$

Computation of the solution:

subsystem 1:

$$D = \begin{bmatrix} -\frac{2 v_{11}}{w_1} & -\frac{2 v'_{12}}{w_2} & 0 \\ 1+0.2\bar{x}_1 - \frac{v'_{12}}{w_1} & -\frac{v_{11}}{w_1} - \frac{v'_{22}}{w_2} + \frac{p_2 v'_{12}}{2K_2 w_2^2} & 0.2 v_{11} \\ -\frac{\bar{x}_1}{w_1} + \frac{1}{w_1} \frac{dM_1}{dt} & -\frac{\bar{x}'_2}{w_2} + \frac{1}{w_2} \frac{dM_2}{dt} - \frac{2p_3 v'_{12}}{w_2^2} & -\frac{v_{11}}{w_1} \end{bmatrix}$$

$$\mathcal{E} = \begin{bmatrix} 0 & 0 & 0 \\ 0 & \frac{v'_{12}{}^2}{2K_2 w_2^2} & 0 \\ 0 & 0 & -1 - \frac{2 v'_{12}{}^2}{w_2} \end{bmatrix} \quad w_1 = \begin{bmatrix} 0 \\ \frac{v'_{12}}{2K_2 w_2^2} \delta H v'_{22} \\ \delta H m_1 - \frac{2 v'_{12}}{w_2} \delta H x'_2 \end{bmatrix}$$

$$\mathcal{L} = \begin{bmatrix} -2p_2 + \frac{2p_1}{w_1} & \frac{p_3}{w_1} & \frac{p_3}{w_1} - 0.2 p_2 \\ \frac{p_2}{w_1} & \frac{2p_1}{w_2} - \frac{p_2^2}{2K_2 w_2^2} + \frac{2p_3^2}{w_2^2} & 0 \\ -0.2p_2 + \frac{p_3}{w_1} & 0 & -0.5 + 2 K_1 \end{bmatrix}$$

$$w_2 = \begin{bmatrix} 0 \\ -\frac{p_2}{2K_2 w_2} \delta H v'_{22} + \frac{2p_3}{w_2} \delta H \bar{x}'_2 \\ 0 \end{bmatrix}$$

subsystem 2:

The equations are far more complex. Only the equations were derived:

$$\delta \bar{x}'_1 = \frac{1}{1+0.4 q_3} [-0.4 q_2 \delta v'_{11} + \frac{2q_3}{w_1} \delta v''_{12} - 0.4 v'_{11} \delta q_2 - 2(1 + 0.2 \bar{x}'_{11} - \frac{v''_{12}}{w_1}) \delta q_3 + 2\delta Hx'_1]$$

$$\delta v'_{11} = \frac{1}{2R_2} [-\frac{q_2}{w_1} \delta v''_{12} + (1 + 0.2 \bar{x}'_1 - \frac{v''_{12}}{w_1}) \delta q_2 + 0.1 \delta q_3 - \delta H v'_{11} + 0.2 q_2 \delta \bar{x}'_1]$$

$$\left\{ \begin{aligned} \dot{\delta v}_{22} &= -\frac{2 v_{22}}{w_2} \delta v_{22} + (2.4 - \frac{2 v''_{12}}{w_1}) \delta v''_{12} \\ \dot{\delta v}''_{12} &= -\frac{v''_{12}}{w_2} \delta v_{22} + (-\frac{v_{22}}{w_2} - \frac{v'_{11}}{w_1}) \delta v''_{12} + (1 + 0.2 \bar{x}'_1 - \frac{v''_{12}}{w_1}) \delta v'_{11} + 0.2 v'_{11} \delta \bar{x}'_1 \\ \dot{\delta \bar{x}}_2 &= (-\frac{\bar{x}_2}{w_2} + \frac{1}{w_2} \frac{dM_2}{dt}) \delta v_{22} + (-\frac{\bar{x}'_1}{w_1} + \frac{1}{w_1} \frac{dM_1}{dt}) \delta v''_{12} - \frac{v_{22}}{w_2} \delta \bar{x}_2 + 0.1 \delta v'_{11} + (1 + 0.2 \bar{x}'_1 - \frac{v''_{12}}{w_1}) \delta \bar{x}'_1 \end{aligned} \right.$$

$$\left\{ \begin{aligned} \dot{\delta q}_1 &= - \{ (2K_2 - \frac{2q_1}{w_2}) \delta v_{22} - \frac{q_2}{w_2} \delta v''_{12} - \frac{2 v_{22}}{w_2} \delta q_1 - \frac{v''_{12}}{w_2} \delta q_2 + (-\frac{x_2}{w_2} + \frac{1}{w_2} \frac{dM_2}{dt}) \delta q_3 - \frac{q_3}{w_2} \delta \bar{x}_2 \} \end{aligned} \right.$$

$$\left\{ \begin{aligned} \dot{\delta q}_2 &= - \left\{ - \frac{q_2}{w_2} \delta v_{22} - \frac{2q_1}{w_1} \delta v_{12}'' + \left(2.4 - \frac{2 v_{12}''}{w_1} \right) \delta q_1 \right. \\ &\quad \left. + \left(- \frac{v_{11}'}{w_1} - \frac{v_{22}'}{w_2} \right) \delta q_2 + \left(- \frac{\bar{x}_1'}{w_1} + \frac{1}{w_1} \frac{dM_1}{dt} \right) \delta q_3 - \frac{q_3}{w_1} \delta \bar{x}_1' \right\} \\ \dot{\delta q}_3 &= - \left\{ - \frac{q_3}{w_2} \delta v_{22} + 0.5 \delta \bar{x}_2 \right\}. \end{aligned} \right.$$

4.3 Generalization

Let us consider a general system with additive noise:
noise:
system:

$$\begin{cases} \dot{x}_1 = f_1(x_1, x_2, m_1, m_2, t) + \frac{dz_1}{dt} \\ \dot{x}_2 = f_2(x_1, x_2, m_1, m_2, t) + \frac{dz_2}{dt} \end{cases}$$

measurements:

$$\begin{cases} \frac{dM_1}{dt} = x_1 + \frac{dN_1}{dt} \\ \frac{dM_2}{dt} = x_2 + \frac{dN_2}{dt} \end{cases}$$

performance:

$$\int_0^t e^{-\rho t} \varphi [v_{11}, v_{22}, v_{12}, \bar{x}_1, \bar{x}_2]$$

controls : m_1, m_2 .

state variables : x_1, x_2 .

We shall call

$$g_1 [v_{11}, v_{22}, v_{12}, \bar{x}_1, \bar{x}_2, m_1, m_2, t] = E \{f_1\}.$$

$$g_2 [v_{11}, v_{22}, v_{12}, \bar{x}_1, \bar{x}_2, m_1, m_2, t] = E \{f_2\}.$$

$$g_3 [v_{11}, v_{22}, v_{12}, \bar{x}_1, \bar{x}_2, m_1, m_2, t] = E \{ (f_1 - g_1) \\ (x_1 - \bar{x}_1) \}.$$

$$g_4 [v_{11}, v_{22}, v_{12}, \bar{x}_1, \bar{x}_2, m_1, m_2, t] = E \{ (f_2 - g_2) \\ (x_2 - \bar{x}_2) \}.$$

$$g_5 [v_{11}, v_{22}, v_{12}, \bar{x}_1, \bar{x}_2, m_1, m_2, t] = E \{ (f_2 - g_2) \\ (x_1 - \bar{x}_1) \}.$$

$$g_6 [v_{11}, v_{22}, v_{12}, \bar{x}_1, \bar{x}_2, m_1, m_2, t] = E \{ (f_1 - g_1) \\ (x_2 - \bar{x}_2) \}.$$

Two strong assumptions have to be done on the system:

-The possibility of using the decomposition technique for the deterministic problem, i.e., we must check the argumentation based on a saddle value point at the optimal.

-We assume during all the demonstration that the variable (x_1, x_2) has a two dimensional normal distribution which is unlikely if the system is strongly non-linear.

We have:

$$x_1(t+\delta t) = x_1(t) + f_1 \delta t + \delta Z_1$$

$$x_2(t+\delta t) = x_2(t) + f_2 \delta t + \delta Z_2.$$

Taking the expectations, we get:

$$\begin{cases} \bar{x}_1(t+\delta t) = \bar{x}_1(t) + g_1 \delta t \\ \bar{x}_2(t+\delta t) = \bar{x}_2(t) + g_2 \delta t \end{cases}$$

$$\begin{cases} v_1(t+\delta t) = v_1(t) + \delta t(2g_3 + q_1) \\ v_2(t+\delta t) = v_2(t) + \delta t(2g_4 + q_2) \\ v_{12}(t+\delta t) = v_{12}(t) + \delta t(g_5 + g_6). \end{cases}$$

As before, the assumption of a normal distribution gives us:

$$\begin{cases} v_1 = \frac{v_1}{w_1} - \frac{v_1^2}{w_1} \delta t - \frac{v_{12}^2}{w_2} \delta t \\ v_{12} = \frac{v_{12}}{w_1} - \frac{v_{11} v_{12}}{w_1} \delta t - \frac{v_{22} v_{12}}{w_2} \delta t \\ v_{22} = \frac{v_{22}}{w_1} - \frac{v_{12}^2}{w_1} \delta t - \frac{v_{22}^2}{w_2} \delta t \end{cases}$$

$$\left\{ \begin{aligned} \bar{x}_1 &= \bar{x}_1 - \frac{\bar{x}_1 v_{11}}{w_1} \delta t - \frac{\bar{x}_2 v_{12}}{w_2} \delta t + \frac{v_{11}}{w_1} \delta M_1 + \frac{v_{12}}{w_2} \delta M_2 \\ \bar{x}_2 &= \bar{x}_2 - \frac{\bar{x}_1 v_{12}}{w_1} \delta t - \frac{\bar{x}_2 v_{12}}{w_1} \delta t - \frac{\bar{x}_2 v_2}{w_2} \delta t + \frac{v_{12} \delta M_1}{w_1} \\ &\quad + \frac{v_{22} \delta H_2}{w_2} \end{aligned} \right.$$

Combining the two systems of equations, we get:

$$\left\{ \begin{aligned} \frac{dv_{11}}{dt} &= 2 g_3 + q_1 - \frac{v_{11}^2}{w_1} g_1^2 - \frac{v_{12}^2}{w_2} g_2^2 \\ \frac{dv_{12}}{dt} &= g_5 + g_6 - \frac{v_{11} v_{12}}{w_1} g_1^2 - \frac{v_{22} v_{12}}{w_2} g_2^2 \\ \frac{dv_{22}}{dt} &= 2 g_4 + q_2 - \frac{v_{12}^2 g_1^2}{w_1} - \frac{v_{22} v_{12}}{w_2} g_2^2 \end{aligned} \right.$$

$$\left\{ \begin{aligned} \frac{d\bar{x}_1}{dt} &= g_1 - \frac{\bar{x}_1 v_{11}}{w_1} - \frac{\bar{x}_2 v_{12}}{w_2} + \frac{v_{11}}{w_1} \frac{dM_1}{dt} + \frac{v_{12}}{w_2} \frac{dM_2}{dt} \\ \frac{d\bar{x}_2}{dt} &= g_2 - \frac{\bar{x}_1 v_{12}}{w_1} - \frac{\bar{x}_2 v_{22}}{w_2} + \frac{v_{12}}{w_1} \frac{dM_1}{dt} + \frac{v_{22}}{w_2} \frac{dM_2}{dt} \end{aligned} \right.$$

We succeeded in transforming the problem with stochastic variables in a deterministic problem. So we can apply the decomposition technique:

Level 1:

*subproblem 1:

-State variables : $\bar{x}_1, v_{11}, v_{12}$

-Controls : m_1, \bar{x}_2', v_{22}'

system:

$$\left\{ \begin{aligned} \frac{dv_{11}}{dt} &= 2 g_3 + q_1 - \frac{v_{11}^2}{w_1} g_1^2 - \frac{v_{12}^2}{w_2} g_2^2 \\ \frac{dv'_{12}}{dt} &= g_5 + g_6 - \frac{v_{11} v'_{12}}{w_1} g_1^2 - \frac{v'_{22} v'_{12}}{w_2} g_2^2 \\ \frac{d\bar{x}_1}{dt} &= g_1 - \frac{\bar{x}_1 v_{11}}{w_1} - \frac{x_2 v'_{12}}{w_2} + \frac{v_{11}}{w_1} \frac{dM_1}{dt} + \frac{v'_{12}}{w_2} \frac{dM_2}{dt} \end{aligned} \right.$$

performance:

$$\phi = \int_0^t e^{\frac{1}{2} \varphi [v_{11}, v_{22}, v'_{12}, \bar{x}_1, \bar{x}'_2] + R_1 x_1 + R_2 v_{11} - K_1 \bar{x}'_2 - K_2 v'_{22}} dt$$

*subproblem 2:

-State variables : $\bar{x}_2, v_{22}, v''_{12}$

-Controls : m_2, v'_1, \bar{x}'_1

system:

$$\left\{ \begin{aligned} \frac{dv_{22}}{dt} &= 2 g_4 + q_2 - \frac{v_{12}^2}{w_1} g_1^2 - \frac{v_{22} v_{12}}{w_2} g_2^2 \\ \frac{dv''_{12}}{dt} &= g_5 + g_6 - \frac{v_{11} v''_{12}}{w_1} g_1^2 - \frac{v_{22} v''_{12}}{w_2} g_2^2 \\ \frac{d\bar{x}_2}{dt} &= g_2 - \frac{\bar{x}'_1 v''_{12}}{w_1} - \frac{\bar{x}_2 v_{22}}{w_2} + \frac{v''_{12}}{w_1} \frac{dM_1}{dt} + \frac{v_{22}}{w_2} \frac{dM_2}{dt} \end{aligned} \right.$$

performance:

$$\phi = \int_0^t e^{\epsilon \left\{ \frac{1}{2} \varphi [v'_{11}, v_{22}, v''_{12}, \bar{x}'_1, \bar{x}_2] - R_1 \bar{x}'_1 - R_2 v'_{11} + K_1 \bar{x}_2 + K_2 v_{22} \right\}} dt.$$

Level 2 or coordination level:

We vary K_1, K_2, R_1, R_2 according to:

$$[R_1]_{n+1} = [R_1]_n + \epsilon * [\bar{x}_1 - \bar{x}'_1]$$

$$[R_2]_{n+1} = [R_2]_n + \epsilon * [v_{11} - v'_{11}]$$

$$[K_1]_{n+1} = [K_1]_n + \epsilon * [\bar{x}_2 - \bar{x}'_2]$$

$$[K_2]_{n+1} = [K_2]_n + \epsilon * [v_{22} - v'_{22}].$$

CHAPTER V

CONCLUSIONS

The application of the satisfaction approach of Takahara to linear quadratic systems was easy to implement, once it was shown that the set of internal disturbances could be reduced to one point. To extend this technique to non linear systems, a way of formulating the mathematical models of the first level and of implementing the coordination must be found first.

A heuristic dealing with discrete linear systems was studied in Chapter 3. The main advantage of this heuristic lies in the fact that the programming of the computation of the optimal control is much easier to do than with the general method. This heuristic dealing with separate subsystems, should be of some interest from a computing time point of view. But this has to be proved. One can expect, too, that, with some more assumptions, this heuristic converges for linear continuous systems.

In Chapter 4, the decomposition technique was applied to linear systems with disturbances, with the help of the Kalman technique. No significant reduction in the computing time was given by the application of the technique, but it should be remembered that the technique is efficient for large scale systems, which was not the case here. For non linear systems, the state variable

is not likely to have a gaussian distribution, and the Kalman technique cannot be used. So the problem of application of the decomposition technique to non linear systems with disturbances has still to be solved.

APPENDIX I

A COMPUTATIONAL TECHNIQUE USED TO SOLVE OPTIMAL PROGRAMMING PROBLEMS: THE SUCCESSIVE SWEEP METHOD.

A complete study of the successive sweep method can be found in reference [6]. The method will be explained briefly here in order to define the notations which will be used later.

Consider the system:

$$\dot{x} = f(x, m, t) \quad x(0) = x_0$$

The performance can be written as:

$$\phi = \int_0^{t_e} [H(p, x, m) - p^T \dot{x}] dt$$

with:

$x(t)$: n -component state vector.

$m(t)$: m -component control vector.

$p(t)$: n -component Lagrange multiplier vector.

The necessary conditions for an extremal path are:

$$\dot{p} = -H_x \quad (1)$$

$$H_m = 0 \quad (2)$$

$$p(t_e) = 0 \quad (3)$$

If some arbitrary control function $m(t)$ is chosen, then equation (2) will not be satisfied. We consider a perturbation around $m(t)$: we get:

$$\left\{ \begin{array}{l} \dot{\delta x} = f_x \delta_x + f_m \delta_m \quad (4) \\ \dot{\delta p} = -H_{xx} \delta_x = f_x^T \delta_p - H_{xm} \delta_m \quad (5) \\ \delta H_m = H_{mx} \delta_x + H_{mm} \delta_m + f_m^T \delta_p \quad (6) \end{array} \right.$$

Solving (6) for $\delta m(t)$ gives:

$$\delta m(t) = -H_{mm}^{-1} [-\delta H_m + H_{mx} \delta_x + f_m^T \delta_p] \quad (7)$$

We can now write:

$$\dot{\delta x} = \mathcal{D} \delta_x + \mathcal{E} \delta_p + w_1 \quad (8)$$

$$\dot{\delta p} = \mathcal{L} \delta_x - \mathcal{L}^T \delta_p + w_2 \quad (9)$$

with:

$$\begin{aligned} \mathcal{D} &= f_x - f_m H_{mm}^{-1} H_{mx} \\ \mathcal{E} &= -f_m H_{mm}^{-1} f_m^T \\ \mathcal{L} &= -H_{xx} + H_{xm} H_{mm}^{-1} H_{mx} \\ w_1 &= f_m H_{mm}^{-1} \delta H_m \\ w_2 &= -H_{xm} H_{mm}^{-1} \delta H_m \end{aligned}$$

To solve this problem we use the usual matrix Riccati transformation: we express δp as a function of δx such that (8) and (9) are satisfied.

$$\delta p(t) = T(t) \delta x(t) + h(t) \quad (10)$$

The result of this transformation yields the following equations:

$$\dot{T} = -\mathcal{D}^T T - T \mathcal{D} - T \mathcal{E} T + \mathcal{L} \quad (11)$$

$$T(t_e) = 0$$

$$\dot{h} = -(\mathcal{D}^T + T \mathcal{E}) h - T w_1 + w_2 \quad (12)$$

$$h(t_e) = 0$$

Substituting (10) into (7) gives an equation for δm which will produce a change δH_m in H_m as required.

$$\delta m(t) = -H_{mm}^{-1} \{ [H_{mx} + f_m^T T] \delta x + [-\delta H_m + f_m^T h] \} \quad (13)$$

Because of the boundary conditions, $\dot{x}(t)$ is integrated forward in time while $\dot{p}(t)$, $\dot{T}(t)$, and $\dot{h}(t)$ are integrated backward in time.

By repeating this forward-backward sweep N times we can bring H_m to zero. A reasonable policy is to choose for each step:

$$\delta H_m^{(j)}(t) = -\frac{J}{N} H_m^{(j-1)}(t)$$

where j is the step number.

In this way larger and larger reductions are made with each step, and with the last step the whole remaining correction is made.

APPENDIX II

THE DECOMPOSITION TECHNIQUE

This brief summary and explanation of the decomposition technique for linear quadratic deterministic problems is done in order to precise the method and the notations used in Chapter 4. For more details on the decomposition technique, refer to [3].

The decomposition technique can be presented using a saddle value argument on the variational form of a control problem.

Consider the following system:

$$\begin{cases} \dot{x}_1 = c_{11} x_1 + c_{12} t_2 + l_1 m_1 \\ \dot{x}_2 = c_{21} t_1 + c_{22} x_2 + l_2 m_2 \end{cases}$$

or

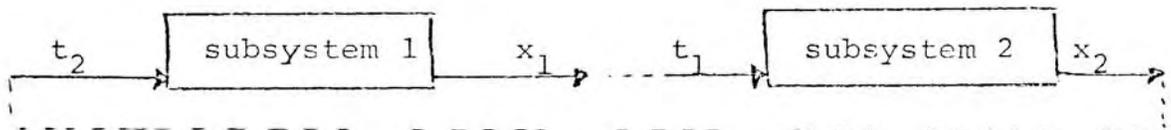
$$\dot{x} = C x + C' t + L m$$

with the following constraints:

$$x_2 = t_2 \quad x_1 = t_1$$

This system can be represented in two ways:

1)



2)



The cost function is:

$$\int_0^t e^{-\rho t} \{ A_1 (r_1 - x_1)^2 + A_2 (r_2 - x_2)^2 + B_1 m_1^2 + B_2 m_2^2 \} dt$$

Proceeding directly to the solution the Lagrangian form for the integrated system is given by:

$$\begin{aligned} J(x_1, x_2, t_1, t_2, m_1, m_2, p_1, p_2, K_1, K_2) = & A_1 (r_1 - x_1)^2 \\ & + A_2 (r_2 - x_2)^2 + B_1 m_1^2 + B_2 m_2^2 + K_1 (x_1 - t_1) + K_2 (x_2 - t_2) \\ & + p_1 [c_{11} x_1 + c_{12} t_2 + l_1 m_1 - \dot{x}_1] + p_2 [c_{21} t_1 + c_{22} x_2 \\ & + l_2 m_2 - \dot{x}_2]. \end{aligned}$$

For this problem it is known that:

$$J(x_1, x_2, t_1, t_2, m_1, m_2, p_1, p_2, K_1, K_2)$$

has a saddle value as follows:

$$J^0 = J [x_1^0, x_2^0, t_1^0, t_2^0, m_1^0, m_2^0, p_1^0, p_2^0, K_1^0, K_2^0] =$$

$$\text{Max} \\ p_1 p_2 K_1 K_2$$

$$\text{Min} \\ x_1 x_2 t_1 t_2 m_1 m_2$$

$$J [x_1, x_2, t_1, t_2, m_1, m_2, p_1, p_2, K_1, K_2].$$

This last equation, together with the separable nature of the problem directly suggests a two-level procedure for the solution:

Level 1:

Given the arbitrary bounded continuous functions $K_1(t), K_2(t), 0 \leq t \leq t_e$, find the optimal solutions $x_1^0(t, K_1, K_2), x_2^0(t, K_1, K_2), t_1^0(t, K_1, K_2), t_2^0(t, K_1, K_2), m_1^0(t, K_1, K_2), m_2^0(t, K_1, K_2)$ which minimize the parametric subproblems subject to the independent subsystems equations.

$$\min_{x_1 x_2 t_1 t_2 m_1 m_2} J[x_1, x_2, t_1, t_2, m_1, m_2] \equiv \min_{x_1, t_2, m_1} J_1 + \min_{x_2, t_1, m_2} J_2.$$

with

$$J_1 = A_1 (r_1 - x_1)^2 + B_1 m_1^2 + K_1 x_1 - K_2 t_2 + p_1 [c_{11} x_1 + c_{12} t_2 + \ell_1 m_1 - \dot{x}_1]$$

and

$$J_2 = A_2 (r_2 - x_2)^2 + B_2 m_2^2 + K_2 x_2 - K_1 t_1 + p_2 [c_{21} t_1 + c_{22} x_2 + l_2 m_2 - \dot{x}_1].$$

Level 2:

Given the optimal solutions from level 1:

$x_1^0(t, K_1, K_2)$, $x_2^0(t, K_1, K_2)$, $m_1^0(t, K_1, K_2)$, $m_2^0(t, K_1, K_2)$, $t_1^0(t, K_1, K_2)$, $t_2^0(t, K_1, K_2)$, find the optimal coordinating functions $K_1^0(t)$, $K_2^0(t)$ which maximize

$$J(K_1, K_2) = J[x_1^0(t, K_1, K_2), x_2^0(t, K_1, K_2), t_1^0(t, K_1, K_2), t_2^0(t, K_1, K_2), m_1^0(t, K_1, K_2), m_2^0(t, K_1, K_2), K_1, K_2].$$

The computation technique for this second level is easy to do:

Consider a perturbation in $K_1(t)$ to $K_1(t) + \delta K_1(t)$, in $K_2(t)$ to $K_2(t) + \delta K_2(t)$.

$$\begin{aligned} \delta J(K_1, K_2) &= \frac{\delta J}{\delta m_1} \delta m_1 + \frac{\delta J}{\delta m_2} \delta m_2 + \frac{\delta J}{\delta x_1} \delta x_1 + \frac{\delta J}{\delta x_2} \delta x_2 \\ &+ \frac{\delta J}{\delta t_1} \delta t_1 + \frac{\delta J}{\delta t_2} \delta t_2 + \frac{\delta J}{\delta K_1} \delta K_1 + \frac{\delta J}{\delta K_2} \delta K_2 + \text{higher order} \\ &\text{term where } \frac{\delta J}{\delta m_1}, \dots \text{ denotes the functional derivatives} \\ &\text{or first derivations.} \end{aligned}$$

But when we solve for the optimal subproblems (1st level) the following conditions are satisfied:

$$\frac{\delta J}{\delta m_1} = \frac{\delta J}{\delta m_2} = \frac{\delta J}{\delta x_1} = \frac{\delta J}{\delta x_2} = \frac{\delta J}{\delta t_1} = \frac{\delta J}{\delta t_2} = 0$$

Therefore, we get:

$$\begin{aligned} \delta J (K_1, K_2) &= \frac{\delta J}{\delta K_1} \delta K_1 + \frac{\delta J}{\delta K_2} \delta K_2 \\ &= (x_1 - t_1) \delta K_1 + (x_2 - t_2) \delta K_2. \end{aligned}$$

Therefore, a gradient method of adjustment for $K_1(t)$, $K_2(t)$ to give steepest ascent is given by:

$$[K_1]_{n+1} = [K_1]_n + \epsilon [x_1 - t_1]$$

$$[K_2]_{n+1} = [K_2]_n + \epsilon [x_2 - t_2].$$

where ϵ is a number chosen small enough to insure correctness of the first order expansion.

APPENDIX III, PROGRAM 1


```

202 H711(T)=C13(T)*C14(T)+C23(T)*C24(T)+
203 (B1(T)+C13(T)+C14(T)+P2(T)+C23(T)+C24(T))*C25(T)+C26(T)+C27(T)+C28(T)+
204 (B1(T)+C13(T)+C14(T)+P2(T)+C23(T)+C24(T))*C29(T)+C30(T)+C31(T)+C32(T)+
205 (B1(T)+C13(T)+C14(T)+P2(T)+C23(T)+C24(T))*C33(T)+C34(T)+C35(T)+C36(T)+
206 H811(T)=P1(T)+C14(T)+C15(T)+C16(T)+C17(T)+C18(T)+C19(T)+C20(T)+C21(T)+C22(T)+
207 +C23(T)+C24(T)+C25(T)+C26(T)+C27(T)+C28(T)+C29(T)+C30(T)+C31(T)+C32(T)+
208 (B1(T)+C14(T)+C15(T)+C16(T)+C17(T)+C18(T)+C19(T)+C20(T)+C21(T)+C22(T)+
209 (B1(T)+C14(T)+C15(T)+C16(T)+C17(T)+C18(T)+C19(T)+C20(T)+C21(T)+C22(T)+
210 H911(T)=P1(T)+C15(T)+C16(T)+C17(T)+C18(T)+C19(T)+C20(T)+C21(T)+C22(T)+
211 (B1(T)+C15(T)+C16(T)+C17(T)+C18(T)+C19(T)+C20(T)+C21(T)+C22(T)+
212 +C23(T)+C24(T)+C25(T)+C26(T)+C27(T)+C28(T)+C29(T)+C30(T)+C31(T)+C32(T)+
213 (B1(T)+C15(T)+C16(T)+C17(T)+C18(T)+C19(T)+C20(T)+C21(T)+C22(T)+
214 G11(T)=C31(T)+C32(T)+C33(T)+C34(T)+C35(T)+C36(T)+C37(T)+C38(T)+
215 G211(T)=C41(T)+C42(T)+C43(T)+C44(T)+C45(T)+C46(T)+C47(T)+C48(T)+
216 G311(T)=C51(T)+C52(T)+C53(T)+C54(T)+C55(T)+C56(T)+C57(T)+C58(T)+
217 ENDS
218 T4K (H011,H211,H311,H411,H511,H611,H711,H811,H911,H011,H11,H211,H311,H411,H511,
219 P23,P41,P55,C33,C34,C35,C43,C44,C45,C46,C47,C48,C49,C53,C54,C55,C611,G211,H011,H11,
220 H311,H411,H511,H611,H711,H811,H911,H011,H11,H211,H311,H411,H511,H611,H711,H811,H911,
221 FOR T=0:1:TF DO WRITE (X1(T),X2(T),X3(T),X4(T),X5(T),X6(T),X7(T),X8(T),X9(T),X0(T))
222 X2(T),X3(T),X4(T),X5(T)) IS
223 COMMENT COMPUTATION OF MINIMUMS
224 FOR T=0:1:TF-1 DO BEGIN
225 TAI(T)=X1(T)+X2(T)+X3(T)+X4(T)+X5(T)+X6(T)+X7(T)+X8(T)+X9(T)+X0(T)+
226 DX3(T)=(X3(T)+1)-X3(T)/X5 (DX4(T)=(X4(T)+1)-X4(T)/X1)
227 DX5(T)=(X5(T)+1)-X5(T)/X5 ENDS
228 DX1(T)=DX1(T)+X1(T)+X2(T)+X3(T)+X4(T)+X5(T)+X6(T)+X7(T)+X8(T)+X9(T)+X0(T)+
229 DX4(T)=DX4(T)+X4(T)+X5(T)+X6(T)+X7(T)+X8(T)+X9(T)+X0(T)+
230 FOR T=0:1:TF DO BEGIN
231 MIN(T)=X1(T)+X2(T)+X3(T)+X4(T)+X5(T)+X6(T)+X7(T)+X8(T)+X9(T)+X0(T)+
232 C15(T)+X5(T)
233 NEN(T)=X2(T)+X3(T)+X4(T)+X5(T)+X6(T)+X7(T)+X8(T)+X9(T)+X0(T)+
234 C25(T)+X5(T)
235 N2N(T)=X3(T)+X4(T)+X5(T)+X6(T)+X7(T)+X8(T)+X9(T)+X0(T)+
236 C35(T)+X5(T)
237 N4N(T)=X4(T)+X5(T)+X6(T)+X7(T)+X8(T)+X9(T)+X0(T)+
238 C45(T)+X5(T)
239 N5N(T)=X5(T)+X6(T)+X7(T)+X8(T)+X9(T)+X0(T)+
240 C55(T)+X5(T)
241 DLEF(T)=X1(T)+X2(T)+X3(T)+X4(T)+X5(T)+X6(T)+X7(T)+X8(T)+X9(T)+X0(T)+
242 +X3(T)+X4(T)+X5(T)+X6(T)+X7(T)+X8(T)+X9(T)+X0(T)+
243 A3(T)=X3(T)+X4(T)+X5(T)+X6(T)+X7(T)+X8(T)+X9(T)+X0(T)+
244 B2(T)=X2(T)+X3(T)+X4(T)+X5(T)+X6(T)+X7(T)+X8(T)+X9(T)+X0(T)+
245 +X5(T)+X6(T)+X7(T)+X8(T)+X9(T)+X0(T)
246 WHITE (MIN(T),NEN(T),N2N(T),N4N(T),N5N(T),DLEF(T))
247 MIN(T),N2N(T),N4N(T),N5N(T),DLEF(T)
248 ENDS

```

END BLOCK 1 LEVEL 1

APPENDIX IV, PROGRAM 2

```

BLOCK 1 LEVEL 1
1 REAL APPAY C11,C12,C21,C22,A1,A2,B1,B2,X1,X2,X10,X20,M1,M2,M10,M20,R1,
2 R2,Z(-1.,.101)S
3 REAL V,T,I,J,E,Y10,Y20
4 PROCFN(FP GLOBAL (C11,C12,C21,C22,A1,A2,B1,B2,R1,R2,Y10,Y20,TF,V,I,X1,X2
BLOCK 2 LEVEL 2
5 *N1,P2)
6 VAL(F C11,C12,C21,C22,A1,A2,B1,B2,R1,R2,Y10,Y20,TF,V,I
7 REAL APPAY C11,C12,C21,C22,A1,A2,B1,B2,X1,X2,M1,M2,P1,R2
8 REAL Y10,Y20,TF,V,I
9 BEGIN OPAL J,E,*
10 REAL APPAY M1,M2,DEL,P1,P2,T11,T12,T21,T22,M1,M2,X1S,X2S(-1.,.101)S
11 FOR T=(0.,1,TF) DO M1(T)=0,M2(T)=0S
12 FOR J=1(1,1+1) DO BEGIN
13 E=-J/TC
14 COMMENT FORWARD INTEGRATIONS
15 FOR T=(0.,1,TF) DO BEGIN
16 X1(0)=Y10S,X2(0)=Y20S
17 X1(T+1)=X1(T)+V*/C11(T)*X1(T)+C12(T)*X2(T)+M1(T) S
18 X2(T+1)=X2(T)+V*/C21(T)*Y1(T)+C22(T)*X2(T)+M2(T) S
19 ENDO
20 CUMMANT MACROBARS INTEGRATION S
21 FOR T=(TF,-1,0) DO BEGIN
22 P1(T)=0S,P2(TF)=0S
23 P1(T-1)=P1(T)-V*/(-2*A1(T)+X1(T)-M1(T))=P1(T)+C11(T)*C1(T)-P2(T)+C21(T) S
24 P2(T-1)=P2(T)-V*/(-2*A2(T)+Y2(T)-R2(T))=P1(T)+C12(T)-P1(T)+C12(T)-P2(T)+C22(T) S
25 M1(T)=0*M1(T)+P1(T) S
26 M2(T)=0*M2(T)+P2(T)+P2(T) S
27 IF J.FO(1+1) THEN GOTO P3S
28 T11(T)=0S,T12(T)=0S,T21(TF)=0S,T22(TF)=0S,M2(TF)=0S
29 T11(T-1)=T11(T)-V*/(-2*C11(T)+T11(T))-C21(T)*T12(T)-C21(T)*T21(T)+
30 T11(T)+T11(T)/(2+H1(T)) +T12(T)*T21(T)/(2*P2(T))-2*A1(T) S
31 T12(T-1)=T12(T)-V*/(-C12(T)+T11(T))-C11(T)+C22(T)*T12(T)-
32 C21(T)*T22(T)+T11(T)+T12(T)/(2*P1(T))+T12(T)+T22(T)/(2*P2(T))
33 T21(T-1)=T21(T)-V*/(-C12(T)+T11(T))-C11(T)+C22(T)*T21(T)-
34 C21(T)*T22(T)+T21(T)+T11(T)/(2*P1(T))+T22(T)+T21(T)/(2*P2(T))
35 T22(T-1)=T22(T)-V*/(-C12(T)+T11(T))-C12(T)*T21(T)-C22(T)*T22(T)+
36 T12(T)+T21(T)/(2+H1(T)) +T22(T)*T22(T)/(2*P2(T))+T22(T)+
37 H1(T-1)=H1(T)-V*/(T11(T)/(2*P1(T))+T22(T)-C11(T)+H1(T)+
38 (T12(T)/(2*P2(T))-C21(T)+H2(T)-T11(T)+H2(T)/(2*P1(T))+2*P1(T))-
39 T12(T)+H2(T)/(2*P2(T))
40 H2(T-1)=H2(T)-V*/(T21(T)/(2*P1(T))-C12(T)+H1(T)+
41 (T22(T)/(2*P2(T))-C22(T)+H2(T)-T21(T)+H2(T)/(2*P1(T))
42 -T22(T)+H2(T)/(2*P2(T)) S

```

```

43 M1(T)=M1(T)+E*HM1(T)/(2*B1(T))-(T11(T)*(X1(T)-X1S(T))+
44 T12(T)*(X2(T)-X2S(T))+H1(T))/(2*B1(T))
45 M2(T)=M2(T)+E*HM2(T)/(2*B2(T))-(T21(T)*(X1(T)-X1S(T))+
46 T22(T)*(X2(T)-X2S(T))+H2(T))/(2*B2(T))
47 X1S(T)=X1(T)*X2S(T)+X2(T)*X1S(T)
48 B3.,FNDE
49 FOR T=(0,1,IF) DO BEGIN
50 DEL(N)=0$
51 DEL(T+1)=DEL(T)+V*(A1(T)*(X1(T)-R1(T)**2)+
52 A2(T)*(X2(T)-R2(T)**2)+B1(T)*M1(T)+B2(T)*M2(T))
53 IF T FOL TF THEN
54 WRITE (,DEL(T),J,T,,DEL(T),J,T)
55 ENDE
56 ENDS
57 FOR T=(0,1,IF) DO
58 WRITE (,HM1(T),HM2(T),DFL(T),T,,HM1(T),HM2(T),DEL(T),T)
59 ENDS
60
61 Y10=5$ Y20=2$
62 TF=10$V=0.01$1=20$
63 FOR T=(0,1,IF) DO BEGIN
64 Z(T)=0$
65 C11(T)=2$
66 C12(T)=2$C21(T)=2$C22(T)=3$
67 A1(T)=10$
68 A2(T)=10$
69 B1(T)=1$
70 B2(T)=1$
71 R1(T)=0$R2(T)=0$
72 ENDS
73 GLOBAL (C11,C12,C21,C22,A1,A2,B1,B2,R1,R2,Y10,Y20,TF,V,I,X10,X20,M10,M20)
74 )$
75 FOR T=(0,1,IF) DO WRITE
76 (,X10(T),X20(T),M10(T),M20(T),T,,X10(T),X20(T),M10(T),M20(T),T)$

```

E4

B5

E5

E2

E1

END BLOCK 2 LEVEL 2

B6

E6

END BLOCK 1 LEVEL 1

COMPLATION COMPLETED IN 8.81 SECONDS

APPENDIX IV, PROGRAM 3

```

BLOCK 1 LEVEL 1
1 REAL ARRAY C11(-1.,101),C12(-1.,101),C21(-1.,101),C22(-1.,101),
2 A1(-1.,101),A2(-1.,101),P1(-1.,101),B2(-1.,101),P1(-1.,101),
3 Z(-1.,101),
4 Z(-1.,101),
5 X10(-1.,101),X20(-1.,101),X1R(-1.,101),X2R(-1.,101),X1(-1.,101),
6 X2(-1.,101),X(-1.,101),
7 M1P(-1.,101),M2P(-1.,101),M1(-1.,101),M2(-1.,101),
8 F(-1.,101),G(-1.,101),
9 P(-1.,101),M1(-1.,101),T1(-1.,101),
10 DEL(-1.,101),DEL0(-1.,101)
11 C2P,C2,
12 C21,C22,M1,M2N,DEL,
13 D1P,D1,D1P,
14 F1,F2,D1,C2,G1,C2,CX1M,CX2K,DEL3(-1.,101)
15 $
16 REAL V,TF,T,I,J,F,Y10,Y20
17 PROCEDURE OPTIMIZATION (C,F,A,B,P,D,G,Y0,TF,V,I,X,M)$
18 $
19 $
20 $
21 $
22 $
23 $
24 $
25 $
26 $
27 $
28 $
29 $
30 $
31 $
32 $
33 $
34 $
35 $
36 $
37 $
38 $
39 $
40 $
41 $
42 $
43 $
44 $
45 $
46 $
47 $
48 $
49 $
50 $
51 $
52 $
53 $
54 $
55 $
56 $
57 $
58 $
59 $
60 $
61 $
62 $
63 $
64 $
65 $
66 $
67 $
68 $
69 $
70 $
71 $
72 $
73 $
74 $
75 $
76 $
77 $
78 $
79 $
80 $
81 $
82 $
83 $
84 $
85 $
86 $
87 $
88 $
89 $
90 $
91 $
92 $
93 $
94 $
95 $
96 $
97 $
98 $
99 $
100 $
101 $
102 $
103 $
104 $
105 $
106 $
107 $
108 $
109 $
110 $
111 $
112 $
113 $
114 $
115 $
116 $
117 $
118 $
119 $
120 $
121 $
122 $
123 $
124 $
125 $
126 $
127 $
128 $
129 $
130 $
131 $
132 $
133 $
134 $
135 $
136 $
137 $
138 $
139 $
140 $
141 $
142 $
143 $
144 $
145 $
146 $
147 $
148 $
149 $
150 $
151 $
152 $
153 $
154 $
155 $
156 $
157 $
158 $
159 $
160 $
161 $
162 $
163 $
164 $
165 $
166 $
167 $
168 $
169 $
170 $
171 $
172 $
173 $
174 $
175 $
176 $
177 $
178 $
179 $
180 $
181 $
182 $
183 $
184 $
185 $
186 $
187 $
188 $
189 $
190 $
191 $
192 $
193 $
194 $
195 $
196 $
197 $
198 $
199 $
200 $
201 $
202 $
203 $
204 $
205 $
206 $
207 $
208 $
209 $
210 $
211 $
212 $
213 $
214 $
215 $
216 $
217 $
218 $
219 $
220 $
221 $
222 $
223 $
224 $
225 $
226 $
227 $
228 $
229 $
230 $
231 $
232 $
233 $
234 $
235 $
236 $
237 $
238 $
239 $
240 $
241 $
242 $
243 $
244 $
245 $
246 $
247 $
248 $
249 $
250 $
251 $
252 $
253 $
254 $
255 $
256 $
257 $
258 $
259 $
260 $
261 $
262 $
263 $
264 $
265 $
266 $
267 $
268 $
269 $
270 $
271 $
272 $
273 $
274 $
275 $
276 $
277 $
278 $
279 $
280 $
281 $
282 $
283 $
284 $
285 $
286 $
287 $
288 $
289 $
290 $
291 $
292 $
293 $
294 $
295 $
296 $
297 $
298 $
299 $
300 $
301 $
302 $
303 $
304 $
305 $
306 $
307 $
308 $
309 $
310 $
311 $
312 $
313 $
314 $
315 $
316 $
317 $
318 $
319 $
320 $
321 $
322 $
323 $
324 $
325 $
326 $
327 $
328 $
329 $
330 $
331 $
332 $
333 $
334 $
335 $
336 $
337 $
338 $
339 $
340 $
341 $
342 $
343 $
344 $
345 $
346 $
347 $
348 $
349 $
350 $
351 $
352 $
353 $
354 $
355 $
356 $
357 $
358 $
359 $
360 $
361 $
362 $
363 $
364 $
365 $
366 $
367 $
368 $
369 $
370 $
371 $
372 $
373 $
374 $
375 $
376 $
377 $
378 $
379 $
380 $
381 $
382 $
383 $
384 $
385 $
386 $
387 $
388 $
389 $
390 $
391 $
392 $
393 $
394 $
395 $
396 $
397 $
398 $
399 $
400 $
401 $
402 $
403 $
404 $
405 $
406 $
407 $
408 $
409 $
410 $
411 $
412 $
413 $
414 $
415 $
416 $
417 $
418 $
419 $
420 $
421 $
422 $
423 $
424 $
425 $
426 $
427 $
428 $
429 $
430 $
431 $
432 $
433 $
434 $
435 $
436 $
437 $
438 $
439 $
440 $
441 $
442 $
443 $
444 $
445 $
446 $
447 $
448 $
449 $
450 $
451 $
452 $
453 $
454 $
455 $
456 $
457 $
458 $
459 $
460 $
461 $
462 $
463 $
464 $
465 $
466 $
467 $
468 $
469 $
470 $
471 $
472 $
473 $
474 $
475 $
476 $
477 $
478 $
479 $
480 $
481 $
482 $
483 $
484 $
485 $
486 $
487 $
488 $
489 $
490 $
491 $
492 $
493 $
494 $
495 $
496 $
497 $
498 $
499 $
500 $
501 $
502 $
503 $
504 $
505 $
506 $
507 $
508 $
509 $
510 $
511 $
512 $
513 $
514 $
515 $
516 $
517 $
518 $
519 $
520 $
521 $
522 $
523 $
524 $
525 $
526 $
527 $
528 $
529 $
530 $
531 $
532 $
533 $
534 $
535 $
536 $
537 $
538 $
539 $
540 $
541 $
542 $
543 $
544 $
545 $
546 $
547 $
548 $
549 $
550 $
551 $
552 $
553 $
554 $
555 $
556 $
557 $
558 $
559 $
560 $
561 $
562 $
563 $
564 $
565 $
566 $
567 $
568 $
569 $
570 $
571 $
572 $
573 $
574 $
575 $
576 $
577 $
578 $
579 $
580 $
581 $
582 $
583 $
584 $
585 $
586 $
587 $
588 $
589 $
590 $
591 $
592 $
593 $
594 $
595 $
596 $
597 $
598 $
599 $
600 $
601 $
602 $
603 $
604 $
605 $
606 $
607 $
608 $
609 $
610 $
611 $
612 $
613 $
614 $
615 $
616 $
617 $
618 $
619 $
620 $
621 $
622 $
623 $
624 $
625 $
626 $
627 $
628 $
629 $
630 $
631 $
632 $
633 $
634 $
635 $
636 $
637 $
638 $
639 $
640 $
641 $
642 $
643 $
644 $
645 $
646 $
647 $
648 $
649 $
650 $
651 $
652 $
653 $
654 $
655 $
656 $
657 $
658 $
659 $
660 $
661 $
662 $
663 $
664 $
665 $
666 $
667 $
668 $
669 $
670 $
671 $
672 $
673 $
674 $
675 $
676 $
677 $
678 $
679 $
680 $
681 $
682 $
683 $
684 $
685 $
686 $
687 $
688 $
689 $
690 $
691 $
692 $
693 $
694 $
695 $
696 $
697 $
698 $
699 $
700 $
701 $
702 $
703 $
704 $
705 $
706 $
707 $
708 $
709 $
710 $
711 $
712 $
713 $
714 $
715 $
716 $
717 $
718 $
719 $
720 $
721 $
722 $
723 $
724 $
725 $
726 $
727 $
728 $
729 $
730 $
731 $
732 $
733 $
734 $
735 $
736 $
737 $
738 $
739 $
740 $
741 $
742 $
743 $
744 $
745 $
746 $
747 $
748 $
749 $
750 $
751 $
752 $
753 $
754 $
755 $
756 $
757 $
758 $
759 $
760 $
761 $
762 $
763 $
764 $
765 $
766 $
767 $
768 $
769 $
770 $
771 $
772 $
773 $
774 $
775 $
776 $
777 $
778 $
779 $
780 $
781 $
782 $
783 $
784 $
785 $
786 $
787 $
788 $
789 $
790 $
791 $
792 $
793 $
794 $
795 $
796 $
797 $
798 $
799 $
800 $
801 $
802 $
803 $
804 $
805 $
806 $
807 $
808 $
809 $
810 $
811 $
812 $
813 $
814 $
815 $
816 $
817 $
818 $
819 $
820 $
821 $
822 $
823 $
824 $
825 $
826 $
827 $
828 $
829 $
830 $
831 $
832 $
833 $
834 $
835 $
836 $
837 $
838 $
839 $
840 $
841 $
842 $
843 $
844 $
845 $
846 $
847 $
848 $
849 $
850 $
851 $
852 $
853 $
854 $
855 $
856 $
857 $
858 $
859 $
860 $
861 $
862 $
863 $
864 $
865 $
866 $
867 $
868 $
869 $
870 $
871 $
872 $
873 $
874 $
875 $
876 $
877 $
878 $
879 $
880 $
881 $
882 $
883 $
884 $
885 $
886 $
887 $
888 $
889 $
890 $
891 $
892 $
893 $
894 $
895 $
896 $
897 $
898 $
899 $
900 $
901 $
902 $
903 $
904 $
905 $
906 $
907 $
908 $
909 $
910 $
911 $
912 $
913 $
914 $
915 $
916 $
917 $
918 $
919 $
920 $
921 $
922 $
923 $
924 $
925 $
926 $
927 $
928 $
929 $
930 $
931 $
932 $
933 $
934 $
935 $
936 $
937 $
938 $
939 $
940 $
941 $
942 $
943 $
944 $
945 $
946 $
947 $
948 $
949 $
950 $
951 $
952 $
953 $
954 $
955 $
956 $
957 $
958 $
959 $
960 $
961 $
962 $
963 $
964 $
965 $
966 $
967 $
968 $
969 $
970 $
971 $
972 $
973 $
974 $
975 $
976 $
977 $
978 $
979 $
980 $
981 $
982 $
983 $
984 $
985 $
986 $
987 $
988 $
989 $
990 $
991 $
992 $
993 $
994 $
995 $
996 $
997 $
998 $
999 $
1000 $

```

```

03 D(T)*X(T)*X(T)+C(T)*X(T) )S
04 IF T EQ 1 THEN WRITE ('DEL(T),J,T,DEL(T),J,T) )S
05 ENDS
06 ENDS
07 FOR T=(0,1,IF) DO
08 WRITE ('M(T),C1(T),T,M(T),DEL(T),T) )S
09 IF T EQ 1 THEN WRITE ('DEL(T),Y,DEL(T),T) )S
10 ENDS
11 Y10=55*Y20=25
12 T=10*V=0*015
13 I=75
14 FOR T=(0,1,IF) DO BEGIN
15 Z(T)=R5
16 C1(T)=25
17 C2(T)=25
18 A1(T)=105
19 A2(T)=105
20 P1(T)=15
21 P2(T)=25
22 ENDS
23 CURRENT COMPUTATION OF X10*Y20 )S
24 FOR T=(0,1,IF) DO BEGIN
25 X1P(T)=0*2*2(T)=05
26 ENDS
27 CURRENT COMPUTATION OF Y10*Y20 )S
28 FOR T=(0,1,IF) DO BEGIN
29 X1R10=X105
30 X1R20=X20 )S
31 X1R(T)=X1R10+X1R20*(C1(T)+X1R(T)+C12(T)+X2P(T)+X1R(T))
32 X2P(T)=X1R(T)+X1R20*(C2(T)+X1P(T)+C22(T)+X2P(T)+X2R(T))
33 C1(T)=05
34 DEL(X1)=DEL(X1)+X1R(T)+X1R20*(C1(T)+X1R(T)+C12(T)+X2P(T)+X1R(T))
35 A2(T)=X2R(T)-X1R(T)+X2P(T)+X2R(T)+X1R(T)+X1R20*(C2(T)+X1P(T)+C22(T)+X2P(T)+X2R(T))
36 C2(T)=X2P(T)+X2R(T)+X1R(T)+X1R20*(C2(T)+X1P(T)+C22(T)+X2P(T)+X2R(T))
37 X1P(T)=X2P(T)+X2R(T)+X1R(T)+X1R20*(C2(T)+X1P(T)+C22(T)+X2P(T)+X2R(T))
38 ENDS
39 FOR T=(0,1,IF) DO BEGIN
40 F1(T)=C12(T)+X2-C15
41 C1(T)=C2(T)+C21(T)+C21(T) )S
42 IF T EQ 1 THEN
43 C2P(T)=X2M(T)+X2P(T)+V
44 C2R(T)=X2M(T)+X2P(T)+V
45 C2P(T)=X2M(T)+X2P(T)+V
46 G1(T)=X2M(T)+X2P(T)+X2R(T)+C22(T)+X2P(T) )S
47 ENDS
48 OPTIMIZATION (C1(T)+F1+X1P1+01*DI+G1+Y10*F1+V+I+X1+M1) )S
49 FOR T=(0,1,IF) DO WRITE
50 ('X2P(T),M1(T),V1(T),T,DX2R(T),M1(T),X1(T),T) )S
51 FOR T=(0,1,IF) DO BEGIN
52 F2(T)=C21(T)+X1(T) )S

```

```

96 O2(T)=B1(T)*C12(T)*C12(T) S
97 IF T LSS TF THEN
98 OX1(T)=(X1(T)+1)-X1(T)/V S
99 OX1(T)=OX1(T)*C11(T) S
100 G2(T)=2*B1(T)*C12(T)*OX1(T)-C11(T)*X1(T) S
101 ENDS
102 OPTIMIZATION (C22*F2+A2*B2*R2*O2+G2*Y20*TF+V*I*X2*M2)S
103 FOR T=0:1:TF DO WRITE
104 (OX1(T),X2(T),M2(T),T,OX1R(T),X2(T),M2(T),T)S
105 FOR T=(0:1:TF) DO BEGIN
106 DEL3(0)=0S
107 DEL3(T+1)=DEL3(T)
108 +V*(A1(T)*(X1(T)-R1(T))*X1(T)-R1(T))+
109 A2(T)*X2(T)-R2(T))*X2(T)-R2(T)
110 +B1(T)*M1(T)*M1(T)+P2(T)*M2(T)*M2(T) IS
111 WRITE (X1(T),X2(T),M1(T),M2(T),DEL3(T),T)S
112 X1(T),X2(T),M1(T),M2(T),DEL3(T) IS
113 ENDS
114 COMMENT COMPUTATION OF MINIM2NS
115 FOR T=(0:1:TF) DO BEGIN
116 IF T LSS TF THEN
117 OX1(T)=(X1(T)+1)-X1(T)/V S
118 OX1(T)=OX1(T)*C11(T)S
119 IF T LSS TF THEN
120 OX2(T)=(X2(T)+1)-X2(T)/VS
121 OX2(T)=OX2(T)*C12(T)S
122 MIN(T)=OX1(T)-C11(T)*OX1(T)-C12(T)*OX2(T) S
123 M2N(T)=OX2(T)-C22(T)*OX2(T)-C21(T)*OX1(T)S
124 DELF(0)=0S
125 DELF(T+1)=DELF(T)+ V*(A1(T)*(X1(T)-R1(T))*X1(T)-R1(T) +
126 A2(T)*X2(T)-R2(T))*X2(T)-R2(T)
127 +B1(T)*M1N(T)*M1N(T)+
128 WRITE (MIN(T),M2N(T),X1(T),X2(T),DELF(T),T)S
129 MIN(T),M2N(T),X1(T),X2(T),DELF(T),T) S
130 ENDS
131 FOR T=(0:1:TF) DO BEGIN
132 O1R(0)=0S
133 O1R(T+1)=O1R(T)+V*(A1(T)*(X1(T)-R1(T))*X1(T)-R1(T))+
134 A2(T)*X2R(T)-R2(T))*X2R(T)-R2(T) +B1(T)*(M1(T)*X1(T)-
135 C12(T)*X2R(T))*M2(T)+B2(T)*(OX2R(T)-C21(T)*X1(T)-C22(T)*X2R(T))*M2 ) S
136 O1(0)=0S
137 O2(0)=0S
138 O2(T+1)=O2(T) +V*(A2(T)*(X2(T)-R2(T))*M2(T)+B1(T)*
139 C12(T)*X2(T)-R2(T))*X2(T)-R2(T)+B2(T)*(OX2(T)-C21(T)*X1(T)-C11(T)*X1(T))
140 +B2(T)*(OX2(T)-C22(T)*X2(T)-C21(T)*X1(T))*M2) S
141 O2R(0)=0S
142 O2R(T+1)=O2R(T)+V*(A2(T)*(X2R(T)-R2(T))*M2(T)+
143 B1(T)*C12(T)*X2R(T)-R2(T))*X2R(T)+B2(T)*
144 2*C12(T)*X2M(T)+OX1(T)-C11(T)*X1(T))+B2(T)*((
145 OX2R(T)-C22(T)*X2R(T)-C21(T)*X1(T))*M2) ) S
146 O1R(0)=0S
147 O1(T+1)=O1(T)+ V*(A1(T)*(X1(T)-R1(T))*M2(T)+
148 B2(T)*C21(T)*X1(T)-C21(T)*X1(T)-
149 2*C21(T)+OX2R(T)+C22(T)*X2R(T))*X1(T)+ B1(T)*(OX1(T)-

```

```
150 C11(T)=X1(T)-C1(T)*X2R(T)**2) )S
151 Q1R(T)=Q1R(T)+V*(A1(T)*(X1R(T)-R1(T))**2)+
152 B2(T)*(C21(T)-C21(T)*X1P(T)+X1D(T)-2*C21(T)*(DX2P(T)-C22(T)+X2R(T))*X1R(
153 T)) +Q1(T)*I*P(T)**2))S
154 ENDS
155 FOR T=(0+1,IF) DO WRITE
156 (*D12R(T),D1R(T),U1(T),D2P(T),D2(T),T,*,D12R(T),Q1R(T),Q1(T),Q2R(T),Q2(T)
157 )S
```

END

END_RLÜCK 1 LEVEL 1

APPENDIX IV, PROGRAM 4

```

1 REAL ARRAY C11,C12,C21,C22,D11,D12,D21,D22,A1,A2,B1,B2,R1,R2,Z,X10,X20,
2 M10,
3 X1R,X2R,X1,X2,X,M1R,M2R,M1,M2,MIN,M2N,F,G,D1,D2,F1,F2,K11,K12,K21,K22,
4 K31,K32,K41,K42,G1,G2,DX1,DX2,DEL0,C1R,C2R,CX1R,DX2R(-1..101) $
5 REAL V,TF,I,J,F,Y10,Y20 $
6 PROCEDURE OPTIMIZATION (C,D,F,A,B,R,K1,K2,K3,K4,G,Y0,TF,V,I,X,M,M10)$
7 VALUE C,D,F,A,B,R,K1,K2,K3,K4,G,Y0,TF,V,I,M10$
8 REAL ARRAY C,D,F,A,B,R,K1,K2,K3,K4,G,X,M,M10 $
9 REAL Y0,TF,V,I $
10 BEGIN REAL J,E,T $
11 REAL ARRAY HM,DEL,P,T1,H1,XS(-1..101) $
12 FOR T=(0,1,TF) DO M(T)=M10(T) $
13 FOR J=(1,1,1+1) DO BEGIN
14 E=-J/IF
15 COMMENT FORWARDS INTEGRATION $
16 FOR T=(0,1,TF) DO BEGIN
17 X(0)=Y0$
18 X(T+1)=X(T)+V*(C(T)*X(T)+D(T)*X(T)*X(T)+M(T)+F(T)) $
19 ENDS
20 COMMENT BACKWARDS INTEGRATION $
21 FOR T=(0,1,TF) DO BEGIN P(TF)=0$
22 P(T-1)=P(T)-V*(-2*A(T)*X(T)-R(T))-K1(T)-2*K2(T)*X(T)-3*K3(T)*X(T)*X(T)
23 -4*K4(T)*X(T)*X(T)*X(T)-P(T)*C(T)-2*P(T)*D(T)*X(T) $
24 H1(T)=R(T)*M(T)+P(T)$
25 IF J.FOL(I+1) THEN GOTO R3 $
26 T1(TF)=0$H1(TF)=0$
27 T1(T-1)=T1(T)-V*(-2*(C(T)+2*D(T)*X(T))*T1(T)+T1(T)*T1(T)/(2*B(T))
28 -2*A(T)-2*K2(T)-6*K3(T)*X(T)-12*K4(T)*X(T)*X(T)-2*P(T)*C(T) ) $
29 H1(T-1)=H1(T)-V*(-(C(T)+2*D(T)*X(T))-T1(T)/(2*B(T)))*H1(T)-
30 T1(T)*E*HM(T)/(2*B(T)) $
31 M(T)=M(T)+(E*HM(T)-(T1(T)*X(T)-XS(T))+H1(T))/(2*B(T)) $
32 XS(T)=X(T)$
33 B3=ENDS
34 FOR T=(0,1,TF) DO BEGIN DEL(0)=0$
35 DEL(T+1)=DEL(T)+V*(A(T)*X(T)+R(T))*2)+B(T)*M(T)+K1(T)*X(T)+
36 K2(T)*X(T)*X(T)+K3(T)*X(T)*X(T)*X(T)+K4(T)*X(T)*X(T)*X(T)+G(T) $
37 IF T.FOL(TF) THEN
38 WRITE ('DEL(T),J,T',DEL(T),J,T) $
39 ENDS
40 ENDS
41 FOR T=(0,1,TF) DO
42 WRITE ('HM(T),DEL(T),T',HM(T),DEL(T),T) $

```

```

43      END%
44      Y10=55Y20*2
45      TF=10*re105*U*ni$
46      FOR T=(0,1,IF) NO BEGIN
47      Z(T)=0%
48      C1(T)=2%
49      C12(T)=10%
50      C21(T)=15%
51      C22(T)=35
52      A1(T)=10%
53      A2(T)=10%
54      B1(T)=1%
55      B2(T)=1%
56      R1(T)=0%$H2(T)=0%
57      D1(T)=0%
58      D12(T)=0%
59      C21(T)=0%
60      C22(T)=0%
61      END%
62      COMMENT COMPUTATION OF MIP*X2K      S
63      FOR T=(0,1,IF) NO BEGIN
64      MIP(T)=100%*2R(T)=100%
65      ENDS
66      COMMENT COMPUTATION OF XIP*X2K      S
67      FOR T=(0,1,IF) NO BEGIN
68      XIP(0)=Y10$
69      X2R(0)=Y20%
70      XIP(T+1)=XIP(T)+V*(C11(T)+XIP(T)+C12(T))*X2R(T)+MIP(T)+
71      D11(T)+XIP(T)+XIP(T)+C12(T)*X2R(T)+X2R(T)
72      X2R(T+1)=X2R(T)+V*(C21(T)+XIP(T)+C22(T))*X2R(T)+
73      D21(T)+XIP(T)+XIP(T)+C22(T)*X2R(T)+X2R(T)
74      DEL(0)=0%
75      DEL(T+1)=DEL(T)+V*(A1(T)+XIP(T)+XIP(T)+X2R(T)+
76      A2(T)+X2R(T)+C2(T)+X2R(T)+B1(T)+MIP(T)+MIP(T)+B2(T)+
77      WRITE (XIP(T),X2R(T),MIP(T),X2R(T),DEL(T),T)
78      XIP(T),X2R(T),MIP(T),X2R(T),DEL(T),T)
79      ENDS
80      FOR T=(0,1,IF) NO SFGIN
81      F1(T)=C12(T)*X2R(T)+C12(T)*X2R(T)+X2R(T)      S
82      IF T LSS TF THEN
83      OX2R(T)=X2R(T+1)-X2R(T)/V      S
84      IF T EOL TF THEN
85      OX2R(T)=OX2R(T*-1)
86      K1(T)=2*B2(T)+C21(T)+C22(T)+OX2R(T)-C22(T)*X2R(T)+X2R(T)      S
87      K21(T)=2*(C21(T)+C21(T)-2*O21(T)+OX2R(T)-O22(T)*X2R(T)+X2R(T)
88      -C22(T)*X2R(T))
89      K31(T)=2*B2(T)+C21(T)+O21(T)+
90      K41(T)=2*(Y10*O21(T)+C21(T)
91      G1(T)=
92      ((OX2R(T)-O22(T)+X2R(T))*X2R(T)-C22(T)*X2R(T))*2)      S
93      ENDS
94      FOR T=(0,1,IF) NO WRITE
95      ((O1(T)+F1(T)+M11(T)+K21(T)+K31(T)+K41(T)+G1(T),
96      O11(T)+E1(T)+M11(T)+K21(T)+K31(T)+K41(T)+G1(T)      )S

```

```

06 OPTIMIZATION (C11+D11*F1+A1*B1+R1*K11+K21+K31+K41+G1+Y10*TF+V1*X1+M1+M1
07 R1)S
08 FOR T=(0,1,TF) DO WRITE
09 (DX2R(T)+M1*TF,X1(T)+T*,DX2R(T),M1(T),X1(T),T) S
100 FOR T=(0,1,TF) DO BEGIN
101 F2(T)=C21(T)*X1(T)+C21(T)*X1(T)+S
102 IF T LSS TF THEN
103 DX1(T)=(X1(T)+1)-X1(T)/V S
104 IF T EOL TF THEN
105 DX1(T)=DX1(TF+1) S
106 K12(T)=2*B1(T)+C12(T)+C11(T)*DX1(T)-D11(T)*X1(T)+X1(T)*X1(T) S
107 K22(T)=B1(T)*C12(T)+C12(T)*C12(T)-2*D12(T)*X1(T)+D11(T)*X1(T)*X1(T)-
108 C11(T)*X1(T) S
109 K32(T)=2*B1(T)+C12(T)+C12(T) S
110 K42(T)=B1(T)+D12(T)+D12(T) S
111 G2(T)=(DX1(T)-C11(T)*X1(T)+X1(T)*X1(T)-C11(T)*X1(T))**2 S
112 ENDS
113 OPTIMIZATION (C22+D22*F2+A2*B2+R2*K12+K22+K32+K42+G2+Y20*TF+V1*X2+M2+M2
114 R1)S
115 FOR T=(0,1,TF) DO WRITE
116 (DX1(T)+X2(T)+M2(T)+T*,DX1(T)+X2(T)+M2(T),T) S
117 COMMENT COMPUTATION OF MIN1+M2S
118 FOR T=(0,1,TF) DO BEGIN
119 IF T LSS TF THEN
120 DX1(T)=(X1(T)+1)-X1(T)/V S
121 IF T EOL TF THEN
122 DX1(T)=DX1(TF+1)S
123 IF T LSS TF THEN
124 DX2(T)=(X2(T)+1)-X2(T)/V S
125 IF T EOL TF THEN
126 DX2(T)=DX2(TF+1) S
127 WRITE (X1(T)+DY1(T)+X2(T)+DX2(T)+X1(T)*DX1(T)+X2(T)*DX2(T) )S
128 MIN(T)=X1(T)-C11(T)*X1(T)-C12(T)*X2(T)-D11(T)*X1(T)*X1(T) S
129 -D12(T)+X2(T)*X2(T) S
130 M2N(T)=X2(T)-C11(T)*X1(T)-C22(T)*X2(T)-D21(T)*X1(T)*X1(T)
131 -D22(T)+X2(T)*X2(T) S
132 DELF (N1)=0'S
133 DELF (T+1)=DELFF(T)+V*(A1(T)*X1(T)+D1(T)*X1(T)+M2(T)+A2(T)*X2(T)-R2(T))**2)
134 +B1(T)*MIN(T)+M1N(T)+R2(T)+M2N(T)+M2N(T) S
135 WRITE (MIN(T)+M1N(T)+M2N(T)+X1(T)+X2(T)+DELFF(T),T),*
136 MIN(T)+M2N(T)+X1(T)+X2(T)+DELFF(T)+T S
137 ENDS
138 FOR T=(0,1,TF) DO BEGIN
139 Q1R(N1)=M5Q2M(N1)=0'S
140 Q1R(T+1)=Q1R(T)+V*(A1(T)*X1R(T)+M1R(T)-R1(T))**2) +
141 B1(T)*MIN(T)+M1R(T)+M2R(T)+X1(T)*X1R(T)+X1R(T)+X1R(T)*X1R(T)
142 +K31(T)*X1R(T)+X1R(T)*X1R(T)+X1R(T)+X1R(T)+X1R(T)+X1R(T)
143 +G1(T) S
144 Q2R(T+1)=Q2M(T)+V*(A2(T)+X2R(T)-R2(T))**2)+B2(T)+M2R(T)
145 +K12(T)+X2R(T)+X22(T)+X2R(T)+K32(T)+X2R(T)+X2R(T)+X2R(T)
146 +K42(T)+X2R(T)+X2R(T)+X2R(T)+X2R(T)+G2(T) S
147 WRITE (Q1R(T)+Q2R(T)+T*,Q1R(T),Q2R(T),T) S
148 ENDS
149 END ALUCK 1 LEVEL 1

```

APPENDIX IV, PROGRAM 5

```

B0
BLOCK 1      LEVEL 1
1  REAL  V,TF,I,I,J,E,X10,X20,X30,X40,X50,N,M
2  COM1,COM2,COM3,COM4,COM5,COMT,E0,E5$
3  REAL ARRAY  C1,C12,C13,C14,C15,C21,C22,C23,C24,C25,
4  S11,
5  M1,M2,M3,M4,M5,
6  C31,C32,C33,C34,C35,C41,C42,C43,C44,C45,
7  C51,C52,C53,C54,C55,A1,A2,A3,A4,A5,B1,B2,B3,B4,B5,
8  R1,R2,R3,R4,R5,X12,X22,X32,X42,X52,MIN,M2N,M3N,M4N,M5N,
9  X11,X21,X31,X41,X51,X11,X21,X31,X41,X51,M1R,M2R,M3R,M4R,M5R,
10 HNE1,HNE2,HME3,HME4,HME5,
11 X1R,X2R,X3R,X4R,X5R,O,DFLR(-1,101)$
12 PROCEDURE SVP (A11,A21,A31,A41,A51,R11,B21,B31,B41,B51,C111,C121,C131,
13 C141,C151,C211,C221,C231,C241,C251,C311,C321,C331,C341,C351,C411,
14 C421,C431,C441,C451,C511,C521,C531,C541,C551,R11,R21,R31,R41,R51,Y1,
15 Y2,Y3,Y4,Y5,M11,M21,M31,M41,M51,Y10,Y20,Y30,Y40,Y50,TF,V,I,S11)$
16 VALUE  A11,A21,A31,A41,A51,B11,B21,B31,B41,B51,
17 C111,C121,C131,C141,C151,C211,C221,C231,C241,C251,C311,C321,C331,
18 C341,C351,C411,C421,C431,C441,C451,C511,C521,C531,C541,C551,
19 R11,R21,R31,R41,R51,Y2,Y3,Y4,Y5,Y10,Y20,Y30,Y40,Y50,S11,
20 TF,V,I,$
21 REAL ARRAY,
22 A11,A21,A31,A41,A51,B11,B21,B31,B41,B51,
23 C111,C121,C131,C141,C151,C211,C221,C231,C241,C251,C311,C321,C331,
24 C341,C351,C411,C421,C431,C441,C451,C511,C521,C531,C541,C551,
25 R11,R21,R31,R41,R51,Y2,Y3,Y4,Y5,
26 S11,
27 Y1,M1,M21,M31,M41,M51$
28 REAL TF,V,I,Y10,Y20,Y30,Y40,Y50
29 BEGIN PFAL J,E,T
30 REAL ARRAY  DY2,DY3,DY4,DY5,HM1,T1,H1,DELL,P1,YIS(-1,101)$
31 FOR T=(0,1,TF) NO M11(T)=S11(T)$
32 FOR T=(0,1,TF-1) DO PFGIN
33 DY2(T)=(Y2(T+1)-Y2(T))/V$DY3(T)=(Y3(T+1)-Y3(T))/V$
34 DY4(T)=(Y4(T+1)-Y4(T))/V$DY5(T)=(Y5(T+1)-Y5(T))/V$ENDS
35 DY2(TF)=DY2(TF-1)$DY3(TF)=DY3(TF-1)$DY4(TF)=DY4(TF-1)$DY5(TF)=DY5(TF-1)$
36 FOR J=(1,1,1) NO BEGIN
37 E=-J/T$
38 COMMENT FORWARD INTEGRATIONS
39 FOR T=(0,1,TF) NO BFGIN
40 Y1(0)=V/0$
41 Y1(T+1)=Y1(T)+V*(C111(T)+Y1(T)+C121(T)+Y2(T)+C131(T)+Y3(T)+
42 C141(T)+Y4(T)+C151(T)+Y5(T)+M11(T))$

```

B1

B2
E2

B3

B4

```

43 M21(T)=Y2(T)-C21(T)*Y1(T)-C221(T)*Y2(T)-C231(T)*Y3(T)
44 -C241(T)*Y4(T)-C251(T)*Y5(T)
45 M31(T)=Y3(T)-C311(T)*Y1(T)-C321(T)*Y2(T)-C331(T)*Y3(T)
46 -C341(T)*Y4(T)-C351(T)*Y5(T)
47 M41(T)=Y4(T)-C411(T)*Y1(T)-C421(T)*Y2(T)-C431(T)*Y3(T)
48 -C441(T)*Y4(T)-C451(T)*Y5(T)
49 M51(T)=Y5(T)-C511(T)*Y1(T)-C521(T)*Y2(T)-C531(T)*Y3(T)
50 -C541(T)*Y4(T)-C551(T)*Y5(T)
51 ENDS
52 COMMENT BACKWARDS INTEGRATION 5
53 FOR T=TF1-I*0) DO BEGIN
54 P1(TF)=05
55 P1(T-I)=P1(T)+V*(2*M11(T)*Y1(T)-R11(T)-2*B21(T)*C211(T)*M21(T)
56 -2*B31(T)*C311(T)*M31(T)-2*B41(T)*C411(T)*M41(T)-
57 2*B51(T)*C511(T)*M51(T)+P1(T)*C11(T))
58 H1(T)=2*B11(T)*M11(T)+P1(T)
59 IF J.FOL (I+1) THEN GOTC K2 5
60 T1(TF)=05H1(TF)
61 T1(T-I)=T1(T)-V*(-2*C111(T)*T1(T)+T1(T)*T1(T)/(2*B11(T))-
62 (2*A11(T)+2*B21(T)*C211(T)-C211(T)+2*B41(T)*C411(T)+
63 2*B31(T)*C311(T)+2*B51(T)*C511(T))
64 H1(T-I)=H1(T)-V*(-C111(T)-T1(T)/(2*B11(T))*H1(T)-T1(T)*F*M11(T)/(2*B11(
65 T)))
66 M11(T)=M11(T)+E*M11(T)/(2*B11(T))-(T1(T)*Y1(T)-V15(T))+H1(T)/(2*B11(T)
67 )
68 V15(T)=Y1(T)
69 K2=ENDS
70 FOR T=(0+1,IF) DO BEGIN
71 DELI(0)=05
72 DELI(T+1)=DELI(T)+V*(A11(T)*Y1(T)-R11(T))*2)+A21(T)*Y2(T)-
73 A31(T)*Y3(T)+A31(T)*Y3(T)-R31(T)+2*B41(T)*C411(T)+
74 A51(T)*Y5(T)-R51(T))*2)+B11(T)*M11(T)+
75 B21(T)*M21(T)+P31(T)+B31(T)*M31(T)+B41(T)*M41(T)+
76 B51(T)*M51(T)+M11(T))
77 IF T.FOL THEN WRITE
78 (DELI(T),T,J,I,DELI(T),T,J)
79 ENDS
80 ENDS
81 FOR T=(0+1,IF) DO WRITE
82 (M11(T),J,T,M11(T),J,T)
83 ENDS
84 I=I+5
85 V=0.0015X10=25X0=3EX40=05X50=63TF=105
86 FOR T=(0+1,IF) DO BEGIN
87 A1(T)=A2(T)+A3(T)+A4(T)+A5(T)=15A5(T)=15B1(T)=25B2(T)=25B3(T)=15
88 B4(T)=15P5(T)=15
89 C11(T)=15C12(T)=25C13(T)=05C14(T)=55
90 C21(T)=0.15C22(T)=0.25C23(T)=15C24(T)=85C25(T)=05
91 C31(T)=0.15C32(T)=0.25C33(T)=35C34(T)=0.45C35(T)=0.55
92 C41(T)=0.85C42(T)=0.75C43(T)=0.65C44(T)=0.95C45(T)=05
93 C51(T)=105C52(T)=125C53(T)=45C54(T)=55C55(T)=25
94 S1(T)=105P2(T)=05B2(T)=305B4(T)=05B5(T)=505
95 ENDS

```

E4

B5

FR

E5

B6

E6

E3

E1

END BLOCK 2 LEVEL 2

B7

E7

```

96 COMMENT STEP 0 COMPUTATION OF A REFERENCE CONTROL S
97 FOR T=(0,1,TF) DO BEGIN
98 M1R(T)=1005*2R(T)*=-1005*3R(T)=1005*4R(T)=-1005*5R(T)=1005
99 ENDS
100
101 COMMENT STEP 0 COMPUTATION OF A REFERENCE TRAJECTORY S
102 FOR T=(0,1,TF) DO BEGIN
103 X1R(0)=X10*X2R(0)=X20*X3P(0)=X30*X4R(0)=X40*X5R(0)=X50$
104 X1R(T)=X14(X1(T)+V*(C11(T)*X1P(T)+C12(T)*Y2R(T)+C13(T)*X3R(T)+
105 C14(T)*X4R(T)+C15(T)*X5P(T)+M1R(T))$
106 X2R(T)=X28(T)+V*(C21(T)*X1R(T)
107 +C22(T)*X2R(T)+
108 C23(T)*X3R(T)+C24(T)*X4P(T)+C25(T)*X5R(T)+M2R(T))$
109 X3R(T)=X33(T)+V*(C31(T)*X1R(T)+C32(T)*X2R(T)+C33(T)*X3R(T)+
110 C34(T)*X4R(T)+C35(T)*X5P(T)+M3R(T))$
111 X4R(T)=X48(T)+V*(C41(T)*X1R(T)+C42(T)*X2R(T)+C43(T)*X3P(T)+
112 C44(T)*X4R(T)+C45(T)*X5P(T)+M4R(T))$
113 X5R(T)=X54(T)+V*(C51(T)*X1R(T)+C52(T)*X2R(T)+
114 C53(T)*X3R(T)+C54(T)*X4P(T)+C55(T)*X5R(T)+M5R(T))$
115 DELR(0)=0$
116 DELR(T)=DELR(T)+V*(A1(T)*X1R(T)-R1(T))+A2(T)*X2R(T)-R2(T))+A2
117 +A3(T)*X3R(T)-P3(T))+A4(T)*X4R(T)-R4(T))+A2
118 +A5(T)*X5R(T)-P5(T))+R1(T)+M1R(T)+M2R(T)+M2R(T)+
119 B3(T)+M3P(T)+B4(T)+M4P(T)+M4P(T)+M5P(T)+M5R(T))$
120 WRITE ((T),X1P(T),X2P(T),X3P(T),X4R(T),X5R(T),M1R(T),M2R(T),M3R(T),
121 M4R(T),M5R(T),DELR(T))$
122 T,X1R(T),X2R(T),X3R(T),X4R(T),X5R(T),M1R(T),M2R(T),M3R(T),M4R(T),M5R(T),
123 DELR(T))$
124 ENDS
125 W=5$
126
127 FOR T=(0,1,TF) DO BEGIN
128 X11(T)=X1R(T)+X21(T)=X2R(T)+X31(T)=X3R(T)+X41(T)=X4P(T)+X51(T)=X5R(T)$
129 M1(T)=M1R(T)+M2(T)=M2R(T)+M3(T)=M3R(T)+M4(T)=M4P(T)+M5(T)=M5R(T)$
130 ENDS
131 FOR N=(1,*) DO BEGIN
132 WRITE (N,STEP1,N)$
133 E0=CLOCK$
134
135 SVP (A1,A2,A3,A4,A5,B1,P2,B3,B4,P5,C11,C12,C13,C14,C15,C21,C22,C23,C24,
136 C25,C31,C32,C33,C34,C35,C41,C42,C43,C44,C45,C51,C52,C53,C54,C55,
137 R1,R2,P3,R4,R5,V12,X21,X31,Y41,X51,M1,M2,M3,M4,M5,
138 X10,X20,X30,X40,X50,TF,V,N,C11)$
139 E5=CLOCK$
140 CCM1=FS-FUS
141
142 FOR T=(0,1,TF) DO WRITE (M1(T),M2(T),M3(T),M4(T),M5(T))$,
143 M1(T),M2(T),M3(T),M4(T),M5(T))$
144 WRITE (N,STEP2,N)$
145 FOR T=(0,1,TF) DO S11(T)=P2(T)$
146 E0=CLOCK$
147
148 SVP (A2,A3,A4,A5,A6,A7,B2,B3,B4,B5,B1,B2,C22,C23,C24,C25,C21,
149 C32,C33,C34,C35,C31,C42,C43,C44,C45,C41,C52,C53,C54,C55,C51,C12,C13,C14,
150 C15,C11,A2,M3,R4,P5,R1,X22,Y31,X41,X51,X12,M2,M3,M4,M5,
151 M1,X20,X30,X40,X50,X10,TF,V,I,S11)$
152 E5=CLOCK$
153 CCM2=FS-FUS
154
155 FOR T=(0,1,TF) DO WRITE (M1(T),M2(T),M3(T),M4(T),M5(T))$,

```

B8
E8

B9

U

E9

B10

F10

B11

```

150 M1(T),M2(T),M3(T),M4(T),M5(T))$
151 WRITE (N,STEP 3,'N')$
152 FOR T=(0,1,TF) DO S11(T)=M3(T)$
153 EO=CLOCKS$
154 SVP (A3,A4,A5,A1,A2,B3,R4,B5,B1,B2,C33,C34,C35,C31,C32,
155 C43,C44,C45,C41,C42,C53,C54,C55,C51,C52,C13,C14,C15,C11,C12,C23,C24,C25,
156 C21,C22,R3,M4,R1,R2,X32,Y41,X51,X12,X22,M3,M4,M5,M1,M2,X30,X40,
157 X50,X10,X20,TF,V,I,S11)$
158 E5=CLOCKS$
159 COM3=EE-F05
160 FOR T=(0,1,TF) DO WRITE (M1(T),M2(T),M3(T),M4(T),M5(T),'',
161 M1(T),M2(T),M3(T),M4(T),M5(T))$
162 WRITE (N,STEP 4,'N')$
163 FOR T=(0,1,TF) DO S11(T)=M4(T)$
164 EO=CLOCKS$
165 SVP (A4,A5,A1,A2,A3,B4,B5,B1,B2,B3,C44,C45,C41,C42,C43,
166 C54,C55,C51,C52,C53,C14,C15,C11,C12,C13,C24,C25,C21,C22,C23,
167 C34,C35,C31,C32,C33,R4,P5,R1,R2,R3,X42,X51,X12,X22,X32,
168 M4,M5,M1,M2,M3,Y40,X50,X10,X20,X30,TF,V,I,S11)$
169 E5=CLOCKS$
170 COM4=EE-F05
171 WRITE (N,STEP 5,'N')$
172 FOR T=(0,1,TF) DO S11(T)=M5(T)$
173 EO=CLOCKS$
174 SVP (A5,A1,A2,A3,A4,B5,B1,B2,B3,B4,C55,C51,C52,C53,C54,
175 C15,C11,C12,C13,C14,C25,C21,C22,C23,C24,
176 C35,C41,C32,C33,C34,
177 C45,C41,C42,C43,C44,R5,R1,R2,R3,R4,X52,
178 X12,X22,X32,X42, M5N,M1N,M2N,M3N,M4N,X50,X10,X20,X30,X40,TF,V,I,S11)$
179 E5=CLOCKS$
180 COM5=EE-F05
181 FOR T=(0,1,TF) DO BEGIN
182 X21(T)=X22(T)$X31(T)=X32(T)$X41(T)=X42(T)$X51(T)=X52(T)$
183 END$
184 FOR T=(0,1,TF) DO WRITE
185 (T,X12(T),X22(T),X32(T),X42(T),X52(T),M1N(T),M2N(T),M3N(T),M4N(T),M5N(T)
186 ),',',
187 T,X12(T),X22(T),X32(T),X42(T),X52(T),M1N(T),M2N(T),M3N(T),M4N(T),M5N(T)
188 ))$
189 COMT=COM1+COM2+COM3+COM4+COM5$
190 WRITE (1,2,3,4,5,TOT,'COM1,COM2,COM3,COM4,COM5,COMT)$
191 ENDS

```

b12
e12
u

b11
END BLOCK 1 LEVEL 1

APPENDIX V, PROGRAM 6


```

44 M1(T)=M1(T)+0.5*F*HM1(T)-0.5*(T11(T)*(X1(T)-X1S(T))+
45 T12(T1)*(X2(I)-X2S(I)) +H1(I))
46 M2(T)=M2(T)+0.5*F*HM2(T)-0.5*(T21(T)*(X1(T)-X1S(T))
47 +T22(T)*(X2(I)-X2S(I)) +H2(I))
48 X1S(T)=X1(T)*S X2S(T)=X2(T)*S
49 B3=END$
50 IF ( T EQL 6 ) AND ( J EQL 7 ) THEN FOR T=(0,1,TF) DO WRITE
51 (X1(T),X2(I),M1(T),M2(T),DEL(T),HM1(T),HM2(T),T),
52 X1(T),X2(T),M1(T),M2(T),DEL(T),HM1(T),HM2(T),T)*S
53 ENDS
54 WRITE (CLOCK)*S
55 ET=CLOCK*5
56 TIME=FT-ET*5
57 WRITE (COMPUTING TIME, TIME )$
58 END*

```

```

END_BLOCK_1 LEVEL_1

```

APPENDIX V, PROGRAM 7

```

1 COMMENT DETERMINISTIC PROBLEM DECOMPOSITION METHOD $
2 REAL T,FT,B1,T1,F1,F,V1,J,F,N,R,EPS $
3 REAL ARRAY X1,X2,T1,T2,M1,M2,X1S,X2S,HM1,HM2,HT1,HT2,P1,P2,T11,T22,
4 H1,H2,K1,K2,DEL(=1..10)S
5 N=1+EPS=0.65
6 I=75
7 TF=50*N=0.0015
8 WRITE (CLOCK)S
9 BT=CLOCK$
10 FOR I=(0,1,IF) DO BEGIN
11 K1(T)=X2(T)=X1(T)*X2(T)=M1(T)=M2(T)=T1(T)=T2(T)=0$SENDS
12 FOR P=(1,1,N) DO BEGIN
13 WRITE ('STEP')S
14 COMMENT COORDINATION $
15 FOR T=(0,1,IF) DO BEGIN
16 K1(T)=X1(T)+EPS*(X1(T)-T1(I)) $
17 K2(T)=X2(T)+EPS*(X2(T)-T2(T)) $
18 ENDS
19 FOR J=(1,1,I+1) DO BEGIN
20 E=J/I$
21 COMMENT SUBSYSTEM1 $
22 COMMENT FORWARDS INTEGRATION $
23 FOR T=(0,1,IF) DO BEGIN
24 X1(0)=5$
25 X1(T+1)=X1(T)+V*(X1(T)+T2(T)+M1(T))$
26 ENDS
27 COMMENT BACKWARDS INTEGRATION $
28 FOR T=(T,1,0) DO BEGIN
29 P1(T)=0$
30 P1(T)=P1(T)+V*(X1(T)-T/1000+P1(T))+K1(T) $
31 H1(T)=2*M1(T)+P1(T)$
32 H2(T)=T2(T)-2*T/1000+P1(T)-K2(T) $
33 IF J=0 (I+1) THEN GOTO P35
34 T1(T)=0.5*H1(T)=0$
35 T1(T)=T1(T)+V*(2*M1(T)-3*T1(T)+T11(T)/2+1) $
36 H1(T)=H1(T)+V*(1-T)/2)*H1(T)+(0.5*E*H1(T)+E*HT2(T))*T11(T))$
37 M1(T)=X1(T)+0.5*E*H1(T)-0.5*(T1(T)-X1(T)-X1S(T))+M1(T) $
38 T2(T)=T2(T)+E*HT2(T)-(T11(T)+X1(T)-X1S(T))+H1(T) $
39 X1S(T)=X1(T)S
40 B3=E*NS
41 COMMENT SUB SYSTEM 2$
42 FOR T=(0,1,IF) DO BEGIN
43 X2(0)=2$

```

```

44 X2(T+1)=X2(T)+V*(T1(T)+X2(T)+M2(T))$
45 ENDS
46 COMMENT BACKWARDS INTEGRATION $
47 FOR T=(TF,1,0) DO BEGIN
48 P2(TF)=0$
49 P2(T-1)=P2(T)+V*(X2(T)-2*T/1000+P2(T))+K2(T)) $
50 H2(T)=2*M2(T)+P2(T)$
51 H1(T)=T1(T)-T/1000+P2(T)-K1(T) $
52 IF J EOL (I+1) THEN GOTO B4$
53 T2(TF)=0$H2(TF)=0$
54 T2(T-1)=T2(T)+V*(2*T2(T)-3*T2(T)/2+1) $
55 H2(T-1)=H2(T)+V*(1-3*T2(T)/2)*H2(T)+T22(T)*E*HM2(T)+E*HT1(T))$
56 M2(T)=M2(T)+0.5*F*HM2(T)-0.5*(T2(T)-X2S(T))+H2(T) $
57 T1(T)=T1(T)+E*HT1(T)-(T2(T)-X2S(T))+H2(T)) $
58 X2S(T)=X2(T)$
59 B4 ENDS
60 IF ( P FOL N )AND ( J EOL 7) THEN
61 FOR T=(0,1,IF) DO BEGIN
62 WRITE
63 (H21(T),HM2(T),HT1(T),HT2(T),X1(T),T1(T),X2(T),M1(T),M2(T),
64 H1(T),H2(T),HT1(T),HT2(T),X1(T),T1(T),X2(T),M1(T),M2(T) )$
65 ENDS
66 ENDS
67 WRITE (CLOCK)$
68 ET=CLOCKS
69 TIME=FT-BT$
70 WRITE ('COMPUTING TIME',TIME )$
71 ENDS

```

APPENDIX V, PROGRAM 8

```

B0
BLOCK 1 LEVEL 1
1 REAL TF=1,GE,T,ET,BT,TIME,01,02,W1,W2 ,V,EL,E2,E3
2 REAL ARRAY, I11(-1.,1.,111),I22(-1.,111),I33(-1.,111),I44(-1.,111),
3 DEL,
4 I15(-1.,111),I21(-1.,111),I22(-1.,111), I23(-1.,111),I24(-1.,111),
5 I25(-1.,111),I31(-1.,111),I32(-1.,111),I33(-1.,111),I34(-1.,111),
6 I35(-1.,111),I41(-1.,111),I42(-1.,111),I43(-1.,111),I44(-1.,111),
7 I45(-1.,111),I51(-1.,111),I52(-1.,111),I53(-1.,111),I54(-1.,111),
8 I55(-1.,111),I61(-1.,111),I62(-1.,111),I63(-1.,111),I64(-1.,111),
9 H5(-1.,111),V1(-1.,111),V2(-1.,111),V12(-1.,111),M1(-1.,111),
10 M2(-1.,111),P1(-1.,111),P2(-1.,111),P3(-1.,111),P4(-1.,111),P5(-1.,111),
11 X1(-1.,111),X11(-1.,111),S1(-1.,111),S2(-1.,111),L1(-1.,111),
12 L2(-1.,111),V10(-1.,111),V20(-1.,111),V120(-1.,111),M10(-1.,111),
13 M20(-1.,111),F2(-1.,111)
14 $
15 I=205
16 WRITE (NUMBER OF CONVERGENCE ITERATIONS,I) $
17 COMMENT INTEGRATED PROBLEM $
18 TF=505
19 V=0.0015
20 V1=0.15,W2=0.15,Q1=0.15,Q2=0.15 $
21 FOR T=(0,1,TF) DO F2(T)=T $
22 FOR T=(0,1,TF) DO BFGN_L1(T)=0.00045L2(T)=0.0006*0.015 ENDS
23 FOR T=(0,1,TF) DO X1(T)=105
24 BT=CLOCK-SWRITE(-BT,F,BT) $
25 E2=BTS
26 FOR J=(1,1,1) DO BEGIN
27 E=J/I
28 COMMENT FORWARD INTEGRATION OF V1,V2,V12,M1,M2 $
29 FOR T=(0,1,TF) DO BFGN
30 V1(T)=V1(T)+V*(Q1-V1(T)+V1(T)/W1-V12(T)*V12(T)/W2)S
31 V2(T+1)=V2(T)+V*(2*V12(T)+Q2-V12(T)+V12(T)/W1-V2(T)*V2(T)/W2)S
32 V12(T+1)=V12(T)+V*(V1(T)-V1(T)-V1(T)*V12(T)/W1-V2(T)*V12(T)/W2)S
33 M1(T+1)=M1(T)+V*(X1(T)-V1(T)+M1(T)/W1-V12(T)*M2(T)/W2+V1(T)*L1(T)/W1
34 +V12(T)*L2(T)/W2)S
35 M2(T+1)=M2(T)+V*(M1(T)-V12(T)*M1(T)/W1-V2(T)*M2(T)/W2
36 +V12(T)*L1(T)/W1+V2(T)*L2(T)/W2)S
37 ENDS
38 COMMENT BACKWARD INTEGRATION OF P1,P2,P3,P4,P5 $
39 FOR T=(TF,-1,0) DO PEGIN
40 P1(TF)=P2(TF)+P3(TF)+P4(TF)+P5(TF)+H1(TF)+H2(TF)+H3(TF)+H4(TF)+H5(TF)+05
41 P1(T-1)=P1(T)+V*(0.5-P2(T)+V1(T)+P3(T)-P3(T)*V12(T)/W1
42 -P4(T)+M1(T)/W1+P4(T)*L1(T)/W1)S

```

158



04 -T24(T)*T44(T))\$
 09 -T25(T)-1)*T25(T)+V*(
 100 -2*V2(T)*T25(T)/W2 -V12(T)*T35(T)/W2 +S2(T)*T55(T)
 101 -V12(T)*T24(T)/W2-V2(T)*T25(T)/W2
 102 -T24(T)*T45(T)-P5(T)/W2)\$
 103 -T31(T)-1)*T31(T)+V*(
 104 -2*V12(T)*T11(T)/W2+2*(1-V12(T)/W1)*T21(T)+(-V1(T)/W1-V2(T)/W2)*T31(T)
 105 +S2(T)*T41(T)+S1(T)*T51(T)
 106 -2*V1(T)*T31(T)/W1+1-V12(T)/W1)*T33(T)+S1(T)*T30(T)
 107 -T34(T)*T41(T)-P3(T)/W1)\$
 108 -T32(T)-1)*T32(T)+V*(
 109 -2*V12(T)*T12(T)/W2+2*(1-V12(T)/W1)*T22(T)+(-V1(T)/W1-V2(T)/W2)*T32(T)
 110 +S2(T)*T42(T)+S1(T)*T52(T)
 111 -2*V2(T)*T32(T)/W2-V12(T)*T33(T)/W2+S2(T)*T35(T)
 112 -T34(T)*T42(T)-P3(T)/W2)\$
 113 -T33(T)-1)*T33(T)+V*(
 114 -2*V12(T)*T13(T)/W2+2*(1-V12(T)/W1)*T23(T)+(-V1(T)/W1-V2(T)/W2)*T33(T)
 115 +S2(T)*T43(T)+S1(T)*T53(T)
 116 -2*V12(T)*T31(T)/W2+2*(1-V12(T)/W1)*T32(T)+(-V1(T)/W1-V2(T)/W2)*T33(T)
 117 +S2(T)*T34(T)+S1(T)*T35(T)
 118 -T34(T)*T43(T)-P3(T)/W2)\$
 119 -T34(T)-1)*T34(T)+V*(
 120 -2*V12(T)*T14(T)/W2+2*(1-V12(T)/W1)*T24(T)+(-V1(T)/W1-V2(T)/W2)*T34(T)
 121 +S2(T)*T44(T)+S1(T)*T54(T)
 122 -V1(T)*T34(T)/W1+(1-V12(T)/W1)*T35(T)
 123 -T34(T)*T44(T)-P5(T)/W1)\$
 124 -T35(T)-1)*T35(T)+V*(
 125 -2*V12(T)*T15(T)/W2+2*(1-V12(T)/W1)*T25(T)+(-V1(T)/W1-V2(T)/W2)*T35(T)
 126 +S2(T)*T45(T)+S1(T)*T55(T)
 127 -V12(T)*T34(T)/W2-V2(T)*T35(T)/W2
 128 -T34(T)*T45(T)-P4(T)/W2)\$
 129 -T41(T)-1)*T41(T)+V*(
 130 -V1(T)*T41(T)/W1+(1-V12(T)/W1)*T51(T)
 131 -2*V1(T)*T41(T)/W1+(1-V12(T)/W1)*T43(T)+S1(T)*T40(T)
 132 -T44(T)*T41(T)-P4(T)/W1)\$
 133 -T42(T)-1)*T42(T)+V*(
 134 -V1(T)*T42(T)/W1+(1-V12(T)/W1)*T52(T)
 135 -2*V2(T)*T42(T)/W2-V12(T)*T43(T)/W2+S2(T)*T45(T)
 136 -T44(T)*T42(T))\$
 137 -T43(T)-1)*T43(T)+V*(
 138 -V1(T)*T43(T)/W1+(1-V12(T)/W1)*T53(T)
 139 -2*V12(T)*T41(T)/W2+2*(1-V12(T)/W1)*T42(T)+(-V1(T)/W1-V2(T)/W2)*T43(T)
 140 +S2(T)*T44(T)+S1(T)*T45(T)
 141 -T44(T)*T43(T)-P5(T)/W1)\$
 142 -T44(T)-1)*T44(T)+V*(
 143 -V1(T)*T44(T)/W1+(1-V12(T)/W1)*T54(T)
 144 -V1(T)*T44(T)/W1+(1-V12(T)/W1)*T45(T)
 145 -T44(T)*T44(T)+)\$
 146 -T45(T)-1)*T45(T)+V*(
 147 -V1(T)*T45(T)/W1+(1-V12(T)/W1)*T55(T)
 148 -V12(T)*T44(T)/W2-V2(T)*T45(T)/W2
 149 -T44(T)*T45(T))\$
 150 -T51(T)-1)*T51(T)+V*(
 151 -V12(T)*T41(T)/W2-V2(T)*T51(T)/W2


```
206 J,T,HX1(T),M1(T),M2(T),V1(T),V2(T))$  
207 ENDS  
208 ET=CLOCKSWRITE(,ET,,ET)$  
209 TIME=ET-RTS  
210 WRITE(,COMPUTING TIME,,TIME) S
```

E2

END BLOCK-1 LEVEL 1

APPENDIX V, PROGRAM 9


```

b5 K1(T)=K1(T)+EPS*(V1(T)+V1(T)+V1(T)+V1(T)+V1(T)+V1(T))$
b6 K2(T)=K2(T)+EPS*(VV2(T)+VV2(T)+VV2(T)+VV2(T)+VV2(T))$
b7 K3(T)=K3(T)+EPS*(M1(T)+M1(T)+M1(T)+M1(T))$
b8 K4(T)=K4(T)+EPS*(MM2(T)+MM2(T)+MM2(T)+MM2(T))$
b9 ENDS
b10 FOR J=(1+1+1) DO BEGIN
b11 WRITE ('ITJ',ITJ)
b12 SUM1=0$
b13 E=J/15
b14 COMMENT FORWARD INTEGRATION OF SUB PROBLEM 1
b15 FOR T=(0+1+TF) DO BEGIN
b16 V1(T)=0$V121(T)=0$M1(T)=0$
b17 V1(T+1)=V1(T)+V*(A1-V1(T)+V1(T)/W1-V121(T)/W1+V121(T)/W2)
b18 V121(T+1)=V121(T)+V*(V1(T)-V1(T)+V121(T)/W1-V121(T)/W2)
b19 M1(T+1)=M1(T)+V*(X1(T)-M1(T)+M1(T)/W1+M1(T)/W2)
b20 ENDS
b21 COMMENT BACKWARDS INTEGRATION OF SUB PROBLEM 1
b22 FOR T=(TF+1+0) DO BEGIN
b23 P1(T)=P1(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b24 P2(T)=P2(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b25 P3(T)=P3(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b26 P4(T)=P4(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b27 P5(T)=P5(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b28 P6(T)=P6(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b29 P7(T)=P7(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b30 P8(T)=P8(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b31 P9(T)=P9(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b32 P10(T)=P10(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b33 P11(T)=P11(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b34 P12(T)=P12(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b35 P13(T)=P13(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b36 P14(T)=P14(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b37 P15(T)=P15(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b38 P16(T)=P16(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b39 P17(T)=P17(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b40 P18(T)=P18(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b41 P19(T)=P19(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b42 P20(T)=P20(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b43 P21(T)=P21(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b44 P22(T)=P22(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b45 P23(T)=P23(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b46 P24(T)=P24(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b47 P25(T)=P25(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b48 P26(T)=P26(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b49 P27(T)=P27(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b50 P28(T)=P28(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b51 P29(T)=P29(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b52 P30(T)=P30(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b53 P31(T)=P31(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b54 P32(T)=P32(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b55 P33(T)=P33(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b56 P34(T)=P34(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b57 P35(T)=P35(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b58 P36(T)=P36(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b59 P37(T)=P37(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b60 P38(T)=P38(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b61 P39(T)=P39(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b62 P40(T)=P40(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b63 P41(T)=P41(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b64 P42(T)=P42(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b65 P43(T)=P43(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b66 P44(T)=P44(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b67 P45(T)=P45(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b68 P46(T)=P46(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b69 P47(T)=P47(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b70 P48(T)=P48(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b71 P49(T)=P49(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b72 P50(T)=P50(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b73 P51(T)=P51(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b74 P52(T)=P52(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b75 P53(T)=P53(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b76 P54(T)=P54(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b77 P55(T)=P55(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b78 P56(T)=P56(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b79 P57(T)=P57(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b80 P58(T)=P58(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b81 P59(T)=P59(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b82 P60(T)=P60(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b83 P61(T)=P61(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b84 P62(T)=P62(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b85 P63(T)=P63(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b86 P64(T)=P64(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b87 P65(T)=P65(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b88 P66(T)=P66(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b89 P67(T)=P67(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b90 P68(T)=P68(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b91 P69(T)=P69(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b92 P70(T)=P70(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b93 P71(T)=P71(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b94 P72(T)=P72(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b95 P73(T)=P73(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b96 P74(T)=P74(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b97 P75(T)=P75(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b98 P76(T)=P76(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b99 P77(T)=P77(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b100 P78(T)=P78(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b101 P79(T)=P79(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b102 P80(T)=P80(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b103 P81(T)=P81(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b104 P82(T)=P82(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b105 P83(T)=P83(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b106 P84(T)=P84(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b107 P85(T)=P85(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b108 P86(T)=P86(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b109 P87(T)=P87(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b110 P88(T)=P88(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b111 P89(T)=P89(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b112 P90(T)=P90(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b113 P91(T)=P91(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b114 P92(T)=P92(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b115 P93(T)=P93(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b116 P94(T)=P94(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b117 P95(T)=P95(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b118 P96(T)=P96(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b119 P97(T)=P97(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b120 P98(T)=P98(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b121 P99(T)=P99(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+
b122 P100(T)=P100(T)+V*(U+5-2*P1(T)+V1(T)/W1+P2(T))*(1-V121(T)/W1)+

```



```

151 (T31(T)*V1(T)-V10(T)+T22(T)+V121(T)-V1210(T))+T33(T)*V1(T)-V10(T))
152 +T3(T))
153 V2(T)+V22(T)+(E+V22(T)+P2(T)+V121(T)-V1210(T))/W2+
154 V121(T)*(T21(T)+(V1(T)-V10(T))+T22(T)+V121(T)-V1210(T))+T23(T)*V1(T))
155 +T10(T)+T2(T))/W2)/(2*W2(T))
156 P2(T)+V22(T)+P2(T)+(V121(T)-V1210(T))/W2+
157 (T31(T)*V1(T)-V10(T)+T22(T)+V121(T)-V1210(T))+T33(T)*V1(T)-V10(T))
158 +T3(T)+2*V121(T)/W2
159 IF J FOL 1 THEN BEGIN V10(T)=0;V1210(T)=0;V10(T)=0;END
160 ELSE BEGIN
161 M10(T)=M1(T)*V1210(T)+V121(T)*V10(T)=V1(T)*
162 ENDS
163 E1=ENDS
164 COMMENT FORWARD INTEGRATION OF SUE PROBLEM 2
165 FOR T=(0.1*TF) DO BEGIN
166 V2(T)=0;V122(T)=0;P2(T)=0
167 V2(T+1)=V2(T)+W*(2*V122(T)+W2-V122(T)+V122(T)/W1-V2(T)+V2(T)/V2(T))
168 V122(T+1)=V122(T)+W*(V1(T)-V10(T)+V122(T)/W1-V2(T)+V2(T)/V2(T))
169 M2(T+1)=M2(T)+W*(M1(T)-V122(T)+M1(T)/W1-V2(T)+V2(T)/V2(T))
170 V122(T)+L1(T)/W1+V2(T)+V2(T)/W2(T))
171 ENDS
172 COMMENT BACKWARDS INTEGRATION OF SUE PROBLEM 2
173 FOR T=(TF-1.0) DO BEGIN
174 V1(T)=0;T2(T)=0;T3(T)=0
175 V1(T-1)=V1(T)+W*(0.5+2*V1(T)+V2(T)/W2-0.5*(V122(T)/W2-0.5*(V122(T)/W2+
176 +3*(T-1)*L2(T)/W2-2*P2(T)+V2(T))
177 Q2(T-1)=Q2(T)+W*(2*Q1(T)-2*Q1(T)+V122(T)/W1-C2(T)+V1(T)/W1
178 -C2(T)+V2(T)/W2-0.5*(T-1)*L1(T)/W1
179 Q3(T-1)=Q3(T)+W*(0.5+P2(T)-P2(T)+V2(T)-0.5*(V122(T)/W2-0.5*(V122(T)/W2+
180 +3*(T-1)*L2(T)/W2-2*P2(T)+V2(T))
181 P2(T)=0.5*P1(T)+0.5*(T-1)-V122(T)/W1-V2(T)
182 IF J LSS 1 THEN SUM1=0
183 IF J FOL 1 THEN
184 BEGIN
185 SUM1=SUM1+V1(T)-P1(T)+2*V1(T)-V1(T)+2*(P2(T)-P1(T)+V2(T))
186 (V2(T)-V22(T))+W2
187 IF T FOL 0 THEN WRITE (*SUE2**SUM1)
188 IF T FOL 50 THEN WRITE (*SUM1**SUM1)
189 IF J GTP (1-1) AND SUM1 LSS 0.01 AND
190 MIN(M1(T)) GTP -0.001 AND MAX(P1(T)) LSS 0.001 AND MIN(P1(T))
191 GTR -0.001
192 THEN BEGIN
193 FOR T=(TF-5.0) DO WRITE
194 (P1(T)+P22(T)+V22(T)+V2(T)+V1(T)+P1(T)+P2(T)+V2(T)+V1(T)+P1(T)+P2(T))
195 FOR T=(TF-5.0) DO WRITE
196 (P1(T)+P22(T)+V22(T)+V2(T)+V1(T)+P1(T)+P2(T)+V2(T)+V1(T)+P1(T)+P2(T))
197 FOR T=(TF-5.0) DO WRITE
198 (P1(T)+P22(T)+V22(T)+V2(T)+V1(T)+P1(T)+P2(T)+V2(T)+V1(T)+P1(T)+P2(T))
199 FOR T=(TF-5.0) DO WRITE
200 (SUM1+P1(T)+V1(T)+P2(T)+V2(T)+SUM1+P1(T)+V1(T)+P2(T)+V2(T))
201
202 GOTO P4SEND5
203 IF J FOL (1+1) THEN GOTO B2
204 P11(T)=0;P12(T)=0;P13(T)=0
205 P21(T)=0;P22(T)=0;P23(T)=0

```

09 c4

b10
b10
e8

b11

c11

b12

b13

c13

b14

p4
p4

c14

405 P31(TF)*P32(TF)*P33(TF)*Q3
406 H1(TF)*H2(TF)*H3(TF)*Q3
407 S1(T)*H1(T)/K1+L1(T)/K15
408 S2(T)*H2(T)/K2+L2(T)/K25
409 P1(T-1)*P11(T)+V*(
410 -2*V2(T)*P11(T)/K2-V124(T)*P21(T)/K2+S2(T)*P31(T)
411 -2*V2(T)*P11(T)/K2-V122(T)*P12(T)/K2+S2(T)*P31(T)
412 P12(T)*((1-V122(T)/K1)**2)*P21(T)/(2*K1(T))
413 -2*P13(T)*((1-V122(T)/K1)**2)*P31(T)
414 -2*P1(T)/K2-2*K2(T)5
415 P12(T-1)*P12(T)+V*(
416 -2*V2(T)*P12(T)/K2-V124(T)*P24(T)/K2+S2(T)*P24(T) +
417 3*(1-V122(T)/K1)*P11(T)+(-VV1(T)/K1-V2(T)/K2-Q2(T)*((1-V122(T)/K1)
418 /2*K1(T)/K1)*P12(T)+((S1(T)-2*Q3(T)*((1-V122(T)/K1)/K1)*P13(T)
419 +P12(T)*((1-V122(T)/K1)**2)*P22(T)/(2*K1(T))-2*P13(T)*((1-V122(T)/K1)**2)*P31(T)
420)*P32(T)
421 -Q2(T)/K25
422 P13(T-1)*P13(T)+V*(
423 -2*V2(T)*P13(T)/K2-V122(T)*P23(T)/K2+S2(T)*P23(T)
424 -V2(T)*P13(T)/K2
425 +P12(T)*((1-V122(T)/K1)**2)*P23(T)/(2*K1(T))-2*P13(T)*((1-V122(T)/K1)**2)*P31(T)
426)*P33(T)
427 -Q3(T)/K25
428 P21(T-1)*P21(T)+V*(
429 2*(1-V122(T)/K1)*P11(T)+(-VV1(T)/K1-V2(T)/K2-
430 K1)*P21(T) +((S1(T)-2*Q3(T)*((1-V122(T)/K1)/K1)*P21(T)
431 -2*V2(T)*P21(T)/K2-V124(T)*P22(T)/K2+S2(T)*P23(T)
432 +((1-V122(T)/K1)**2)*P22(T)+P21(T)/(2*K1(T))-
433 2*P23(T)*((1-V122(T)/K1)**2)*P31(T)
434 -Q2(T)/K25
435 P22(T-1)*P22(T)+V*(
436 2*(1-V122(T)/K1)*P12(T)+(-VV1(T)/K1-V2(T)/K2-
437 K1)*P22(T) +((S1(T)-2*Q3(T)*((1-V122(T)/K1)/K1)*P22(T)
438 +((1-V122(T)/K1)*P21(T)+(-VV1(T)/K1-V2(T)/K2-Q2(T)*((1-V122(T)/K1)
439 /2*K1(T))*P22(T)+((S1(T)-2*Q3(T)*((1-V122(T)/K1)/K1)*P23(T)
440 +((1-V122(T)/K1)**2)*P22(T)+P22(T)/(2*K1(T))-
441 2*P23(T)*((1-V122(T)/K1)**2)*P31(T)
442 -2*Q1(T)/K1+Q2(T)/K2*(1-V122(T)/K1)*K1**2)*P31(T)
443 -2*Q1(T)/K1+Q2(T)/K2*(1-V122(T)/K1)*K1**2)*P31(T)
444 -2*Q1(T)/K1+Q2(T)/K2*(1-V122(T)/K1)*K1**2)*P31(T)
445 -2*Q1(T)/K1+Q2(T)/K2*(1-V122(T)/K1)*K1**2)*P31(T)
446 2*(1-V122(T)/K1)*P13(T)+(-VV1(T)/K1-V2(T)/K2-
447 K1)*P23(T) +((S1(T)-2*Q3(T)*((1-V122(T)/K1)/K1)*P23(T)
448 -V2(T)*P23(T)/K2
449 +((1-V122(T)/K1)**2)*P23(T)+P23(T)/(2*K1(T))-
450 2*P23(T)*((1-V122(T)/K1)**2)*P33(T)5
451 P31(T-1)*P31(T)+V*(
452 -V2(T)*P31(T)/K2
453 -2*V2(T)*P31(T)/K2-V124(T)*P24(T)/K2+S2(T)*P24(T)
454 +P32(T)*((1-V122(T)/K1)**2)*P21(T)/(2*K1(T))-
455 2*P33(T)*((1-V122(T)/K1)**2)*P31(T)
456 -Q3(T)/K25
457 P32(T-1)*P32(T)+V*(
458 -2*V2(T)*P32(T)/K2-V122(T)*P22(T)/K2+S2(T)*P22(T)

```

459 -V2(T)*P32(T)/W2
460 2*(1-V122(T)/W1)*P31(T)+(-V11(T)/W1-V2(T)/W2-Q2(T)*(-V122(T)/W1-V122(T)/W1
461 1/2*K1(T)*W1)*P32(T)+(5S1(T)+2*Q3(T)*(-V122(T)/W1)/W1)*P33(T)
462 +P32(T)*(-1-V122(T)/W1)**2)*P22(T)/(2*K1(T))-
463 2*P33(T)*((1-V122(T)/W1)**2)*P32(T)
464 P33(T-1)*P33(T)+V*
465 -V2(T)*P33(T)/W2
466 -V2(T)*P33(T)/W2
467 +P22(T)*((1-V122(T)/W1)**2)*P23(T)/(2*K1(T))=
468 2*P33(T)*((1-V122(T)/W1)**2)*P33(T)
469 +0.515
470 H1(T-1)=H1(T)+V*(-2*V2(T)*H1(T)/W2+(-V122(T)/W2+
471 P12(T)*((1-V122(T)/W1)**2)/(2*K1(T)))*H2(T)+
472 (S2(T)-2*P13(T)*(-1-V122(T)/W1)**2)*H3(T)
473 -P12(T)*((1-V122(T)/W1)*H1(T)+H2(T))
474 +2*(1-V122(T)/W1)*P13(T)*H1(T)
475 H2(T-1)=H2(T)+V*(2*(1-V122(T)/W1)*H1(T)+
476 (-V11(T)/W1-V2(T)/W2-Q2(T)*(-1-V122(T)/W1)/(2*K1(T))*H1(T)+
477 P22(T)*((1-V122(T)/W1)**2)/(2*K1(T)))*H2(T)+
478 (S1(T)+2*Q3(T)*(-1-V122(T)/W1)/W1 -2*P23(T)*((1-V122(T)/W1)**2))*H3(T)
479 )+(-P22(T)*(-1-V122(T)/W1)*H1(T)+
480 +2*(1-V122(T)/W1)*P23(T)*H1(T))
481 Q2(T)+E*H1(T)/(2*K1(T))*H1(T)-2*Q3(T)*H1(T)/W1
482 H3(T-1)=H3(T)+V*(P32(T)*((1-V122(T)/W1)**2)*H2(T)/(2*K1(T))
483 +(-V2(T)/W2-2*P33(T)*((1-V122(T)/W1)**2))*H3(T)
484 -P32(T)*((1-V122(T)/W1)*H1(T)+H2(T))/(2*K1(T))
485 +2*(1-V122(T)/W1)*P33(T)*H1(T)
486 V1(T)=V1(T)+(-V122(T)/W1)*P21(T)*V2(T)-V20(T)+H2(T)/(2*K1(T))
487 P22(T)*V122(T)-V1220(T)+P23(T)*V122(T)-V1220(T)/W1-2*(1-V122(T)/W1)*V
488 -Q2(T)*V122(T)-V1220(T)/(2*K1(T))*H1(T)-V20(T)+
489 H1(T)*H1(T)+2*Q3(T)*V122(T)-V1220(T)/W1-2*(1-V122(T)/W1)*V
490 P31(T)*V2(T)-V20(T)+P32(T)*V122(T)-V1220(T)+P33(T)*V2(T)-V20(T)-H20(T)
491 +H3(T)+ 2*E*H1(T)
492 IF J.EQ.1 THEN BEGIN
493 V20(T)=V1220(T)+M20(T)=0
494 ELSE BEGIN
495 V20(T)=V2(T)*V1220(T)+V122(T)*M20(T)+M2(T)
496 ENDS
497 B2..END
498 V(T)=V1(T)-V11(T)
499 FOR T=(0,1,TF) DO A=MAX(T)
500 FOR T=(0,1,TF) DO B=MIN(BU(T))
501 FOR T=(0,1,TF) DO C=MAX(CRMN2(T))
502 FOR T=(0,1,TF) DO D=MIN(DRMN2(T))
503 IF T.EQ.1 THEN WRITE (ATB,C,D,T,ATB,C,D,T)
504 WRITE (NUMBER OF COORDINATION ITERATIONS,R)
505 ET=CLOCK
506 ET=CLOCK
507 TIMESET=BT
508 WRITE (COMPUTING TIME,T,TIME)
509 B4..ENDS
510 ENDS

```

B15 E15

B16 E16
B12 E12

B6 E6
B4 E4

APPENDIX V, PROGRAM 10



```

B0 BLOCK 1 LEVEL 1
1 REAL T,TF,IB,ITIME,TF,AV,IA,JE
2 REAL ARRAY X1,X2,X1S,X2S,P1,P2,M,MM,T11,T12,T21,T22,H1,H2,
3 DEL(-1,101)
4 COMMENT NON LINEAR COUPLING $
5 COMMENT GLOBAL METHOD $
6 FOR I=(1,16) DO BEGIN
7   TF=50%V=0,0015
8   FOR T=(0,1,TF) DO M(T)=0$
9   WRITE (CLOCK)$
10  BT=CLOCKS
11  FOR J=(1,1,1+1) DO BEGIN
12    E=J/TF
13    COMMENT FORWARDS INTEGRATION $
14    FOR T=(0,1,TF) DO BEGIN
15      X1(0)=5%$X2(0)=2$
16      X1(T+1)=X1(I)+V*(M(T))$
17      X2(T+1)=X2(I)+V*(X1(T)+0.1*X1(T)*X1(T)) $
18      DEL(0)=0$
19      DEL(T+1)=DEL(T)+V*(0.5*(X1(T)*X1(T)+X2(T)*X2(T)+M(T)*M(T))) $
20      IF ( T FOL IF ) AND ( J FOL (I+1) ) THEN WRITE
21      (DFL(T),I,T,V,DEL(T),I,T) $
22    ENDS
23    COMMENT BACKWARDS INTEGRATION $
24    FOR T=(TF,1,0) DO BEGIN
25      P1(TF)=0$P2(TF)=0$
26      P1(T)=P1(I)+V*(X1(I)+P2(I)+0.2*P2(I)*X1(I)) $
27      P2(T)=P2(I)+V*X2(T)$
28      HM(T)=M(I)+P1(T)$
29      IF J FOL (I+1) THEN GOTO B3$
30      I1(1,TF)=0$T12(1,TF)=0$T1(1,TF)=0$H2(1,TF)=0$
31      T11(T)=T11(I)+V*(T21(T)*(1+0.2*X1(T))+T12(T)*(1+0.2*X1(T)))
32      T11(I)*T11(I)+1+0.2*P2(T)) $
33      T12(T)=T12(I)+V*(T22(T)*(1+0.2*X1(T))-T11(T)*T12(T)) $
34      T21(T)=T21(I)+V*(T21(T)*(1+0.2*X1(T))-T21(T)*T11(T)) $
35      T22(T)=T22(I)+V*(T21(T)*T12(T)+1)
36      H1(T)=H1(I)+V*(T11(I)*H1(I)+(1+0.2*X1(T))*H2(T)+T11(T)*E*HM(T)) $
37      H2(T)=H2(I)+V*(T21(T)*H1(T)+T21(T)*E*HM(T)) $
38      M(T)=M(I)+E*HM(I)-(T11(T)*X1(T)-X1S(T))+T12(T)*X2(T)+H1(T)) $
39      X1S(T)=X1(T)$ X2S(T)=X2(T)$
40    B3..END$
41  IF ( T FOL 6 ) AND ( J FOL 7 ) THEN FOR T=(0,1,TF) DO WRITE
42  (HM(T),X1(I),X2(I),DEL(T),M(I),I,T)$
43  HM(T),X1(T),X2(T),DFL(T),M(T),T) $

```

E2

44 ENDS

45 WRITE (CLOCK) \$

46 ET=CLOCKS

47 TIME=ET-BI \$

48 WRITE (COMPUTING TIME, TIME) \$

49 ENDS

E1

END BLOCK 1 LEVEL 1



APPENDIX V, PROGRAM 11

```

BLOCK 1 LEVEL 1
1 REAL I,F,I,B,I,I,I,F,I,F,V,I,I,J,I,E,N,I,R,EPS $
2 REAL ARRAY X1,X2,I1,M,X1S,X2S,HM,H1I,P1,P2,T11,T22,H1,H2,DEL,
3 K(-1,0,1)$
4 COMMENT NON LINEAR COUPLING $
5 TF=50SV=0,0U1$
6 I=75
7 N=10SEPS=0,0$
8 WRITE (CLOCK)S
9 BT=CLOCKS
10 FOR I=(0,1,IF) DO BEGIN K(T)=M(T)*I(T)=1$ENDS
11 FOR P=(1,1,N) DO BEGIN
12 WRITE (STEP)S
13 COMMENT COORDINATION $
14 FOR I=(0,1,IF) DO BEGIN
15 K(T)=K(T)+EPS*(Y1(T)+0,1*X1(T)*X1(T)-T1(T)) $
16 ENDS
17 FOR J=(1,1,I+1) DO BEGIN
18 E=J/JI
19 COMMENT SUB SYSTEM 1$
20 COMMENT FORWARDS INTEGRATION $
21 FOR T=(0,1,TF) DO BEGIN
22 X1(0)=S
23 X1(T+1)=X1(T)+V*M(T)$
24 ENDS
25 COMMENT BACKWARDS INTEGRATION $
26 FOR I=(TF,1,0) DO BEGIN
27 P1(T-1)=P1(T)+V*(X1(T)+K(T)*(1+0,2*X1(T))) $
28 H2(T)=M(T)+P1(T)$
29 IF J EQ (I+1) THEN GOTO B3$
30 I1(T-1)=I1(T)-V*(T1(T)*I1(T)+I1(T)-0,2*K(T)) $
31 H1(T-1)=H1(T)-V*(T1(T)*H1(T)-T1(T)*E*H(T)) $
32 M(T)=M(T)+E*H(T)-(T1(T)*(X1(T)-X1S(T))+H1(T)) $
33 X1S(T)=X1(T)$
34 B3,END$
35 COMMENT SUB SYSTEM 2$
36 COMMENT FORWARDS INTEGRATION $
37 FOR T=(0,1,TF) DO BEGIN
38 X2(0)=S
39 X2(T+1)=X2(T)+V*(T1(T)*T1(T)) $
40 ENDS
41 COMMENT BACKWARDS INTEGRATION $
42 FOR I=(TF,1,0) DO BEGIN
43 P2(TF)=S

```

```

44 P2(T-1)=P2(T)+V*X2(T) 5
45 H1(T)=P2*(P2(T)-K(I))*H1(T) 5
46 IF J.EQ.(I+1) THEN GOTO 84$
47 T22(I)=0.5H2(I)
48 T22(T-1)=T22(T)-V*(2*T22(T)+T22(T)*T1(T))/(P2(T)-K(T))-1) 5
49 H2(T-1)=H2(T)-V*(2*T22(T)+T1(T)*H2(T))/(P2(T)-K(T))-
50 T22(T)*T1(T)*E*H1(T)/(P2(T)-K(T)) 5$
51 H1(T)=H1(T)+E*H1(T)/(2*(P2(T)-K(I)))-H1(T)*(T22(T)+X2(T)-X2S(T))+H2(T)
52 )/(P2(T)-K(T)) 5
53 X2S(T)=X2(T)$
54 P4=P4+$
55 IF (P.FOL N.) AND (J.EQ.7) THEN
56 FOR T=(N+1,IF) DO BEGIN
57 WRITE (I,PH(I),HT1(T),M(T),X1(T),X2(T),
58 H1(T),HT1(T),M(T),X1(T),X2(T)) $
59 ENDS
60 ENDS
61 WRITE (CLOCK)$
62 FT=CLOCK$
63 TIME=FT-BT$
64 WRITE (COMPUTING TIME,TIME) $
65 FOR I=(N+1,IF) DO BEGIN
66 DEL(T+1)=DEL(T)+V*(0.5*(X1(T)+X1(T)+X2(T)+X2(T)+M(T)+M(T))) $
67 IF T.EQ.IF THEN WRITE (DEL(T),P,I,DEL(T),R,I) $
68 ENDS
69 ENDS

```

LEVEL 1



BIBLIOGRAPHY

1. Dantzig, G., Wolfe, P., "Decomposition Principle for Linear Programs", Operations Research, vol. 8, No. 1, pp 101-111, 1960.
2. Pfouts, R. W., (editor), "Essays in Economics and Econometrics" Part 1, pp. 34-106, University of North Carolina Press, Chapel Hill.
3. Reich, S., "A Critique of Decomposition Technique for Optimal Control Problems", Systems Research Center, 103-A-67-45, Case Institute of Technology.
4. Kalman, R. E., "Some Methods of Linear Filtering", J. M. C. C., Dec. 15, 1964.
5. Takahara, Y., "Multilevel Systems and Uncertainties", Systems Research Center, 99-A-66-42, Case Institute of Technology.
6. Mc Reynolds, S. R., Bryson, A. E., "Successive Sweep Method for Solving Optimal Programming Problems", Proc. 1965 J. A. C. C., June, 1965.